MAY 1980



# ELECTRONICS TODAY INTERNATIONAL

# power amp! 140 W of 'rich, warm' sound

**'Auto-probe' project Test your car's electricals** 

**New S-100 bus specs** 

### HI-FI

Revolutionary speaker drive units explained SAE preamp and power amp reviewed

# A new dynamic generation of Maxell tapes.

When Maxell announces an improvement in the quality of its tape, you can bet the improvement has to be pretty dynamic. In fact, we think our new generation has even gone beyond our own standards of superior sound reproduction.

Take our high level (CrO<sub>2</sub>) position tape — the UD-XL II. Maxell engineers have succeeded in expanding its dynamic range in the middle-low frequency range by 1 dB, while also pushing its sensitivity by 1 dB in the high frequency range. Then look at our normal position UD-XL I, UD and LN tapes — our engineers expanded the dynamic range at all frequency points, while also boosting output in the high frequency range. The new dynamic range, of course, allows for better music reproduction even for LN-type tapes.

On the UD-XL I and II, we also added an exclusive shell stabilizer for significantly improved tape running and track positioning.

One thing hasn't changed on all Maxell tapes — our functional features like 4-function leader tape, replaceable index labels for UD-XL series tapes and Maxell's through-production system — your guarantee of quality and superior sound reproduction.

Tape selector position UD-XL I, UD, LN: Normal position (Normal bias/120 µsec. EQ) UD-XL II: High level position (High level bias/70 µsec. EQ)









For details on all Maxell Recording Tape write to Available time length UD-XL I: 60, 90 min./UD-XL II: 60, 90 min. Maxell Advisory Service, P.O. Box 307, North Ryde, N.S.W. 2113 UD: 60, 90, 120 min./LN: 60, 90, 120 min.

Distributed by...

HAGEMEYER





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World's 1st Electronic Credit Card

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#### **READERS NOTE!**

THIS EDITORIAL is about how to get the most out of the 'information' pages we include in the magazine each month. These information pages are titled "Shoparound", "Kits for Projects" and "Services". These last two you will always find together at the back of the magazine, immediately before the 'Dregs' page just inside the back cover. In this issue they're on pages 168 and 169.

Kits for Projects lists 17 companies that stock various projects published in the magazine over the past few years. The projects are listed in ten categories and each project is assigned a particular number. Complete kits, or printed circuit boards and the relevant components, may be obtained from the companies indicated in the list. In addition, two companies who can supply virtually every pc board we have ever published — RCS Radio and Radio Despatch Service — are listed. Whenever you are chasing' for bits for past projects — this is the page you should consult first. The information on this page is updated several times a year.

At this point I would also like to make it clear that our business is to publish this magazine — we do not sell kits or components — but our advertisers do!

Shoparound generally discusses projects in the current issue and where kits or components may be found for these. If components are widely available, no specific suppliers will be mentioned. Also, we use this page to keep you up to date on new components or past projects, interesting new gadgets or components, or items of topical interest to the hobbyist.

Recently, we commenced giving price estimates in Shoparound for current projects. We have commented in detail in this month's column, but we would also like to stress here that these prices are estimates only. They should not be taken as recommended prices. On occasion, for a variety of reasons, our estimates may be low. Don't abuse your supplier if you find his price higher than ours. The electronics retail business is too competitive for anyone to be suspected of 'ripoffs'

The **Services** page tells you how to access the various services we provide for you how to make enquiries, how to obtain back issues or photostats of articles, etc. A coupon is provided for your convenience. It makes things so much quicker if you use the coupon when ordering anything from us. If you don't wish to mutilate your magazine, photocopy the coupon and use that.

Turn to each of these three pages, right now — 85, 168 and 169, and see what they're all about

After all, they're there to help you!



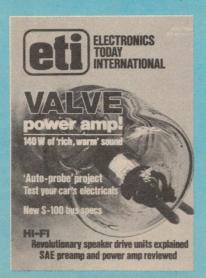
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#### ELECTRONICS TODAY INTERNATIONAL



#### COVER

To herald our first valve project, we just had to have a picture of a valve on the front cover! The device is some 40 years old and is a type 15E triode, made by Eimac for 600 MHz airborne radar systems developed for WW II.

#### features

#### TOOLS & TECHNIQUES IN RADIOMETRIC EXPLORATION

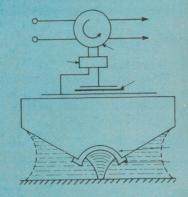
A rundown on the instruments and techniques used in exploring for radioactive minerals.

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#### ULTRASONIC MICROSCOPE LOOKS INSIDE TRANSISTORS

US research has led to the development of an ultrasonic imaging technique that can look 'inside' the structure of materials.

#### WORLD'S 1ST ELECTRONIC CREDIT CARD

A new 'electronic credit card', developed in Italy for use in pre-paid telephones, is likely to have many uses.

#### news

#### **NEWS DIGEST**

Solar generator for the centre?; New TV channel for UK; 25 MHz dual-trace CRO; Technics back JVC video disc; New transistors; Hatched, matched, despatched.

#### PRINTOUT 92

Two local firms win design awards; Micros invade the office; Static ROMS from National; Bar code printer, SMUG club; New LEDs.

#### COMMUNICATIONS NEWS 11

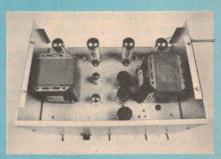
New body for two-way radio users; Sunspots — countdown to a maxima; CB for UK ?; Radio security.

#### SHORTWAVE LOGGINGS

Dubai tests; Latin-African Log; Bhutan; Brazilian signals peak; African news; Radio Thailand in clear.

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#### projects



#### **456: 140W VALVE AMPLIFIER**

Dubbed "The Rocker", this beast is quite versatile as it can be used for guitar work or as a 'hi-fi' valve amp.

#### 325: AUTO-PROBE

Checking faults or tracing wiring in a vehicle's electrical system using a multimeter is generally tedious and frustrating. This little gadget eliminates the drudgery and the guesswork.

#### **560: MAINS CABLE SEEKER**

47

Don't mount that picture hook until you've found where the mains cable runs — this handy project shows you the way.



#### 636: S100 MOTHERBOARD

Now you can tidy up all those S100 project po

#### **LAB NOTES**

All about walking rings and performing other miracles with counter chips

#### sound

#### **SOUND NEWS**

125

Technics' award winners; Speakers and cartridges from Concept; Tune in on Audiosound; Sound Archives conference; Pioneer price cuts; Sanyo cassette decks.



#### **REVOLUTIONARY SPEAKERS EXPLAINED**

and their new SB series speaker systems.

131 All about Technics' new "honeycomb disc" drivers

#### S.A.E. PREAMP-POWER AMP

subjective impressions of the amplifiers performance were outstanding.



#### **MARANTZ 1300DC STEREO AMP** 154

an excellent example of careful design and planning ... a first class piece of equipment

#### **AKAI PS-200T TUNER**

162

146

"The quality of the sound is in general terms as good as some of the best tuners and receivers we have listened to ...

#### **REEL-TO-REEL TAPE OFFER**

121

#### Superb Ampex tapes at a low price.

#### enera

#### **AUTOSTART FOR RTTY**

101

Now you can automate your RTTY station and leave it to print messages in your absence. Tom Moffat's concluding article.

#### **UPDATE ON THE S100 BUS**

Inside the all-new, singing, dancing, virgin-refresh, \$100 bus.

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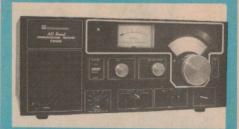
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#### next month



#### **RECEIVERS FOR THE BUDGET MINDED SW LISTENER**

If you'd like to get into the hobby of shortwave listening and 'DXing', but have a limited budget — then you should read this article.



#### 3-WAY SPEAKER — THE 4000/2

Continuing our Series 4000 projects, this three-way system is another superb design from David Tilbrook.



#### THE ROTEL RX-1000 AM/FM RECEIVER

Featuring a phase-locked loop tuner, this receiver should attract the hi-fi enthusiast interested in joining in the boom on the FM band.

Although these articles are in an advanced state of preparation, circumstances may affect the final content. However, we will make every attempt to include all features mentioned here.

### STAGE EN ELFERS LIGHTING ALLYOUR REQUIREMENTS AUSTRALIA WIDE



# HASER 4



This is the lighting controller that makes any imported controller obsolete — The Chaser 4 Four channels, up to 10 amps maximum unit loading, will chase at a preselected rate, variable at the rate control. On music peaks, the chase mode automatically reverses! Push buttons allow chase, shadow chase (3 channels on, 1 off) and Colour Organ. In the Colour Organ mode, the 4 channels respond to different frequencies - the audio signal feed is via a 6.5mm jack socket at the rear of the the unit. Audio level-in is at speaker level — up to 200 watts. The Chaser 4 is well built, designed for Australian applica-tions, and guaranteed. With local service facilities available

- 4 CHANNEL AUDIO CHASER
- 4 CHANNEL COLOUR ORGAN
- RESISTIVE or INDUCTIVE LOADS
- 10A MAXIMUM LOAD
- FORWARD AND REVERSE CHASE
- SHADOW CHASE FUNCTION

THE COMBINATION CHASER/COLOUR ORGAN THAT CAN BE USED WITH HOTSPOTS!

### ROBE CONT ROLL











NOW - 20 percent off recommended prices on a complete package of 4 superstrobes, and the new Cietex strobe pulser. The strobe pulser gives you total control over your strobes, offering either rainbow chase, tandem flip-flop or all flash functions. Either at a preset rate or with an audio input! Create

#### SNAKELITE TUBELITE

The Flowbox allows direct connection of 24V Snakelite or Tubelite - up to 20 metres! Where a Snakelite audio chaser is not reguired, the Flowbox does the trick. For that budget application, or for displays - the Flowbox! (Flow rate variable by preset control).

#### SEE US FOR **EVERYTHING** IN STAGE & EFFECTS LIGHTING

- Spotlights Strand & Altman
  Dimmers Flight, Strand &
- Jands
- Colour Gel Roscolene & Lee • Effects — We've got it all
  - EVERYTHING!

# THE NEW GENERATION

RACK MOUNT RANGE IS COMING!

This 1 cm sq high-impact plastic tube is made to order, with tiny clear lamps at varying spacings. Wired at 24V, it can be used for anything! In dance floors, around windows, and - never before in architecture! Just imagine tubelite built into walls, up handrails, even in swimming pools!!! The posssibilities are limitless, especially considering the miniature lamps have a 25,000 hour rated life! Tubelite can be run from a transformer or from a Snakelite Flowbox (see above).

- LENGTHS TO ORDER
- 25.000 HOUR LAMPS
- HIGH IMPACT TUBING

SYDNEY: Ceitex 2/33 College St Gladesville (02) 896.2900

WOLLONGONG: Trilogy Electronics 40 Princes Hwy Fairy Meadow (042) 831,219

NEWCASTLE: Your Move Lighting 37a Beaumont St Hamilton (043) 693.560 BRISBANE: Harvey Theatrical Lighting 21 Crosby Rd Albion (07) 262.4622 GOLD COAST: Rave Audio Visual 2388 Gold Coast Hwy Mermaid Beach (075) 383.331

MELBOURNE: Clearlight Shows 17 Alex Ave Moorabbin (03) 553.1446

MELBOURNE: Lighting Corporation 131 Brighton St Richmond (03) 429.5122

ADELAIDE: Hiwatt Lighting 37 Angus St Adelaide (08) 212.2033 ADELAIDE: Psycho Lites PO Box 291 Nth Adelaide (08) 471.874 PERTH: Western Strobe Lighting 1142 Hay St West Perth (09) 321.9363

PERTH: Kosmic Sound 1074 Albany Hwy Bentley (09) 361.8981 HOBART: Good Oil Sound 310 Liverpool St Hobart (002) 235.151 Also available Australia-wide at Strand Rank electronic outlets.

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# MAGGATHE

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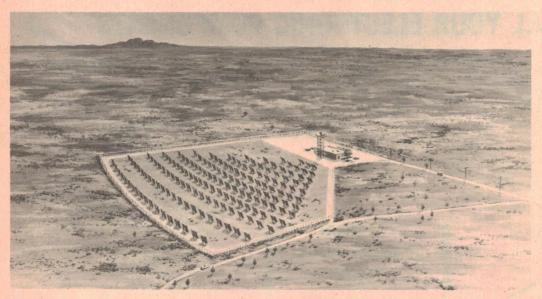
N THE HEART OF MELBOURNE

Where price is important but service is paramount.

FULL RANGE OF COMPONENTS, PC BOARDS, ETC, FOR ETI AND OTHER PROJECTS

# TEMS digest

### Solar generator for the 'centre'?



The Northern Territory Government is studying a proposal to build a 1000 kilowatt solar powered electrical generator near Ayers Rock.

The scheme, proposed by thermal energy 'receiver'. The **McDonnell Douglas (makers** of the DC-10 aircraft), is designed produce to electricity for Yulara, a 300unit tourist village that the N.T. Government propose to build near Ayers Rock, some distance from Alice Springs.

The proposal stems from efforts by the Ministry and the Northern Territory Electricity Commission to sharply reduce the region's dependence on oilbased energy sources.

The generator features a solar-thermal conversion system and it is believed it will cost something like \$10 million to construct.

Whilst the initial capacity is rated at 1000 kW output, provision has been made to expand the plant to 2000 kW capacity. It is anticipated the plant would displace nearly one million litres of oil, that would otherwise be necessary, at its initial capacity of 1000 kW, saving around \$230 000 annually, doubling that at full capacity.

The station is dominated by a 50m high tower, topped by a

tower is surrounded by a four hectare (10 acre) field of mirrors, called heliostats, which follow the sun as it moves across the sky, reflecting its rays onto the receiver atop the tower. The position and movement of the mirrors is controlled by a computer.

The heat of the sun is absorbed at the receiver by a special fluid circulating through it. The heated fluid is then used to convert water to steam in a heat exchanger, which drives a turbine and generator.

A unique feature of the solar generator is the composition of the fluid which is used to store the sun's heat. This fluid is a mixture of special salts, forming a 'eutectic', which melts at 80°C. They are heated to 450°C by the sun, without an increase in pressure in the

Although this fluid has never been used for this purpose before, McDonnell Douglas is confident that the system will have no teething problems. They point out that the hot fluid can be stored overnight so that electricity can be generated continuously.

Excess heat from the steam turbine can be used in a desalination plant making use of the locally available brackish ground water to produce around 70 000 litres of water a day, suitable for domestic or agricultural use.

There are considerable engineering problems in the storage of large quantities of fluid at the high temperautre of 450°C. (Red heat for steel is around 520°C). Some form of backup system will probably be required in case of cloudy days or computer failure, especially since the liquid would return to a solid in the pipes in the event of an extended shutdown.

At the present time however, the solar generator is being promoted as a system which is completely independent of fossil fuel generator back up systems.

Curiously, 1000 kW will only partly supply the energy requirements of a 300-unit village, delivering around 3 kW (peak load) per unit. In an arid climate this only allows for air conditioning, appliances and lights. Such niceties as stoves would have to be fuelled from other sources, as these require 10 kW or more at peak load.

On present day prices, the

cost of electricity from dieselgenerator power stations of similar size is approximately 8c/ kilowatt-hour in comparison to 19c/kilowatt-hour for solar power (assuming 10% interest paid on the capital investment).

The 'Economist' magazine, in its comparison of electrical energy costs for the years 1990 to 2000, predicts that solarthermal generation will remain the most expensive way of producing electricity.

In the year 2000, electricity generated by this method will be 15% more expensive than by direct conversion of the sun's rays to electricity, and nearly twice as expensive as electricity from wind generators.

By comparison, hybrid systems which employ a combination of wind power, solar-electric generation (solar cells) and storage batteries plus standby diesel are considerably

less expensive.

Although currently available systems are only relatively low power, such as the Australianproduced 'Hybrid Energy System' by Dunlite of South Australia, larger capacity systems would be competitive. Projected cost for a 1000 kW system would be in the vicinity of \$5 million — around half that for the McDonnell Douglas solar-thermal system.

McDonnell Douglas also manufactures the F-18 Hornet strike fighter, currently under consideration by the Australian Defence Department modernise the Royal Australian

Air Force.

At a press briefing on April 1st Chief Executive McDonnell Douglas, Sanford McDonnell, said that two years ago the Prime Minister, Malcolm Fraser, had suggested to him that the cost of a solar generator - such as the one being proposed — could possibly be offset against the Australian Industry Participation (AIP) portion of any contract to purchase aircraft. (The AIP

scheme provides that a certain company. portion of military equipment bought overseas must be built in Australia, thus providing jobs and developing skills in local industry as well as reducing the 'external cost' of overseas purchases).

McDonnell Douglas have signed an agreement with Sabemo Pty Ltd, to co-operate on the plan to build the solar power generator. Sabemo is a Sydney-based civil design, construction and engineering group and a sister company of Transfield Pty Ltd, a major steel will be more of a 'symbolic and fabrication

McDonnell Douglas and Sabemo officials say the plant could be operational by mid-1983

The decision to go ahead with an alternative energy system for Yulara is essentially a political one. The McDonnell Douglas solar-thermal generator is expensive and untested. The Northern Territory Government consider it will apeal as a tourist attraction, apart from its 'practical' purpose.

As such, it seems its function

erection sculpture'.

#### New TV channel for UK

Britons are to get a fourth TV programme channel to be transmitted over a network of UHF transmitters and controlled by the Independent Broadcasting Authority.

At present, television viewers in Britain have a choice of three programmes. Two programmes are transmitted by the state-owned British Broadcasting Corporation and are known as BBC-1 and BBC-2. The third channel is operated by the Independent Broadcasting Authority (IBA) and is financed by advertisements transmitted in the intervals between programmes.

The present government decided that the IBA will have control of the fourth channel and that this new programme will be financed through advertising.

The financing of two television channels through advertising involves the danger of both IBA networks striving to achieve maximum popular appeal. There is currently more demand for television advertising than can be accomodated on one channel.

The IBA must not allow the two commercial channels which are financed by advertising to compete for a maximum audience; neither will the five main television companies who produce the present programmes transmitted by the IBA be allowed to dominate the programme content of the proposed new fourth channel, Britain's Home Secretary, William Whitelaw, Said.

The IBA must make arrangements for the largest practicable proportion of programmes to be supplied by organisations and persons other than the television companies contracted to provide the programme being transmitted on the present independent channel, he said.

The new network will have its own controller and its own income. The IBA will be expected to ensure that an adequate budget for the new channel will be provided to achieve the reguired service, but the finance will not necessarily be determined only by the revenue from advertising. Thus it seems revenue from the existing IBA channel will be used to finance the new fourth channel in Britain.

The IBA have already been empowered by Parliament to commence the building of a new network of UHF transmitters for the fourth national television network. The cost of operating the new channel will be about 60 to 80 million pounds per year.

**Brian Dance** 



#### Alarmed? Get Dick on the job

Burglary is an unpleasant business for the victim, no wonder many people seek ways and means to make it unpleasant for the burglar — with electronic burglar alarms.

Dick Smith's latest model burglar alarm, No. L-5102, is designed for installation in the home, office or factory and should certainly make things uncomfortable for the would-be

The unit, housed in an attractive walnut-veneer box, looks not unlike a very small speaker enclosure and features both normally open (n\*c) alarm loops for window and door

panic vibration switches etc. The builtin siren has provision for an external horn if desired. A remote switch function allows for control of the unit from a distant point.

Price is only \$59.50, sensors etc are extra but all available from Dick Smith. Try your nearest Dick Smith store or

dealer.

#### **Briefs**

Plessey Optoelectronics and Microwave Limited of the UK has introduced a new series of passive infrared long range detection systems. These new devices have a detection range of 100 m and police in the UK have been using them for outdoor surveillance for some time. The units will detect a heat source with a temperature greater than one degree Centigrade above background if it is larger than half a metre square at 100 m distance (e.g. a person). Various fields of view are available, and sensitivity is adjustable. The series incorporates a screened micropower amplifier, level detector, an alarm indicator. change-over relay alarm output and triped fixings.

Matsushita have developed a new electron gun they claim improves colour TV image resolution by 20% or more. The main secret, they say, is the development of a new lens device. Apparently, it has an in-line gun but three electron lenses arranged side by side. The firm has already begun mass production of colour TV tubes using the new gun.

new voltage/current threshold detection optocoupler with guaranteed input-threshold specifications and logiccompatible output has been introduced by Hewlett-Packard. It is designed for industrial control computer input boards and other applications where a predetermined input threshold level is desirable.

The HCPL-3700 combines a threshold-sensing input buffer IC, an internal LED and a highgain photon detector to provide an optocoupler which features adjustable external threshold levels and logic-compatible

In quantities of 1 to 99 the HCPL-3700 is priced at \$6.61 for 100 to 999 pieces, the unit price is \$4.82. It is in stock at HP distributors. For further information contact Cema Electronics Pty Ltd, 21 Chandos Street, St Leonards NSW 2065 or at 208 Whitehorse Road, Blackburn Vic

# MEMS digest

# Technics back JVC video disc system

The public will be forced to choose between three video disc systems when the big disc war gets underway in the next two years.

National Panasonic announced at a press conference in Terrigal, NSW, recently that it will back the JVC video disc system.

Asked why Matsushita (the mother company of National Panasonic) had decided to back a third system against the Philips and RCA systems, and cause the sort of confusion that dogged the steps of video recorders, and before that four channel sound, Mr Toshiro Masui (a Technics Director attending the press conference from Osaka) said that Matsushita had decided to abandon its own system and back the JVC system to try and "ease the confusion" that will face the

"We gave up our system to adopt the JVC system," he said "and other Japanese manufacturers are expected to follow."

Although some of the reasons given are sound enough for the company's decision, it looks as if the electronics market place is to always have to contend with the eternal triangle-Japan, versus America, versus Europe.

RCA is American, Philips European and JVC Japanese.

Which Japanese companies are to follow the Matsushita lead to adopt the JVC system is not known and the canny executives from Matsushita were not about to enlighten us at the Terrigal conference.

But as interested as we were to find out what sort of Nipponese weight was to be put behind this third video disc system we were even more intrigued to find out which company would be supplying the vital software material, without which any video disc in the market place is doomed.

MCA Universal, according to

a director of that company, has over 50% of the entertainment industry in the USA tied up, and is completely committed to the Philips system.

RCA will source entertainment software from its vast TV and film companies into supporting its own format, due out in 1981.

Who then is to supply the vital software to JVC? Matsushita executives were tight lipped about this subject too, refusing to say anything although they did exchange a few pointed and knowing grins.

The guess amongst the press is Disney Productions, although this is sheer speculation.

When examined under an unemotional light (we all tend to get very emotional about intercompany and international battles over industry standards because it is always the consumer who loses out in the long run) Matsushita has some sound arguments for going it alone.

Mr Masui says that the MCA Universal — IBM — Pioneer conglomerate is having a lot of problems producing the software for the Philips system because it is such a complex process.

On the other hand the Philips system, using an optical stylus system with random access and freeze frame freatures, is excellent.

The RCA system uses a mechanical stylus and a grooved disc. This sort of disc is easy to produce in conventional record factories but does not offer random access.

The JVC system on the other hand,, has the advantages of both systems without the disadvantages. It uses a disc that can be pressed in normal record factories but has random access. It uses a part mechanical

and part optical system.

Mr Masui claims that the JVC units will be cheaper and more reliable than the Philips units.

He also says that the highlights of the 1980s will be video disc and PCM audio. This will develop side by side and any video disc system should be able to play back PCM audio discs as well.

This, the JVC system will do. However, Philips have developed a separate PCM audio system to complement the Philips video disc system, he points out.

Although the video disc became one of the more heated debates at the Terrigal conference the real reason for all of us being there, besides the booze and the beaches, was to see Technics release its new range of hi-fi. Turn to "Sound News" for a full report.

**Dennis Lingane** 

# Philips win \$1.7M order from South America

Philips-TMC, the telecommunications manufacturing company of Philips, have been awarded a \$1.7 million contract for a radio communications network for Fenatach, the National Federation of Professional Taxi Drivers of Chile.

This communications system innovation is wholly designed and manufactured in Australia by Philips-TMC. It comprises: three SI 10 000 status and identification system

consoles; 1000 FM828 mobile two-way radios and associated base stations and line switching equipment

The system will be installed in Santiago to control the 1000



taxis in the Fenatach fleet.

The Santiago taxi service is similar in size and in operation to Taxis Combined Services in Sydney — one of the world's largest.

Philips supplied an SI 10 000 system to Taxis Combined Services in Sydney early last year and has since supplied a similar system to Hong Kong.

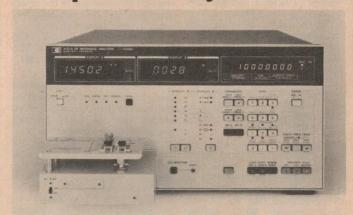
Fenatach President (Senor Juan Jara Cruz) and two of the Federation's Directors are visiting Sydney to study the operation of the SI 10 000 system in Taxi Combined Services.

In the Philips system voice

transmission from each taxi is replaced by coded data transmissions. These provide the identification and status of each vehicle and enable the driver to bid for jobs and acknowledge them in a fraction of a second by a pushbutton operation. The system includes an alarm facility which identifies the taxi and provides a means to monitor conversation within the taxi in the event of hold-ups or attacks.

The complete system will be supplied and installed in Santiago within six months and will be commissioned and fully operational in eight months.

#### MPU controlled RF impedance analyzer



The Hewlett-Packard model 4191A RF impedance analyzer was designed for making high frequency (1 MHz to 1 GHz) evaluation measurements of electronic materials, components and circuitry.

It can measure fourteen impedance parameters over a frequency rang of 1 MHz to 1 GHz with a basic accuracy of 0.5% to 2%. An internal frequency synthesizer, automatic calibration, automatic error correction and specially-designed test fixtures make stable, accurate impedance measurements possible over a measurement range of 1 M to 100 k (1 uses to 50 sec).

In addition, the 4191A features an internal bipolar dc bias source, linear and log sweep capabilities on all 14 paramet-

These features make the 4191A an excellent design and testing tool for high frequency evaluation.

The duty free price is \$13 630 and further information can be obtained from Hewlett-Packard Australia Pty Ltd, 31-41 Joseph St, Blackburn Vic 3130; (03) 89-6351 or any of their branches.

#### New audio oscillator redefines distortion limit

The new Tektronix SG606 audio signal generator features total harmonic distortion of less than 0.0008% from 20 Hz to 20 kHz.

Packaged as a plug-in for the TM500 family of modular test and measurement instruments, the SG505 can be readily combined with the user's choice of over 40 other plug-in instruments (oscilloscopes, counters, digital multimeters, amplifiers, function generators, and others) in a single package. This feature is especially valuable in audio measurements where common applications away from the lab bench dictate por-

The frequency range of 10 Hz to 100 kHz for the SG505 encompasses the entire audio band. This range is covered in four overlapping bands selected by pushbuttons. Within each band frequency is selected by a continuous tuning dial.

Output signal amplitude is greater than 6 V RMS unloaded and greater than 3.12 V RMS into 500 ohms, say Tektronix. Control of the output level is provided by a precise eight-step attenuator ranged from -10 dBm to -60 dBm. Claimed step accuracy for each 10 dBm increment is 0.1 dB. Within each step, a variable control provides continuous adjustment. An on/off switch allows disconnecting the output signal at the touch of a button. A second pushbutton selects between ground-referenced or floating output.

A sync output terminal provides a 200 mV rms sinewave which tracks the selected frequency of the output. Both the output and the sync signals are available at the rear connector of the SG505 as well as at the front panel. This facilitates easy interconnection with other TM500 plug-in instruments.

An optional intermodulation test signal provides, at the touch of a button, a combined signal consisting of a low frequency 60 Hz/250 Hz) (selectable sinewave and a sinewave of the dial-selected frequency. The two components are mixed in a 4:1 amplitude ratio. Amplitude of the combined signal is within 0.2 dB of the amplitude of the fundamental signal alone.

Further details from Tektronix Australia Ptv Ltd. 80 Waterloo Rd, North Ryde NSW 2113. (02) 888-7066.

#### Temperature and pressure instruments

Amalgamated Instruments Co Pty Ltd have a range of temperature and pressure measurement and control instruments available.

These are designed and manufactured in Sydney and AIC are looking for agents around Australia.

Their handheld digital thermometer is believed to be the smallest presently available, and with its high accuracy and wide range is ideal for a pocket unit for quality control.

The circular dash- or panelmounted indicator is proving popular in the marine industry for measuring sea water temperature to locate currents by change in water temperature.

Temperature controllers are also available and AIC offer design prototyping and manufacturing services for most small scale applications.

For further information contact Amalgamated Instruments Co Pty Ltd, P.O. Box 305, Narrabeen NSW 2101. (02) 452-2648.

#### Hatched, matched, despatched

Brief news on company activities, new outlets, mergers, joint ventures and closures.

#### Hatched

• A NSW CSIRO State Committee' was announced recently by the Minister for Science and the Environment, Mr David Thomson.

The committee will act as a link between the CSIRO and individuals and associations in NSW and provide an input to the CSIRO Advisory Council.

The Committee will also be involved in making the work of the CSIRO more widely known in NSW", said Dr J. Paul Wild, Chairman of the CSIRO.

• A new digital components and microcomputer store opened in Sydney late in March. Called Microbits, they carry such goodies as Motorola, Fairchild, and National semiconductors (like the 74 and 74LS series, 4000 series, 6800/9000 series, EPROMs and drivers etc) plus a large range of Molex and Utilux connectors and clips.

On top of all that they carry boards from Pennywise Peripherals (at Melbourne prices) . . . static RAMS, EPROMs, cassette interface etc.

Check them out at 280 Victoria Rd, Gladesville 2111. (02) 89-3145.

• The Standards Association of Australia has published a revision of the standard graphics symbols for electrotechnology, Part 9, binary logic elements. Designated AS.1102 (9.20), copies may be obtained from offices of the Association in all state capitals and Newcastle (NSW).

They also recently released a draft, DR.79187, of a new Australian standard guide for the selection and use of power transformers. Copies obtainable as per above.

 Ferguson Transformers Pty Ltd added three newly-hatched power transformers to their range in March. Designated type nos PF4361, PF4362 and PF4363, they have nominal ratings of 200 VA, 300 VA and 300 VA respectively and may be configured with various output voltages. Readers may remember the PF4363 was used in the power supply for our 300 watt amp featured in the February issue.

Full details from Ferguson Transformers Pty Ltd, P.O. Box 302, Chatswood NSW, 2067. (02) 407-0261

• A new solar-powered watch has been launched on the market. Called the Sunwatch" it comes with 10 display functions: hours, minutes, seconds, months, dates, leap year, speed calibration, AM/PM indicator and seconds count off. It also features an adjustable brightness display (four levels) and is programmed to the year 2100.

No batteries are necessary and the Sunwatch comes complete with a two year warranty from Quality Gifts International, P.O. Box 410, Surfers Paradise QLD 4217. (075) 38-3472

#### Matched

• You can now match some new modules to your TI Speak & Spell". There are three in the range, called Vowel Power', Super Stumper 4-5-6' and Super Stumper 7 and 8'. These modules expand the capability of this unit by 125 to 140 words. Their content has been thoroughly researched to include the most commonly misspelled words.

They come with an informative 12-page booklet that provides basic information and lays out games and activities designed to guide the child through the learning process. More info from Texas Instruments' customer service, (02) 887-1122.

 Datatel Pty Ltd has announced the acquisition of the maintenance facilities of ATL Datatronics Ltd. The purchase includes a range of test equipment and jigs, sub-assembly spare parts and other stock items to support a variety of products manufactured by ATL. A number of former ATL staff have joined Datatel, with Mr Paul Redshaw appointed as Service Manager.

Datatel Managing Director, Mr Dieter Retz, stated that Datatel expected the extended service facilities, located at the company's South Melbourne headquarters, will improve responsiveness to customer repair demands and to enhance the company's marketing base.

Datatel are located at 3 Raglan St., South Melbourne Vic 3205 (03) 699-7614.

#### Despatched

 Australia's first Unimat 4020 computerized telephone exchange was installed at the premises of Dominguez and Barry, the only specialist fixed interest house in this country.

Described as the ultimate small PABX, measuring a mere 670 x 650 x 180 mm, the unit was supplied by STC. Another three are expected to be installed in Sydney shortly, and a further two in Melbourne. Following this introductory stage, STC plans to assemble the units in Australia.

The Unimat 4020 can carry up to eight exchange lines and 32 extensions.

- The annual report of the Electronics Research Laboratory, Department of Defence, for 1978-79, was released recently. It covers the recent activities of the organisation which has been involved in radio propagation, antenna, radio navigation, semiconductor and computer research. One presumes copies are available from the Australian Government Publishing Service. It's very interesting reading.
- A new two-page technical data sheet from Hewlett-Packard describes the use of their low-pass filter kit and how it can be used to reduce high frequency noise errors in low frequency measurements.

Designed specifically with frequency counters in mind, the kit provides a selection of four filters with low attenuation. They can also be used with CROs and spectrum analysers. The data sheet is numbered 5952-7554 and is available free of charge from Hewlett Packard Australia Pty Ltd, P.O. Box 36, Doncaster East Vic 3109.

• Two new catalogues became available from Instant Component Service recently. First up is the Pomona Test Accessories catalogue — 1980 edition. It lists a broad variety of test accessories, including: banana plugs, jacks, patch cords, phone tip jacks, test clips, probes, binding posts, black boxes and sockets. Available on request.

Second comes the Connectors for Commercial and Industrial Applications" catalogue from STC-Cannon Components. The new connector range is designed to MIL-C-5015 and covers applications suitable for Australian environments. It lists crimp, potting, high voltage, RFI shielding, mains and bayonet lock connectors. This catalogue is also available on request from ICS.

• IRH components has moved from their old location in The Crescent, Kingsgrove to 53 Garema Circuit, Kingsgrove 2208. Their postal address is P.O. Box 265, Kingsgrove and phone number (02) 750-6444, telex AA24949.

IRH will continue to manufacture their full range of fixed and variable wire-wound resistors, including the popular PW resistors and AW pots. They are also agents for Fujitsu, Hitachi Condensors, Murata, CTS (USA) and TRW/IRC (USA).

 Dick Smith's Adelaide store has moved a few hundred metres down Wright Street to larger premises.
 Dick Smith's Adelaide outlet first opened in December 1977. The old store had 370 sq. metres of space, while the new store has 550 sq. metres, an increase of almost 50%.
 Parking for 20 vehicles is provided.
 New address is 60 Wright St. phone 211-1962.

ter makes it possible to increase the doping of the base region without degrading any other of the characteristics.

Further transistors using this Sipos method will soon be put on the market by Sony Corporation.

#### High current gain transistors

The Sony Corporation has developed a new npn transistor which is similar to the present ones except that it has a current gain 50 times greater.

It is a silicon device employing a 'heterojunction emitter' having the same emitter area as the conventional npn transistor.

These transistors are manufactured by the use of highly phosphorous-doped low resistivity variation of a semi-insulating polycrystalline silicon, which Sony has named 'Sipos'. In addition to the greater current gain, Sipos provides a 90% decrease in base resistance and an increase in current capacity five times greater than the present one.

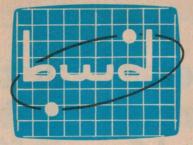
The reason for these advantages is that the heterojunction emit-

#### **Peterson Speaker Laboratories**

The above company's advertisement on page 25 in ETI April inadvertantly contained copy giving the impression that Peterson speakers are available directly from the company.

In fact, Peterson speakers are available **only** via retailers — not directly from the factory. The advertisement should have read (in part) Available at most reputable high fidelity sound centres or **information** from" Peterson Speaker Laboratories Pty Ltd.

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Protronics Pty. Ltd., Adelaide. Ph: 212 3111 Warburton Franki (Perth). Ph: 277 7000 Associated Agencies Pty. Ltd., Hobart. Ph: 23 1843 TAS.

Instrep Pty. Ltd., Hobart. Ph: 34 3194 P.H. Rothschild & Co. Ltd., Wellington. Ph: 66 3581 W. Arthur Fisher Ltd., Auckland. Ph: 59 5527

#### REALISTIC

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- •Tuned AM-RF Stage •Includes custom walnut veneer side panels

75 Watts per Channel, Minimum RMS, at 8 ohms from 20-20,000 Hz with no more than 0.25% total harmonic distortion

The Realistic STA-2000 is designed and manufactured in our own factory to deliver perfectionist quality at an unbeatable price. With 75 low distortion watts on each direct-coupled channel, the most demanding music stays undistorted even at live-performance listening levels. Ultra stable and dependable IC's are in the FM IF detector and PLL sections. Audiophile controls provide wide system flexibility and customized sound. Pushbutton multiplex filter cleans up high-frequency noise on weak FM signals. Complete taping and dubbing facilities for two decks. with long throw switches and both DIN and phono-type in/out jacks for hookup to any equipment. Massive flywheel tuning knob, with switchable muting to eliminate interstation hiss, built-in protection against thermal problems, speaker over-driving or shorting, and switching transients. Plus fine styling that makes people notice the STA-2000 even before you turn it on. 31-2075.





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# Tools and techniques in radiometric exploration

All areas of geophysical exploration are becoming increasingly dependant on electronic instruments in the search for minerals and energy sources. Radioactive minerals, in particular, are in great demand. Here's a rundown on the instruments used and how they are employed.

#### Malcolm J. Plunkett

URANIUM EXPLORATION started in earnest after the second world war when "every man and his dog" was selling up and heading for the bush with geiger counter in hand. At that time, the major deposits were discovered purely by surface indications of radioactivity. However, that era is virtually at an end, and future finds are more likely to be below the surface or in inaccessible areas. The Roxby Downs deposits in South Australia for example are over 300 metres below the surface.

It has been necessary therefore to refine existing prospecting techniques, develop new ones, and improve the sensitivity and discrimination of all instruments in radiometric measurement techniques in common use, and to give some insight into the various methods of radiometric surveying.

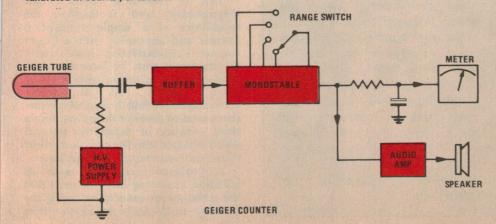
As mentioned before, Geiger counters were the major instrument in use in early uranium exploration and while other detectors are now available, the Geiger counter still has a place in preliminary exploration and radiation monitoring. A Geiger tube consists of a hollow metallic cylinder with a centrallylocated wire inside. The whole system is either sealed in a glass cylinder or the outer metal tube is used as the sealed chamber with appropriate end insulation. The cylinder is evacuated and filled with a gas such as helium, argon or neon, plus a small percentage of an organic or halogen gas as a 'quenching' agent.

A high voltage is applied between the central wire and the outer tube, so that when a gamma ray enters it, the gas filling ionises and causes a discharge.

The discharge is quickly quenched or extinguished by the quenching agent, resulting in a relatively large current pulse through the tube that can be easily measured. The gamma rays must be stopped completely for a discharge to occur, which results in a very low conversion efficiency for Geiger tubes of only 1%, as only one in each hundred rays is completely stopped. This insensitivity can be useful however, as the Geiger counter can be used in areas of very high radioactivity without the count rate becoming excessive.

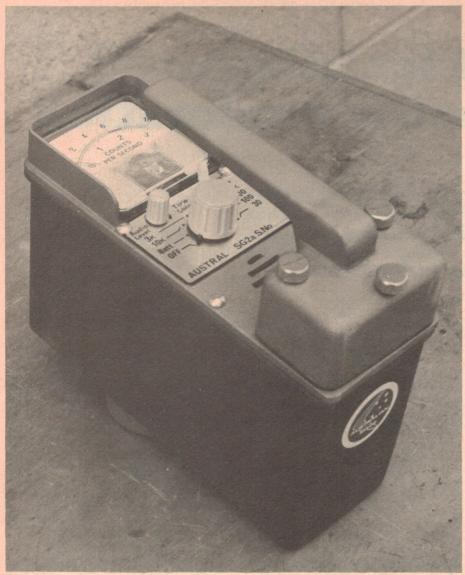
The Geiger counter circuitry shown in the accompanying block diagram is quite simple using a monostable to give a constant width to the pulses, which are averaged over several seconds so that the count rate is proportional to the average dc level. The range switch can change the monostable width, or the meter resistor, or both, to get the correct division ratios. To maintain accuracy with this system, it is important to keep a constant pulse height and stable pulse width. Although the high voltage supply can be very low powered, it is important to keep the output voltage stabilised and within the admissible operating voltage range (known as the counting plateau).

Block diagram of a typical commercial Geiger counter. The monostable has provision for selecting preset pulse widths ('RANGE') for differing count rates, depending on the level of radioactivity being measured. The monostable output is differentiated by a CR network and drives a meter calibrated in counts per second.



#### Scintillation counters

Scintillation detectors are the basis for almost all modern radiometric exploration instruments. As with the Geiger tube, the principal of operation is quite simple. However, the method by which the electrical pulses are produced is



A typical scintillation counter manufactured and marketed in Australia. This model has selectable ranges and an audio output as well as a meter indicating counts per second.

#### THE BASICS

Uranium exploration is based on the measurement of naturally occurring radioactive elements. All igneous and sedimentary rocks contain variable amounts of the three main naturally occurring radioactive elements, uranium, thorium and potassium. The average concentration of these elements is only 0.1 – 10 parts per million, while uranium ore may have a concentration of several percent.

An element is considered to be radioactive when the atoms of which it is made disintegrate

spontaneously, causing it to decay and form new elements known as daughter products. As it decays it may emit several types of radiation, however the one of interest to us is gamma radiation. Gamma rays have no mass, no charge, and can be regarded as highly penetrating electromagnetic radiation. The measuring device must therefore have a detector for converting these gamma rays into electrical pulses which can be counted for a fixed time period, or averaged as in a car tachometer.

completely different. The detector assembly consists of a scintillation crystal which is optically coupled to a photomultiplier tube. The crystal is usually made of thallium-activated sodium iodide which has the property of emitting a small flash of light (scintillation), when a gamma ray is stopped in it. The photomultiplier tube is a light amplifier which gives out an accurate, amplified reproduction of the light flash in the crystal, in the form of a short electrical pulse (approx. 2 us).

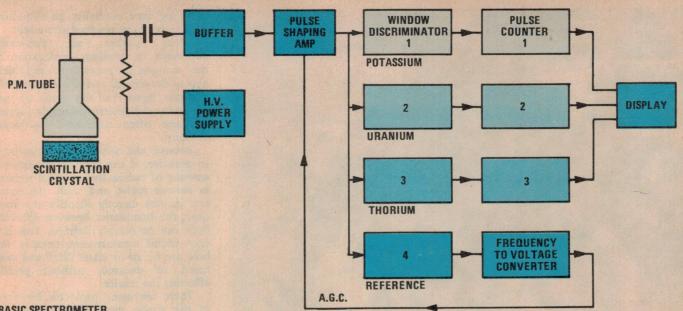
The great advantage of this rather indirect method of detection is in its efficiency, which approaches one hundred percent. Special protection is needed for scintillation crystals and photomultiplier tubes, which results in an instrument which is less rugged, more expensive, but far more sensitive than a Geiger counter. The circuitry of a simple scintillation counter is very similar to a Geiger counter, but usually with extra ranges for the higher count rates.

### Radiometric ground surveying

In the search for unknown uranium deposits the ground is traversed on a regular grid, noting the readings at set intervals. The chance of finding an outcrop on the surface is very low, so it is important to note any change in the normal background radiation level, as even a metre or so of soil may have a considerable masking effect. If an area of high radioactivity is located, it would be very premature to stake a claim at this stage. Firstly, the material may be thorium, potassium, or uranium or a combination of them. These can be distinguished from each other because the radiation they produce has characteristic energy levels, resulting in different height pulses from the photomultiplier tube. By counting only three narrow ranges of pulse heights, the ratio of the three radioactive elements can be determined.

This is known as 'pulse height spectrometry' and is beyond the capabilities of a simple scintillation counter and impossible with a Geiger counter. The scintillation crystal used in spectrometers must be large to obtain good results, and the circuitry must be highly stable and temperature compensated. A fourth channel is sometimes used to monitor the pulses from a small quantity of radioactive material which is doped into the crystal, to allow automatic temperature compensation.

A problem encountered with all radiation measuring instruments is that the emissions are random, requiring the circuitry to be ready to accept pulses



**BASIC SPECTROMETER** 

separated by only a few microseconds when the average time between pulses may be 100 milliseconds. It is clear then that a simple monostable system would not be suitable, and pulse height spectrometers must employ pulse sophisticated shaping and counting circuits to minimise these problems.

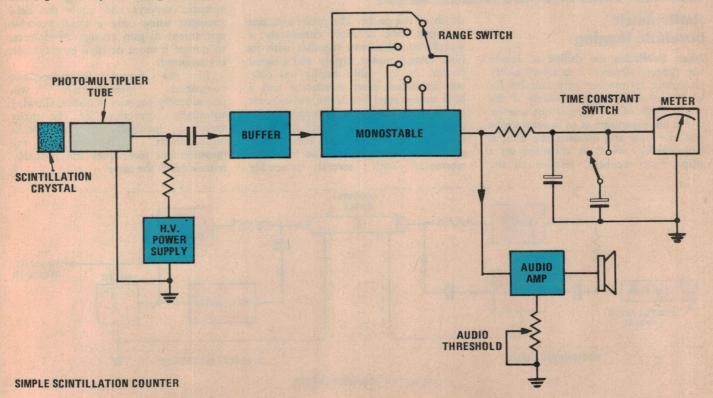
Even spectrometers cannot always determine the usefulness of a deposit, as leaching and weathering can remove the original uranium, leaving only the radioactive daughter products behind.

In conclusion, it can be seen that finding naturally occurring radioactive material is relatively simple, but finding out exactly what you have found is considerably more difficult!

#### Airborne radiometric surveying

Airborne radiometric surveys have been carried out for many years but even using the latest airborne spectrometers, the results can only be used as a guide. The plane must fly on regular grid lines recording the quantities of uranium, potassium and thorium, as well as the total radiation, on strip chart recorders or magnetic tape. The readings are used to produce radiometric contour maps on which the 'peaks' indicate areas of high radioactivity, known as anomalies. However the size and intensity of the anomaly cannot directly determine the actual extent of the deposit, due mainly to the masking effect of any overlying material. Problems also arise with pockets of airborne natural radon gas, uneven terrain, cosmic radiation and temperature changes.

The results then, are mainly used to eliminate areas which have very few anomalies, and to give a starting point for follow up ground surveys, or borehole drilling.





A portable radiometric borehole logger. The logging cable, which conducts power to the head and signals back, is wound off the drum at the rear of the instrument.

### Radiometric borehole logging

When boreholes are drilled to locate any type of deposit, it is a very costly procedure to recover core samples for laboratory analysis, particularly if the exact depth of the seam is not known. The usual procedure is to lower a probe into the hole and measure the natural radioactivity, which is recorded on a strip chart recorder, relative to the

depth of the probe. The probe contains a Geiger tube or more commonly, a scintillation detector, together with its high voltage power supply and a signal buffer. As the cable usually has only one insulated inner conductor and a high tensile steel braid, the pulses must be coupled on to the dc supply to the probe and then picked off across an inductor at the surface. The surface electronics consists of an accurate ratemeter with several selectable

averaging time constants, to allow low count rates to be resolved accurately.

These probes are extremely important in uranium exploration as they can give the exact depth and thickness of the deposit and also a reasonably accurate figure for the grade of ore. However, radiometric borehole logging is quite often not used to locate uranium.

Because the scintillation detector is so sensitive, it can measure the minute amount of radioactive material present in various rocks, and while the count rate cannot directly identify the rock type, the boundaries between different beds can be sharply defined. This is a very useful measurement because the hole can be air or water filled and steel cased or uncased, without greatly affecting the results.

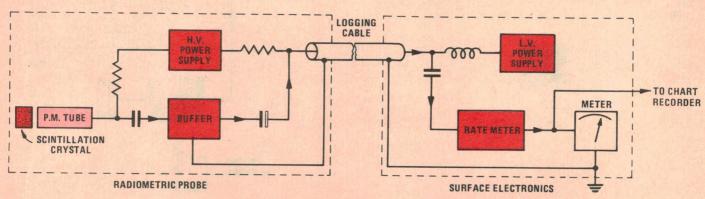
There are some problems however, as the probe must be watertight to depths of 1000 m or more and able to withstand the pressure at that depth. It must also be rugged and have a wide operating temperature range. This is an extremely harsh environment for sensitive electronic equipment, and careful design is essential.

#### Summary

Modern electronics and refined measurement techniques have greatly assisted uranium exploration and has led to radiometric borehole logging being accepted as a tool for exploration in general.

Spectrometer-type instruments have eliminated many errors in ground and airborne surveys and allow the field geologist using only a small portable instrument to gain enough information to decide if more detailed investigation is warranted.

In the future, microprocessor controlled spectrometers will undoubtedly become available, allowing automatic correction for the many variables involved in radiometric measurement. However, the measurement techniques will probably remain much the same.



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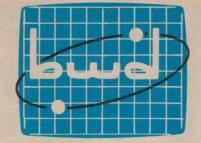
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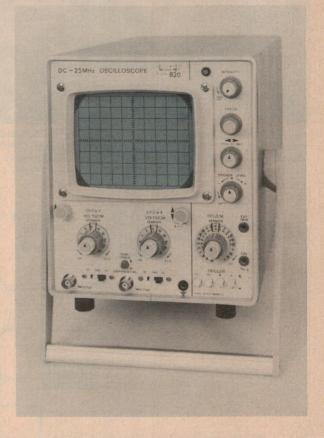
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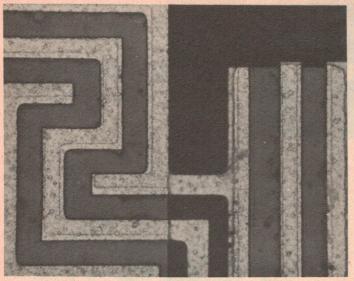
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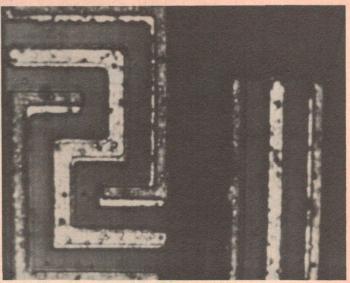
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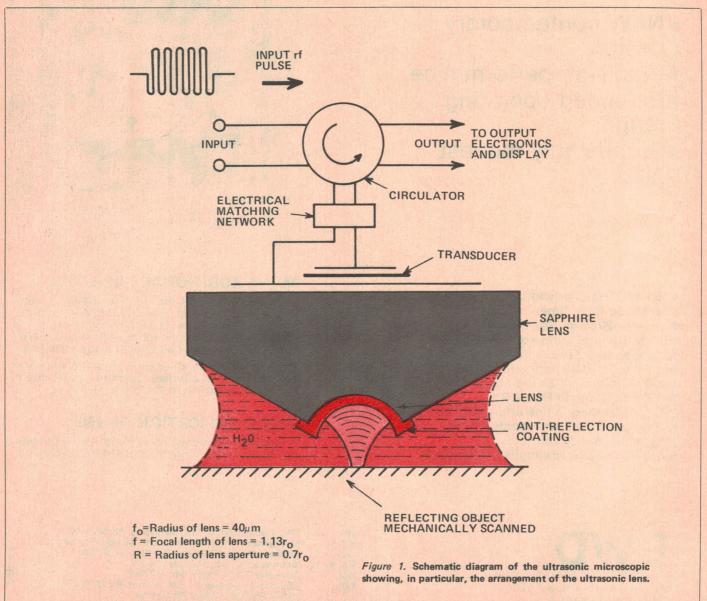
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Optical (left) and ultrasonic (right) comparison of a CMOS integrated circuit that uses silicon-on-saphire (SOS) technology showing the greater resolution of blemishes brought out by the ultrasonic micro-



scope. (Pictures courtesy Professor C.F. Quate, Stanford University, USA).



# Ultrasonic microscope can look inside transistors

#### **Brian Dance**

Research in the US has led to the development of an ultrasonic imaging technique that provides resolution comparable to that of the best optical microscopes using ultrasonic pulses at a frequency of 3 GHz!

WHEN ONE REFERS to ultrasonic frequencies, one may first think of frequencies of perhaps 25 kHz to 100 kHz which bats use for navigation and which can be used in simple ultrasonic remote control applications. Higher frequencies of about 1 MHz to 10 MHz cannot travel more than a very short distance through air, but are widely used in the medical field. Recently, however, Professor C.F. Quate of Stanford University, USA has employed ultrasonic waves with a frequency of about 3 GHz to make a scanning ultrasonic microscope which can form images of small objects with a resolution similar to that obtainable from optical microscopes. In some cases better contrast is obtainable with the ultrasonic microscope and further improvements in resolution expected.

#### Wavelength

The resolution of any form of microscope is limited by the wavelength of the radiation used to view the objects. For this reason ultra-violet radiation can be used in a suitable microscope to provide better resolution than visible light, but a much greater improvement can be made by the use of an electron microscope, since electrons have a much smaller wavelength.

A 1 kHz sound wave in air has a wavelength of the order of 300 mm and can be used only for imaging fairly large objects, whereas a 3 MHz ultrasonic wave in a liquid has a wavelength of a fraction of a millimetre and can therefore be used in medicine and industrial applications for imaging fairly small objects. However, the 3 GHz ultrasonic waves used by Professor Quate have a wavelength of only 520 nm in the medium used which is water heated to 60°C where the velocity of sound is 1.55 km/second.

This wavelength of 520 nm is somewhat less than the wavelength of visible light at the centre of the visible spectrum (green light of 550 nm wavelength). The 3 GHz ultrasonic waves can therefore produce images with a resolution comparable to those of the best optical microscopes utilizing green light. This is three times better than the images produced by any earlier acoustic microscope. It is expected that the next generation of ultrasonic acoustic microscopes will produce better resolution than the best optical microscope.

#### Construction

The ultrasonic microscope used by Professor Quate has the structure shown in Figure 1. It includes a single surface spherical lens ground into a sapphire block; sapphire is aluminium oxide, A1<sub>2</sub>O<sub>3</sub>. The black surface of the sapphire contains a piezoelectric transducer on the axis of the lens. The front surface of the lens is coated with a layer of glass one quarter of a wavelength in thickness which acts as an antireflective coating between the

mechanically rigid sapphire and the hot water at 60°C beneath the lens.

The transducer is fed with 3 GHz radio frequency pulses of 20 ns duration. The ultrasonic pulses produced by the transducer travel through the sapphire and water to converge at a point on the object under examination. After they have penetrated the object, the ultrasonic waves are reflected back through the water and sapphire to a zinc oxide film on the back of the sapphire. This transducer film converts the ultrasonic waves back into electrical impulses. The reflected pulse containing the required information is separated from the input pulse and any spurious reflections are combined with timegating circuits by means of a circulator.

The velocity of sound waves through the warm water is 1.55 km/second, but their velocity in sapphire is 11.1 km/second. It is this great difference in velocity which enables a high resolution focus to be obtained in the acoustic microscope using a single surface lens. The distortion of the beam caused by spherical aberration is inversely

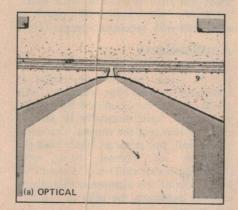




Figure 2. The high resolution obtained with the ultrasonic microscope is well illustrated in the photograph on the right. This shows the internal structure of a Hewlett-Packard FET whose gate length is only 500 nanometers! A photograph taken with a conventional optical microscope is shown, for comparison, on the left.

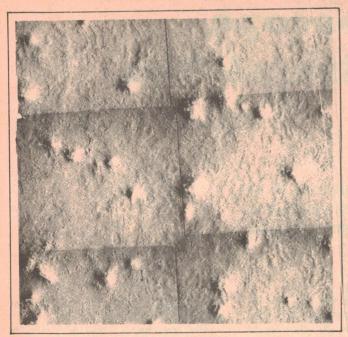
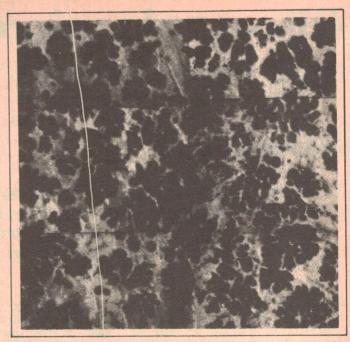


Figure 3. The surface of a cobalt-titanium alloy as seen under an optical microscope is shown on the left, whilst the ultrasonic microscope



photograph on the right shows the distribution of the elements within the alloy.

proportional to the square of the velocity ratio and with such a high velocity ratio is negligible. The high value of the velocity ratio results in a large angle of refraction at the lens/liquid interface, so the waves leave the lens close to the normal and converge to a focus which is only marginally greater in size than the radius of the lens.

The object is moved very rapidly to and fro by a separate oscillator whilst it is under the sharply focused ultrasonic beam. This results in the object being scanned by the beam as it moves backwards and forwards in much the same way as a television camera scans a scene. The output from the zinc oxide film transducer is amplified and used to form the image of the object on a television screen.

The formation of the image by acoustic microscopy depends on the mechanical and structural properties of the specimen. The density, elasticity and viscosity of the object under examination affect the ultrasonic waves which enable images to be formed of the inter-faces between layers of different rigidity.

Frequency

We have already seen that it is important to use very high frequency ultrasonic waves, since the higher the frequency the shorter the wavelength and the better the resolution or image sharpness which can theoretically be obtained. However, there is a fundamental upper limit on the maximum frequency which can be used, since with increasing frequency

there is increasing absorption of the ultrasonic waves. This absorption increases with the square of the frequency over a frequency range from some kilohertz to about 10 GHz and perhaps even higher frequencies. Calculations show that water heated to about 60°C is considerably better than at room temperature.

Considerable thought is being given to the use of liquids other than water as the coupling medium in which the specimen under examination is placed. Although it may be possible to use a different liquid for higher frequencies in order to obtain better resolution, it is not possible to place all types of specimen in some of the liquids which are theoretically capable of giving the best results. Carbon disulphide, liquid helium and mercury are liquids in which one might expect to obtain better resolution than is possible with water, but each of these has its own problems associated with specimen compatibility.

#### **Applications**

Applications of the new microscope are said to range from can cer studies to metallurgical uses. For example, cells which are to be examined by optical microscopy must normally be stained and this damages the normal chemistry of the cell, but it seems likely that the behaviour of normal living cells (including cancer cells) can be examined by the use of the ultrasonic microscope without damaging the cells in any way whatsoever.

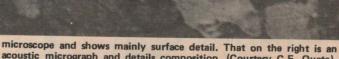
The ultrasonic microscope has been much used to examine very thin layers of materials, since it can reveal subsurface features and imperfections under the surface which cannot be seen using an optical microscope. The instrument can be used to reveal stresses in materials, structural fatigue and subsurface corrosion which could be a valuable testing technique in quality control inspections, etc.

One type of specimen with a very thin surface layer which has been examined with the ultrasonic microscope is the integrated circuit chip. It is interesting to compare the optical and ultrasonic images of such chips. The conventional optical microscope normally shows the aluminiun or other metallisation very clearly with sharp edges, whereas the ultrasonic microscope shows some of the structures beneath the aluminium. Light or dark areas of the ultrasonic image correspond to such sub-surface structures and indicate, for example, the points where emitter or other contacts have been made on the chip. In some cases it is best to alter the position of the object slightly relative to the sapphire lens system so that the focus is beneath the surface; this renders the aluminium metallisation slightly out of focus, but enables better images of the sub-surface lavers to be obtained.

The use of an ultrasonic microscope to view sub-surface layers which are invisible with an optical microscope is of considerable practical importance, since many of the defects in semiconductor devices occur in the underlying layers. It seems likely that the ability to view such layers without destroying the device will greatly assist our understanding of the practical



sample of low alloy steel. The picture at left comes from an optical effects of such defects and perhaps



acoustic micrograph and details composition. (Courtesy C.F. Quate).

enable the proportion of satisfactory devices coming off a production line to be increased; resulting in more economical devices.

#### Conclusions

Acoustic microscopes have been used for some years at Hughes Research Laboratories in California and elsewhere to examine integrated circuits, but the frequency used has been some hundreds of MHz. It is only very recently that Professor Quate's work has enabled GHz frequencies to be employed with a great improvement in the resolution obtainable. Apart from the increased frequency of operation, other improve-

ments associated with the use of hot water, a reduction in the lens size (which results in less ultrasonic wave attenuation) and a carefully designed lens system have greatly improved ultrasonic microscopical techniques.

Work is now commencing on image enhancement by storing the reflected signals on a floppy disc and performing Fourier transform analysis with a Z-80 based Cromemco processing system. The ultrasonic pulses fed to the transducer are generated with bipolar transistors, but the use of field effect transistors is being investigated for use with pulses shorter than 10 ns.

Professor Quate's work has enabled the optimum resolution to be improved

by a factor of two each year over a period of four years. At the present time integrated circuits with known electrical defects are being examined with the ultrasonic microscope to see if any correlation is present between the electrical defects and the ultrasonic images.

If the ultrasonic microscope is put into production commercially, Professor Quate has estimated that its cost would be of the order of US\$25 000 dollars

For further information refer to V. Jipson and C.F. Quate, Acoustic Microscopy at Optical Wavelengths, Appl. Phys. Lett, 32, (12), 789-791, 15 June 1978.

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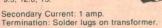
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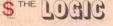
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# World's first electronic credit card

A NEW electronic credit card, developed in Italy for use as a pre-paid telephone card, is likely to have many uses. One of Europe's major semiconductor manufacturers, SGS-ATES of Milan, has developed a unique type of low cost electronic credit card in conjunction with the Italian telephone authority SIP (Societa Italiana per l'Esercizio Telefonico) Known as the XCARD, it contains a 17 x 8 bit non-volatile memory in a low-cost plastic package similar to a conventional credit card. Most of the 136 bit memory is used for storing the number of credit units, but 36 bits are used for security, control and testing.

The system will work in the following way. When the consumer buys the card initially, all of the memory cells are erased and this represents 100 credit units. Each time the card is used, the payphone (or other point of sale concerned) writes into a certain number of the cells according to the cost of the call. When no more erased memory cells are left, an attempt to use the card will result in no service being obtained; the card is then thrown away.

Fraudulent misuse of these cards is prevented through 100% testing by the security code incorporated in the memory and by a plastic tab which must be removed before the card can be inserted into the card reader. This tab prevents the re-sale of used cards.

The security code in the memory identifies the vendor of the card. If any attempt is made to erase the memory so as to restore credit in a used card, the security memory will also be erased and this will render the card useless.

It is claimed that the XCARD system will benefit both consumer and the vendor. The consumer will benefit by not having to carry loose change and it seems likely that less vandalism will occur in telephone booths using the new system, since no cash will be contained in the telephone equipment. Payment in advance will benefit the telephone company or other card vendor, whilst the high immunity against fraud and reduced maintenance will also be beneficial to the company.

It seems likely that the XCARD will be employed not only in payphones, but in many other types of low-cost



automatic machines which are frequently used.

#### M274 chip

The SGS-ATES M274 programmable memory is incorporated in the XCARD, but can also be supplied in a 14-pin dual-in-line package which has seven connections. The EPROM contains an 8-bit word which is used as the security key to detect erasure, for example, by X-rays or by radioactive sources. One row of the memory matrix holds a mask programmable 8-bit code which can identify up to 256 different users. The non-volatile memory has been designed to retain data for at least one hundred years.

After the security word is written into the memory during manufacture, the writing circuits to this row of the

The 'electronic credit card' produced by SGS-ATES of Milan. They will be used with pre-paid telephones. It contains a 136-bit non-volatile memory arranged in a 17 x 8 bit configuration.

memory are destroyed by blowing an on-chip fuse; it is not possible to repair this fuse. Each telephone or service point is designed to check the XCARD for a valid security key before it provides any service.

When the XCARD is inserted in the reader at the point of sale, a seven pin connector makes electrical contact with the point of sale equipment. The voltage applied to the memory in the XCARD is within the range of 9 to 11V. Writing a bit in a memory cell is effected by the application of a single pulse of +25V, 10mA with a duration of 50ms.

The use of cards of this type for charging for parking instead of coin operated meters which can be subject to theft seems very likely. Indeed, trials of coin-less parking meters are being arranged in London in the near future.



#### JUST WRAP'"WIRE WRAPPING TOOL

WHY CUT? WHY STRIP? WHY SLIT? WHY NOT JUST WRAP?

JW-1-B	BLUE WIRE
JW-1-W	WHITE WIRE
JW-1-Y	YELLOW WIRE
JW-1-R	RED WIRE





#### JUST WRAP REPLACEMENT ROLLS

	R-JW-B	BLUE WIRE	50 ft. Roll
	R-JW-W	WHITE WIRE	50 ft. Roll
	R-JW-Y	YELLOW WIRE	50 ft. Roll
2	R-JW-R	RED WIRE	50 ft. Roll



#### UNWRAP TOOL FOR JUST WRAP

JUW-1 UNWRAPPING TOOL



#### JUST WRAP KIT

JWK-6 JUST WRAP KIT



#### "HOBBY" WIRE WRAPPING TOOL BATTERY POWERED

BW-2630	FOR AWG 26-30	
Use "C" size not included.	NICAD Batteries, not included.	Bits

BIT FOR AWG 30 BIT FOR AWG 26-28 BT-2628





#### HOBBY WRAP TOOLS



WSU-30 | REGULAR WRAP WSU-30M MODIFIED WRAP



#### PRE-STRIPPED WIRE WRAPPING WIRE

AWG-30 (0.25mm) KYNAR\* wire, 50 wires per package stripped 1" both ends

	30-W-50-010	30-AWG White Wire, 1" Long
	30-R-50-010	30-AWG Red Wire, 1" Long
	30-B 50-020	30-AWG Blue Wire, 2" Long
	30-Y-50-020	30-AWG Yellow Wire, 2" Long
	30-W-50-020	30-AWG White Wire, 2" Long
	30-R-50-020	30-AWG Red Wire. 2" Long
	30-B-50-030	30-AWG Blue Wire, 3" Long
	30-Y-50-030	30-AWG Yellow Wire. 3" Long
	30-W-50-030	30-AWG White Wire, 3" Long
	30-R-50-030	30-AWG Red Wire: 3" Long
	30-B-50-040	30-AWG Blue Wire, 4" Long
	30-Y-50-040	30-AWG Yellow Wire, 4" Long
	30-W-50-040	30-AWG White Wire, 4" Long
	30-R-50-040	30-AWG Red Wire, 4" Long
	30-B-50-050	30-AWG Blue Wire, 5" Long
8	30 Y 50 050	30-AWG Yellow Wire, 5" Long
	30-W-50-050	30-AWG White Wire, 5" Long
	30-R-50-050	30-AWG Red Wire, 5" Long
	30-B-50-060	30-AWG Blue Wire, 6" Long
16	30-Y-50-060	30-AWG Yellow Wire, 6" Long
	30-W-50-060	30-AWG White Wire, 6" Long
13	30-R-50-060	30-AWG Red Wire. 6" Long
23		



#### TRI-COLOR DISPENSER

WD-30-TRI	TRI-COLOR DISPENSER
R-30-TRI	REPLACEMENT ROLLS

#### WIRE DISPENSER

WD-30-B	BLUE WIRE
WD-30-Y	YELLOW WIRE
WD-30-W	WHITE WIRE
WD-30-R	RED WIRE

#### DISPENSER REPLACEMENT ROLLS

		30-AWG BLUE 50 FT. ROLL
	R-30Y-0050	30-AWG YELLOW50FT.ROLL
1	R-30W-0050	30-AWG WHITE 50 FT. ROLL
-	R-30R-0050	30-AWG RED 50 FT. ROLL





HK-18	18 AWG	25 FT.	SOLID CONDUCTOR
HK-20	20 AWG	25 FT.	SOLID CONDUCTOR
HK-22	22 AWG	50 FT.	SOLID CONDUCTOR
HK-24	24 AWG	50 FT.	SOLID CONDUCTOR
HK-26	26 AWG	50 FT.	SOLID CONDUCTOR
SHK-18	18 AWG	25 FT.	STRANDED CONDUCTOR
SHK-20	20 AWG	25 FT	STRANDED CONDUCTOR
SHK-22	22 AWG	50 FT.	STRANDED CONDUCTOR
SHK-24	24 AWG	50 FT.	STRANDED CONDUCTOR
CHK 26	26 AWG	50 FT	STRANDED CONDUCTOR

#### PRB-1 DIGITAL LOGIC PROBE

- DC to > 50 MHZ
   10 Nsec, pulse response
   120 K 12 impedance
   Automatic pulse attething to 50 Msac.
   Automatic resetting memory
   Open circuit detection
   Open circuit detection

PRB-1 DIGITAL LOGIC PROBE



#### PROTOTYPE BOARD (M-100

TERMINALS: 1,020 TEST POINTS. 188 separate 5 point terminals, plus 2 horizontal bus lines of 40 common test points each.

SIZE: 61/2" Wide, 5" Long.

CM-100 MODULAR PROTOTYPE BOARD



#### PROTOTYPE BORRD (M-200

TERMINALS: 630 TEST POINTS. 94 separate 5 point terminals, plus 4 bus lines of 40 common test points each. SIZE: 6" Wide, 3½" Long.

CM-200 MODULAR PROTOTYPE BOARD



CM-400

1

CM-300

#### PROTOTYPE BOARD (M-300, CM-400

CM-300 and CM-400 have two separated rows of five interconnected contacts each. Each pin of a DIP inserted in the strip will have four additional tie-points per pin to insert connecting wires. They accept leads and components up to .032 in. diameter. Interconnections are readily made with RW-50 Jumper Wire. All contact sockets are on a .100 in. square grid (156 in wide)

CM-300 MODULAR PROTOTYPE BOARD CM-400 MODULAR PROTOTYPE BOARD



CM-500 is a bus strip to be used in conjunction with CM-300 and CM-400 for distribution of power and common signed lines. Two separate rows of common terminals, grouped into clusters of five. All contact sockets are on a .100 in. square grid.

CM-500

MODULAR BUS STRIP



CM-500

#### DIP IC INSERTION TOOLS WITH PIN STRAIGHTNER

Narrow profile. Pin straightener built into tool. Automatic ejector.

INS-1416

14-16 PIN DIP/IC INSERTER

#### mos, cmos-safe

GROUND STRAP NOT INCLUDED

14-16 PIN, MOS CMOS SAFE INSERTER MOS-1416 MOS-2428 CMOS SAFE INSERTER



#### 36-40 PIN CMOS-SAFE IC INSERTION TOOL

Aligns bent out pins. Includes terminal lug for attachment of ground strap.

GROUND STRAP NOT INCLUDED 36-40 PIN CMOS SAFE INSERTION TOOL



#### DIP IC EXTRACTOR TOOL

Extracts all LSI, MSI and SSI devices of from 8 to 24 pins.

EXTRACTOR TOOL EX-1



#### 24-40 CMOS-SAFE EXTRACTOR TOOL

Removes 24-40 pin IC's, .600" centers. C-MOS safe. Includes terminal lug for attachment of ground strap.

GROUND STRAP NOT INCLUDED

EX-2 CMOS SAFE EXTRACTOR TOOL

AMPEC ENGINEERING CO. PTY. LTD. 1 Wellington Street, Rozelle, 2039. Tel. (02) 818-1166. Available from: NSW David Reid Electronics, 29-6601. Radio Despatch Service, 211-0191. Electronics (Distributors), 636-6052. Martin De Launay, 29-5834. Applied Technology, 487-271, Vic. Radio Parts, 329-7888. Stewart Electronics, 534-3733. Arlin Instruments 569-6984. Ellistronics, 602-3282. S. Aust. Protronics, 212-3111. W. Aust. Reserve Electronics, 328-3116. Qld. Wilber Sales, 391-5136.

# "The Rocker" — 140W of rich, warm valve sound!

We have had so many requests for a valve power amplifier in the last year or so, from readers and project suppliers alike, that we finally succumbed. Turn back the clock, heat up your 100 watt iron and read on . . .

Phil Wait Ron Keeley

FASHIONS CHANGE, styles come and go, but some things remain the same ... one of the constants is the preference of many musicians for the warm, deep-throated sound of an old-fashioned valve amplifier.

The "valve vs transistor" argument may never be settled conclusively. Despite all the obvious advantages of solid-state, musicians prefer valves because, they say, valve amps simply sound 'better', subjectively — like the preference of some people for an old Harley-Davidson or Triumph motorbike, rather than a modern, high-revving performance machine. On the other hand, there are definite technical reasons why a valve amp will sound 'different'.

The reason most often advanced is that valves produce predominantly second harmonic distortion, whereas transistor amp distortion is mainly third harmonic. While this is true, it is not the whole truth; the distinctive sound of valves is caused by the synergy of many factors, and the spectral balance of the distortion components is just one of them. Other important factors are the shape of the distortion/power curve, the that valve amps transformer-coupled to the load (which affects the overall response of the amp), the high output impedance of valve amps (resulting in reduced damping of the loudspeaker and a more 'colourful' sound), and the higher 'dynamic output' capability of valve amps (the ability to deliver relatively constant power to a varying load, i.e. a speaker).

If all these factors could be built into a transistor amp, then possibly it would sound, subjectively, like a valve amp. Many have tried to do this — most have failed. We've taken the opposite approach, and built a good, old-fashioned, high power valve amplifier, the "Rocker'.

#### Circuit design

This amplifier circuit is the result of many hours of experimentation and

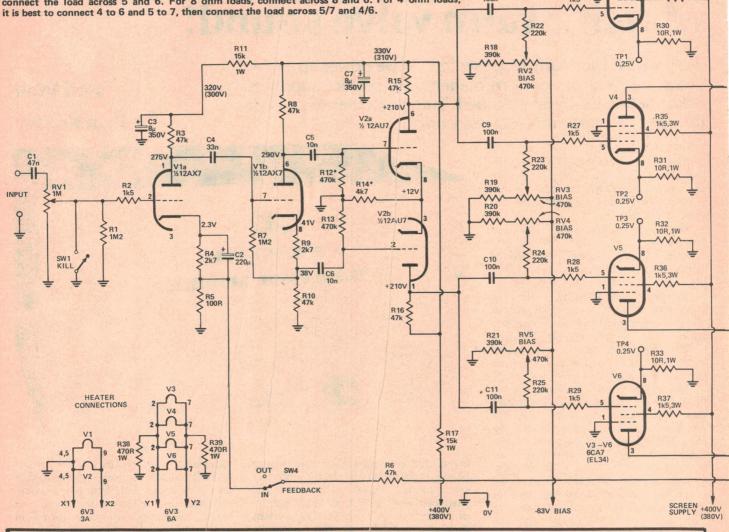


incorporates suggestions from many people, staff and friends of both ETI and sister magazine Sonics, and particularly John Burnett of the School of Electronics, whose suggestions prompted quite a few changes, especially around the input stage. Overall, the circuit uses a triode voltage amplifier stage followed by a phase splitter, a pair of drivers and the output stage, consisting of four valves in push-pull-parallel. The amplifier is

SPECIFICATIONS OF PROTOTYPE — ETI 456 VALVE AMPLIFIER  Power Bandwidth - 1 dB - 3 dB  140 watts 22 Hz to 12 kHz 18 Hz to 17 kHz  50 watts 18 Hz to 22 kHz 14 Hz to 27 kHz						
Distortion at 1 kHz  100 mW 5 watts 50 watts 100 watts 140 watts						
open loop:	1%	0.7%	1.9%	3%	15%	
closed loop:	0.4%	0.22%	0.65%	1%	5%	
Power output for 140 watts (8 ohr Maximum power 200 watts (8 ohr		with fee	ensitivity edback:	200 mV (adjustable) 80 mV		
Hum and Noise - 62 dB with respect to 140 watts output				ck Ratio:		

NOTES: Various voltage readings are given on this drawing as a guide to constructors, but note that they may vary 10 - 20%. Unbracketed readings were taken with no signal present. Bracketed readings were taken with the unit operated at full power output.

Terminal 6 of the output transformer, T1, must be grounded. A total of five output terminals will be needed to obtain the various combinations possible. For 16 ohm loads, join 7 to 4 and connect the load across 5 and 6. For 8 ohm loads, connect across 8 and 6. For 4 ohm loads,



The amplifier has four separate stages: the input voltage amplifier, a phase-splitter, a push-pull driver stage and a push-pull power output stage.

The input stage, V1a, uses one section of a 12AX7 of a high-u twin triode. The input enters via a dc-isolating capacitor, C1, and the gain control, RV1. The 'grid stopper' resistance,R2, is placed directly in series with the grid to reduce susceptibility to RF interference.

The phase-splitter uses the other half of V1 (V1b), its grid being coupled to the anode of the input stage by C4. This stage has no gain. The signal at the grid of V1b appears at the anode inverted, i.e.: 180 out of phase. The signal also appears at the junction of the cathode bias resistors R9 and R10, in the same phase. Thus, the signals coupled to the pushpull driver stage via C5 and C6 are 180 out of phase. Grid bias for the phase-splitter is obtained by returning the grid resistor, IR7, to the junction of the cathode bias resistors, R9 and R10, effectively placing the grid at about -3 V with respect to the cathode.

The driver stage consists of a 12AU7 low-u twin triode. Resistor R14 provides cornmon cathode bias, while R12 and R13 are the two

#### HOW IT WORKS — ETI 456

grid returns. The anode supply for this stage comes from the 400 V supply (screen voltage supply for the output stage) via a decoupling network consisting of R17 and C7. Each driver (V2a and V2b) has a gain of 10, defined by the ratio of R15 to R14 and R16 to R14.

The output stage consilsts of four valves in a push-pull parallel arrangement. V3 and V4 are in parallel and V5 and V6 are in parallel, the two pairs connected in push-pull via the output transformer. The anode of V2a drives the grid circuits of V3-V4 while the anode of V2b drives the grid circuits of V5-V/6. The output stage is operated in class AB, which affords good gain, low distortion and good power output.

Bias for output stage is provided from a common bias supply from the power transformer, the bias for each valve being individually adjusted. As the characteristics of the 6CA7 output valves can vary widely, this adjustment is provided to ensure proper operation from unit to unit.

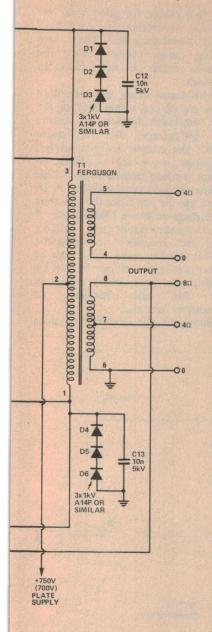
The output transformer matches the plateto-plate impedance of the push-pull output pairs, about 5500 ohms, to the low impedance speaker load. Several output windings are provided: a single 4 ohm winding and an 8 ohm winding, tapped at 4 ohms. Feedback to the cathode of the input stage is taken from one end of the 8 ohm winding, the other end being grounded.

R34 1k5,3W

During each half cycle of the signal waveform, one 'side' of the output stage (i.e.: V3-V4 or V5-V6) will 'turn off'. This will allow that side of the output transformer primary to develop enough back emf to cause arcing across the valve socket pins. To prevent this, the reverse cycle emf is shunted via a set of diodes to ground — D1 — D3 and D4 — D5.

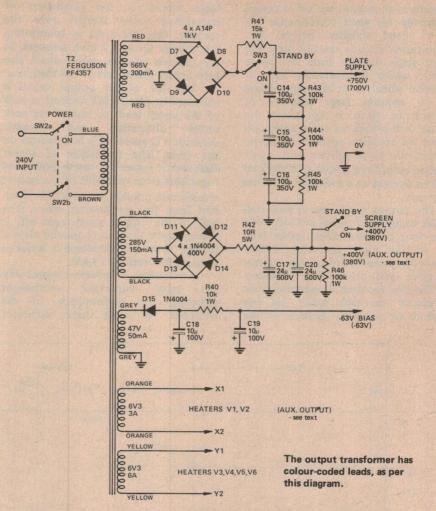
The power supply is fairly conventional. The power transformer has five secondary windings: one 6.3 V/3A heater winding, one 6.3 V/6A heater winding, one 47 V/50 mA bias winding, one 285 V/150 mA HT winding and one 565 V/300 mA HT winding.

Bridge rectifiers with capacitor-input filters are used to provide the appropriate HT voltages: 750 V for the output stage anodes, 400 V for the output stage screens and HT for the driver stages. A half-wave rectifier and pisection filter is used to derive the -63 V bias supply.



capable of driving four, eight or sixteen ohm loads, or two four ohm loads simultaneously.

Overall feedback is taken from the eight ohm winding of the output transformer to the cathode of the input stage, and is wired via a front panel switch, allowing the feedback to be switched out if desired. This will increase the impedance looking back into the output terminals, reducing the damping factor so that the speaker cone is more influenced by the back emf of the voice coil. Normally, hi-fi amps are designed to have very low output impedance — a high damping factor — to suppress the effect of the back emf and reduce the colouration which would otherwise be introduced by the speaker.



With the feedback in, the 'Rocker' is quite clean, and suitable for PA, bass guitar or even as a hi-fi amp; switching the feedback out, however, makes the amp that much 'dirtier' and will also give it a more 'live' sound. Other front panel controls are provided for the usual functions — power, standby and input gain. The 'kill' switch shorts the input to ground, and is an effective way of temporarily 'switching off' without generating any transients or unwanted thumps.

All inputs and outputs are mounted on the rear panel. Although we have used a phone-jack input socket and a single pair of binding post output terminals, there is sufficient room behind the chassis for Cannon/Switchcraft inputs and multiple binding post or phone jack outputs, if required.

At the input stage, we had a choice between a triode-pentode, such as the 6BL8, or a 12AX7 twin triode. Triodes have the disadvantage of large plate to grid capacitance which, together with the plate resistor and the voltage gain of the stage, introduces a phase shift at high frequencies, called the Miller Effect. The degree of phase shift depends on the capacitance, gain and value of the plate resistor. All phase shifts add through the amplifier, the first stage having the largest effect, and when feedback is applied from the output to the input, the amplifier may oscillate. The feedback ratio (and the possible reduction in distortion) is therefore limited by the phase change through the amplifier, and must be kept low if a triode is used in the input stage.

Our first design used a 6BL8 pentode which worked well with about 20 dB of feedback, allowing a good stability margin, and looked very promising. Then we started talking to people in the audio business who had experience with valve amplifiers, who all said that a triode-pentode tube was internally fragile and would fail after a few months on the road. Back to the 12AX7 then, and lower amounts of feedback to preserve stability.

We wanted the amplifier to be useful for hi-fi and bass guitar

### Project 456

applications as well, so we had to design it carefully for good performance but with a good stability margin, too. Conventional circuits usually drive the output stage directly from the phase splitter, which is inherently high in distortion when run at high signal levels and so requires large amounts of feedback to clean it up. Since the amount of feedback we could apply was limited by stability considerations, we followed the phase splitter with a pair of driver amplifiers, allowing the splitter stage to operate at a lower level for less distortion.

The output stages run in push-pull parallel using 6CA7 power pentodes. We chose four of these tubes, rather than two of the more powerful KT88s, because they are less than one quarter the price and are readily available.

The bias for class B operation is set individually on each tube; this was found to be necessary because of the

large spread in the parameters of unmatched tubes bought over the counter. The bias is set by monitoring the voltage across 10 ohm resistors, in the cathode of each valve, which also help reduce the effects of bad matching.

The life of the output valves is increased by placing lk5 resistors in each of the screen leads to reduce the peak dissipation, and parasitic oscillation is avoided by lk5 resistors on the grids. The possibility of socket flashover is reduced by using diodes and capacitors from each side of the output transformer primary to earth. The back emf from the transformer, when each half of the output stage turns off, is conveniently shunted to ground via the diodes. Three are connected in series to obtain a PIV rating of 3 kV.

The output transformer is probably most important component effecting the performance of the amplifier. It must have sufficient winding inductance for good bass, but low leakage inductance for good high frequency performance. These are conflicting requirements and the transformer must be well made to achieve both.

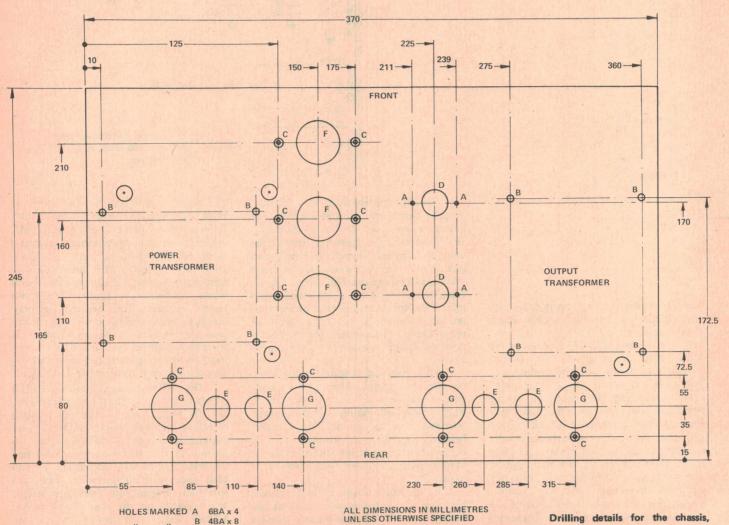
In this transformer, the secondary windings are placed either side of the primary, sandwich fashion, to reduce leakage inductance. For maximum flexibility, the output transformer has two separate secondary windings, an eight ohm winding tapped at four ohms and a separate four ohm winding. A 16 ohm load can be run from the two four ohm windings in series (linking pins 4 and 7, taking the output from 5 and 6), an eight ohm speaker is run from the eight ohm winding, and either one or two four ohm speakers can be run by connecting the four ohm windings in one speaker, for parallel independantly for two.

Throughout the circuit, the values

looking down from the top.

Refer to the picture on the page

opposite.



MATERIAL 1-1.5mm ALUM. OR STEEL

\* DRILL AND INSULATE TO SUIT FOR THROUGH WIRING FROM TRANSFORMER

4BA x 8 B

18mm x 2

9mm x 4

28mm x 3 30mm x 4

C

6BA x 14 or 3mm pop rivet

140w valve amp

of coupling capacitors have been kept as low as possible. If the capacitors are large and if the preceding stage is driven into clipping, there will be a time delay while they discharge, causing a short drop-out in the sound.

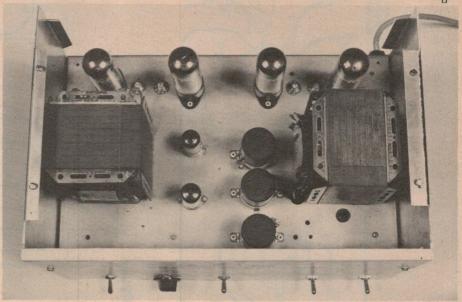
When you look at the power supply circuit, it may seem a little large. It is! It must be, to allow the amplifier to run into hard distortion, especially when used for bass guitar amplification.

The bias supply must be both free from ripple, and must reach its normal value immediately after turn on. If the power to the amplifier is momentarily interrupted (somebody tripping over a cord then quickly plugging it back in) the heaters in the tubes will still be hot; if the bias supply then takes time to come up to value, the output tubes will draw excessive current and may destroy themselves. The bias supply filter capacitors should be quite small and used with a fairly small value reistor in a pi-section filter to remove ripple. Regulation of the screen supply is ensured by using a separate transformer winding for the 400V (screen supply)

One of the heater lines should be earthed to reduce the risk of hum caused by heater to cathode leakage, but you will notice that the output stage heater lines are earthed through two 470 ohm resistors, rather than having one side connected directly to earth. Why? Imagine this: an output tube goes short circuit; the cathode resistor won't last long, and the tube will are over internally from cathode to heater, and then to earth through the heater line.

Now the output transformer has the full supply voltage across it and the current is limited only by the dc winding resistance, with the result that the output transformer burns up! The same thing will happen if a valve socket arcs over from pin 3 to pin 2. If resistors are placed from either side of the heater line to earth, however, they act as fuses protecting the output transformer while still preventing hum problems.

As in any amplifier, the mechanical design is just as important as the electrical. Looking at the layout, you will notice that the two transformers are the same size and are placed at either end of the chassis for correct weight distribution, and the four output valves are spaced along the back of the chassis for good ventilation - an important consideration to ensure them a long life. All power supply components are at the power transformer end of the chassis, while amplifier components are at the other. Bias controls are situated next to



Looking into the unit. WARNING: keep all the covers on in use as lethal voltages are present, The multimesh cover fits under the front panel lip and is secured by the PK screws at either side.

each output valve so that all wiring is short and direct.

#### Construction

Since most of the components are mounted either on the chassis or on the valve sockets, a pc board is of little advantage. The method we used requires some care in wiring, however, and careful cross checking with the circuit diagram to ensure you haven't made any mistakes! Remember that the unit has lethal voltages present and if you make a mistake you may not have the chance to make another.

As the amplifier will be a relatively expensive project, you may wish to save a few dollars by making your own

chassis. Hence we have produced a complete set of metalwork drawings. If you have the patience, the tools and the skill, quite a professional-looking unit can be produced. Many component suppliers sell sheets of aluminium, as well as useful things like hole-punch tool sets. Aluminium sheet and expanded aluminium may also be obtained from hardware stores, don't forget.

Examine the photos and the wiring diagrams and note carefully the positions of the components. The layout should be followed exactly, and all wiring should be of the highest standard. The power supply circuitry is located around the power transformer while the voltage



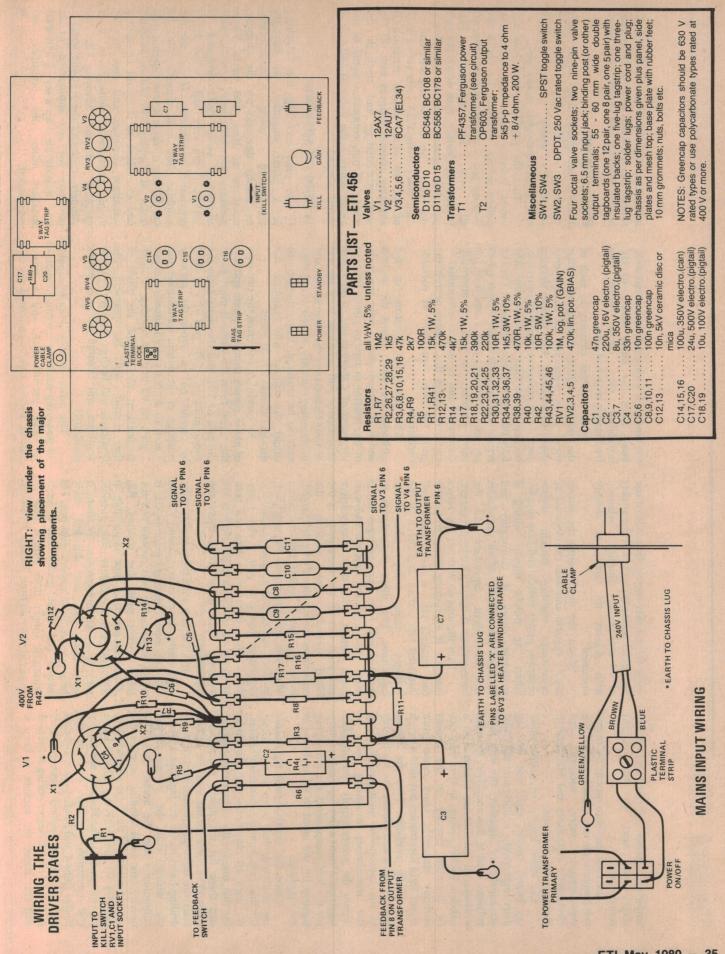
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amplifier, phase splitter and driver stages are next to the output transformer.

The first step is to mount the major components on the chassis. Locate the transformers, valve sockets, can electrolytic capacitors and bias pots in their correct positions.

be mounted directly on the chassis Cut three lengths of double-sided voltages used in this amplifier. We used wide-spaced bakelite tag boards with a without standoffs. Ours came from David Reid Electronics but similar types are widely available. Turn the chassis upside down and mount the tag boards in the appropriate positions. We used the transformer mounting bolts to mount the power supply and amplifier tagstrips. Mount a five-lug single tagstrip for the bias components and a three-lug tagstrip for the input to V1 as shown in tag board, twelve, eight and five tag pairs respectively, making sure the strips are capable of insulating the very high bakelite backing piece, so that they can the diagrams.

Once the tagstrips and tag boards are mounted, drill holes in the chassis We used 10 mm holes with grommets components and the heater lines. The heavier (six amp) winding supplies the supplies V1 and V2? the 12AX7 has a and the voltage applied between pins 9 and pins 4/5. All heater wiring is twisted and run above the sockets to keep it for the leads from the two transformers. for this, one for the output transformer, leads. (The holes for the leads are drilled drilling holes under the tagstrips!). Start the wiring with the power supply output tubes and the three amp winding 12 volt centre-tapped heater, and for six volt operation, the two ends of the heater (pins 4 and 5) are joined together and three for the power transformer after the tagstrips are mounted to avoid

away from other wiring. One side of the 3A heater wiring is earthed at the socket of V2 and the 6A winding is balanced with respect to earth, as already discussed.

Solder the diodes onto the power supply tagstrip and wire the electrolytic capacitors, standby switch, screen resistors, power switch and bias supply. When the power supply wiring is complete check it thoroughly and re-check the polarity of all the diodes and electrolytic capacitors and the connections of the 100k bleed resistors.

Turn the unit on without any valves series should have equal voltages across them. OK? Turn the unit off and wait for a minute. Then take a screwdriver (no smoke!) take a meter, with well insulated test probes, and check all the voltages across the electrolytic capacitors. The three electrolytics in and short out all the capacitors. If the bleed resistors are working the Even so, always repeat this operation on again to check that the heaters are inserted. If everything seems to be OK capacitors should already be discharged. when you are working on the amplifier, as bleed resistors sometimes fail and the capacitors can give you a very nasty shock. Now insert the valves and turn working. Turn it off (and short the capacitors). voltages

If all is well with the power supply, start wiring the circuitry around V1 and V2. The input blocking capacitor, C1, is wired between the gain control and the input socket while the resistor, R2, should be placed as close as possible to the grid pin to reduce the possible pick up of RF interference. We found it unnecessary to use shielded cable between the valve socket, gain pot, kill switch and input socket but if your wiring is longer than ours it may be required to avoid hum pickup. However,

the feedback wiring should be kept wellaway from the input wiring, or HF instability may occur when the feedback is switched out. Wire the bias circuitry to each of the output valves, making sure that there is no possibility of components shorting together. Use plastic sleeving over the component leads for insurance, because if the bias supply to any tube fails the result is very dramatic! The Ik5 resistors in the grids of the output valves are wired between pins 5 and 6 of the valve sockets.; pin 6 is not internally connected and is used as a terminal — and also places this resistor nearest the grids for best supression of parasitic oscillation.

The 10 ohm resistors in the cathodes are wired across the sockets and it is a good idea to wrap the body of the resistor in tape or plastic tube; in the event of a short in one of the valves this resistor will certainly burn up and deposit carbon over the valve socket and surrounding circuitry, which would then have to be replaced. Using the tape to shield the fallout will minimise the damage, should a fault occur.

Be careful not to cross the two outof-phase signals from the phase splitter;
the signal from the cathode must go to
the grid of V2b and the signal from the
anode must go to the grid of V2a. Also
be careful not to cross the primary
windings of the output transformer; pin
3 goes to the V3 and V4 anodes and pin
1 goes to V5 and V6 anodes. If these
connections are crossed, the phase of
the output will be reversed, the
beedback will become positive and the
amplifier will become a higher power
oscillator!

The power supply is quite capable of powering auxiliary equipment such as a valve pre-amplifier, and a power output socket can be mounted on the

overloaded.

rear panel. The 400 V rail will be able to supply about 70 mA and the three amp heater winding will supply 2.4 amps.

# Powering up There's one good thing about valve

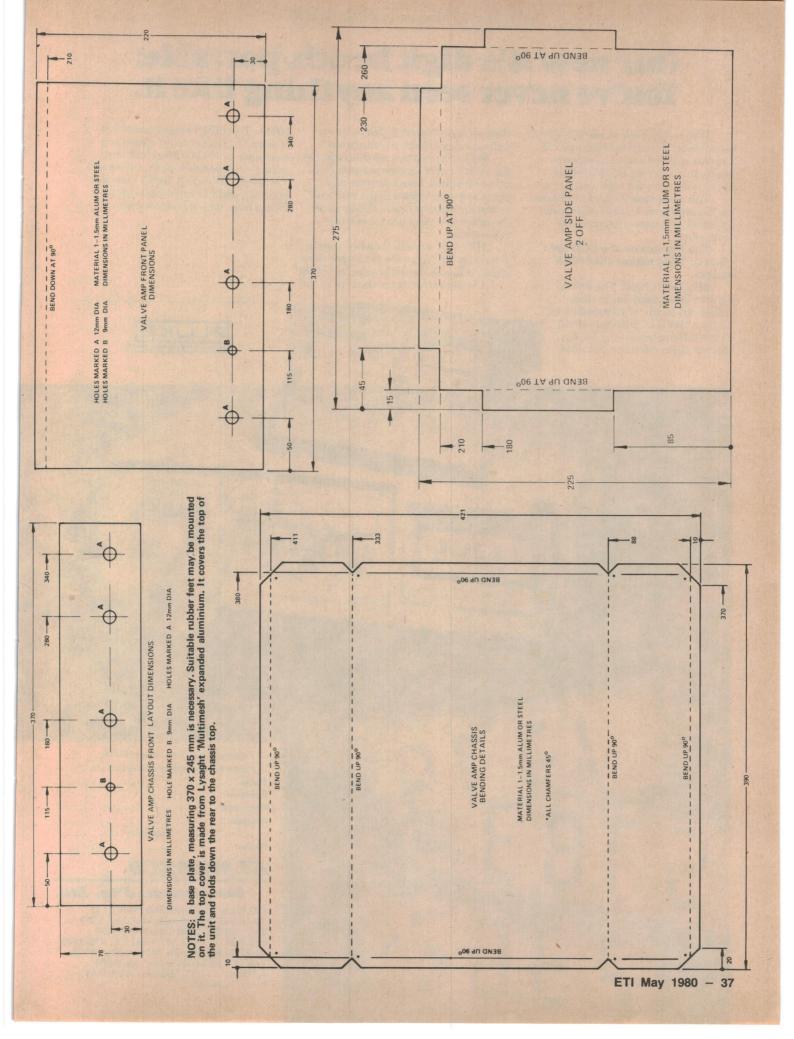
circuitry – it's very obvious if something's wrong – but re-check everything thoroughly in any case.

Turn the amplifier on without any valves inserted first, and check the power supply voltages. To check the big or nin & of each current valves are

lurn the amplitter on without any valves inserted first, and check the power supply voltages. To check the bias on pin 5 of each output valve, set all pots for maximum bias (counterclockwise), turn down the gain pot, then connect a speaker and plug in the valves. Turn on the amplifier and set each bias pot for 0.25 volts across each of the 10 ohm cathode resistors. If anything unusual happens turn off the amp immediately and re-check the wiring! If not, connect a signal to the input, advance the gain pot and you're ready to rock!

# A note on speakers

speakers are extremely rugged, with aluminium voice coils designed to careful not to drive it into clipping. The onset of clipping will not be as harsh transistor amplifier and you may be speakers without knowing it. We strongly recomend the ETI-455 speaker rated to at least 200 watts. These withstand the very high power levels generated by guitarists. If you use the amplifier for hi-fi reproduction, be and as evident as it would be with a doing irrepairable damage to your very quickly blew up a set of 250 watt recommend using loudspeakers specifically designed for the purpose, protector for any application, as we If you plan on using the "Rocker" we strongly the amplifier as a guitar amplifier, speakers when



### Our new 4½-digit bench/portable: You've never seen anything like it.

Take a close look at the face of this instrument. Notice anything new? If you just realized you've never seen words on a low-cost DMM display before, you're on the right track.

This is the new 8050A from Fluke, the lowest priced 4½-digit multimeter available that uses microprocessor technology.

The legends on the LCD are clues to what makes the 8050A

unique.

dB: You're right. The 8050A delivers direct readouts in dBm, referenced to any of 16 impedances. Use the "REF Z" button to scroll through the memory and locate

then set it and forget it. No more tedious calculations or conversions.

REL: For relative references in the dB mode or offset measurements in all other functions. Lets you store any input as a zero value against which all others are automatically displayed as the difference. Another timesaving convenience.

HV: Just a reminder when your input is over 40V, so you won't forget about safety while in the dB or relative modes.

Of course there's much more to the

8050A. True RMS measurements to 50 kHz. Conductance for measuring resistance to 100,000 Megohms and leakage in capacitors, pcb's, cables and insulators. Diode test, 0.03% basic dc accuracy and full input protection. Plus a large family of accessories.

Perth: 398-3362



## 'Auto-probe' for testing vehicle electrical systems

When it comes to probing faults or otherwise in a vehicle's electrical system, a multimeter has distinct disadvantages. This highly convenient probe is very useful in those awkward places so often encountered, plus simple to build and inexpensive.

THE DIFFICULTIES of tracing a fault in a vehicle's electrical system using a multimeter are probably familiar to most readers. As that accursed Murphy's law generally has it, you have to contort yourself in to an awkward position before you can see where to put the test prod, or prods, and having done that, find that you can't twist yourself sufficiently to see the multimeter face.

Damned annoying, isn't it!

Then again, a multimeter can give you a false indication. No, not possible, you cry. It sure is though. If, for some reason, you're measuring the voltage on a particular point and it happens to be connected to the battery via a low, but significant, resistance how do you detect the presence of that low resistance?

A voltmeter measurement won't show it. If that low resistance is the fault, an ohmmeter measurement may well be impossible.

Sorting out the wiring can be a nightmare — especially on motorcycles.

This project gives clear indication of the six conditions one usually finds in an automotive electrical system. These

- Short to +ve supply
- Short to -ve supply
- Open circuit
- Connection to +ve supply via an intermediate impedance
- Grounded via an intermediate impedance
- Connection to a fixed, intermediate (low) voltage level

The Auto-probe is smaller, cheaper, easier to interpret and easier to use and read than a multimeter. It is the sort of device that can be left in the tool kit in the boot of your car or stored in the glove box. It is a worthwhile addition to any mechanically-minded handyman's array of gadgets.

The Auto-probe can be used on 6 V or 12 V systems, with minor changes to the circuit values.



The Auto-probe is housed in a common pill bottle. You can construct it either on matrix board, as shown here, or on a printed circuit board(see over the page). It's an amazingly handy gadget!

To get an idea of how it can be used, and how useful it is, let's take a look at a few typical problems encountered in vehicle electrical systems.

#### The problem

Let us consider the case of a car radio that has 'stopped working'.

Looking at the panel lights, you observe that they aren't lit up when the set's turned on. Obviously, it would seem to be a supply problem. Wriggling, upside down, under the dashboard, you check the fuse and find it intact. Taking the Auto-probe, you attach its supply leads to the rear connection of the cigarette lighter or the ignition switch. Both lights should blink on and off. If they don't then you'd have to reverse the connections and mentally castigate yourself for being a twit. No worries though, it's protected against twits.

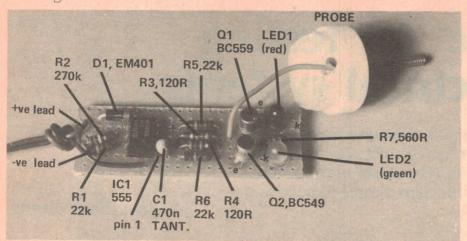
Touching the probe on the radio's

B+ connection, the red LED glows steadily. Aha! This shows the probe tip is connected to the supply. Touching the probe onto the radio's ground lead results in a blinking red LED. Hmm, it's connected to supply via an impedance. It seems the ground connection isn't grounded.

**Ionathan Scott** 

Some jiggling and scraping at the radio's ground lead earthing point results in a steady green LED and a burst of music . . . well, more likely, commercials.

Suppose you wish to know if your car has an ignition ballast resistor. This is a resistance inserted in series with the ignition coil primary during normal running, but is shorted out when the starter is operated so that the coil receives a voltage 'boost'. The resistor may be a heavy wirewound type mounted somewhere in the engine compartment, or (as is common in

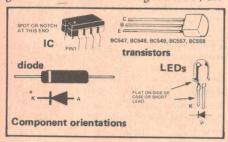


Matrix board construction showing the component positioning and orientation. Note that we used the metal-can type transistors (BC109 etc) in this prototype. R3 and R4 are ½W GLP types.

many late-model vehicles) a resistance lead is used — they're hard to spot.

In this case, the probe tip is touched on the coil primary terminal that is not connected to the contact breaker points. With the ignition on, (engine not running) no light will show on the probe, indicating it is connected via an intermediate impedance. When you touch the starter, the red LED should burst into lusty life, indicating the resistor is shorted, as you would expect.

Tracing wiring and switch operation can be a real hassle. Does this motor-bike operate its horn by supplying power or a ground connection via the horn switch? If touching the two switch contacts in turn shows first a steady green LED then a blinking red LED, the



first contact is grounded and the second is clearly connected to the positive supply via an intermediate impedance, i.e. the horn. If the green LED lights and then both LEDs blink when the probe is touched to the other switch contact, this would indicate that the horn is open circuit.

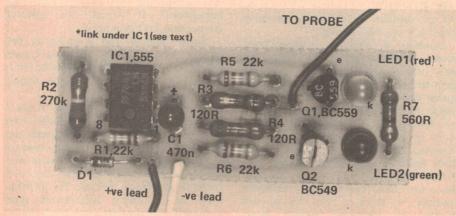
The circuit will cause both LEDs to blink when the probe tip is connected to an open circuit or to either side of the supply via an impedance greater than about 1000 ohms. In an automotive environment 1000 ohms is a high impedance!

Simple, and easy to use, isn't it?

#### Construction

This project may be constructed in either of two ways, depending on your preference: on matrix board, or on a pc board. Both methods are discussed here and overlay photographs are shown also.

If you elect to use matrix board, you will need a piece having holes spaced 0.1" (2.5 mm) apart. Cut the matrix board so that it measures 15 mm wide by 55 mm long — that's about



Overlay for the printed circuit board model. Plastic pack transistors were used for this one.

#### PARTS LIST — ETI 325

Resistors	all 1/4W, 5% unless noted
R1, R5, R6	22k
R2	270k
R3, R4	120R, 1/2W, 5% (GLP type)
	see text
R7	560R

#### Capacitors

C1	 0.47u Tantalum (	35V)

#### Semiconductors

IC1	555
Q1	BC559, or similar
Q2	BC549, or similar
D1	EM401, or similar
LED1	TIL220R or similar, red
LED2	TIL222 or similar, green

#### Miscellaneous

Matrix board — 15 mm  $\times$  55 mm, or ETI-325 pc board; alligator clips; pill container; wire; 30 mm long 4 BA bolt and nut (for probe).

seven holes wide by about 23 holes long (cutting through the 1st and 23rd rows).

It is probably easiest to commence by mounting the two LEDs and the two transistors. You have to take some care when assembling a project on matrix board as the connections between the components are made under the board, using the component leads. Carefully study the overlay picture to see where the components are located and their orientation.

Make the connections between the components using the circuit diagram to guide you. Take care that no short circuits occur between adjacent leads.

Next assemble resistors R3 to R6, IC1 and C1 onto the board and make the appropriate connections. Take care with the orientation of C1. The positive lead is towards the *centre* of the board. Last of all, add R1, R2 and D1.

We'll get around to testing and assembling the unit into the pill bottle shortly, as this will apply to both sorts of construction.

Constructing the project on a pc board is much simpler. First thing to do is locate the position of IC1. A link is inserted between two pads located between the two rows of holes for the IC pins. Having done that, insert the IC. Take care that you have it correctly oriented. All the other components may now be assembled

#### READERS PLEASE NOTE

We do not sell kits or components for the projects described in the magazine. To find out who may be stocking kits or components for the projects featured in this issue, please refer to the 'Shoparound' page. Suppliers for past projects are listed on the 'Kits for Projects' page.

and soldered into the board. Watch the orientation of Q1 and Q2, the two LEDs and C1. Refer to the overlay picture.

Now comes the testing. This procedure applies to either form of construction. You will need either a 12 V battery or a power supply that can deliver around 12 V to 14 V dc. Temporarily solder battery leads and a probe lead to the board. Connect the battery leads to the 12 V supply. The two LEDs should flash. Shorting the probe lead to the negative of the supply should cause the green LED to flash.

If you cannot obtain the correct indications at this stage, look for incorrect connections or components around the wrong way. To check that IC1 is working, connect a multimeter - set to, say, the 30 V range - between the supply negative and pin 3 of IC1 (positive meter lead to the latter). The meter needle should rise and fall at about four times per second.

The pill bottle used to house this project measured 61 mm overall length (with the cap on) by 21 mm outside diameter. A 25 mm long 6 B.A. bolt was used for the probe. This was bolted through a hole made in the cap somewhat off-centre. The photographs show roughly where this needs to be. Just keep it out of the way of the board. A small solder lug under the bolt head is used to attach the probe lead from

D1 EM401 etc The pc board pattern is on page 137. BATT +Ve -LED1 R1 22k 120R 22k R4 120R R2 R7 IC1 270k 560R 555 TO 22k PROBE 02 0.47u TANT LED2 GREEN BATT -Ve

the board. The battery leads should be colour-coded to avoid confusion. The convention is: red for positive, black for negative. Twist together about one metre of each colour hookup wire.

Connect the appropriate leads to the board and tie a knot close to the board (see photograph).

Drill a hole in the end of the pill bottle, near the edge, and pass the battery leads through it. The knot prevents the leads being pulled out of the board. Attach alligator clips to the ends of the battery leads.

Two small cutouts will have to be made in the lip of the pill bottle's cap so that the LEDs may be seen easily. All these details are clearly shown in the photograph of the completed project.

Once you have the unit assembled,

give it a thorough work out.

Once you have this little project working for you, you'll be amazed how quickly electrical problems in your vehicle are sorted out.

#### MODIFICATIONS FOR 6 V OPERATION

Change R3 and R4 to 68 ohms each Change R7 to 180 ohms Change R5 and R6 to 10k

#### **HOW IT WORKS - ETI 325**

Consider first the 'idle' state of the device - i.e: with the probe open circuit. Diode D1 protects the whole circuit against accidental reversal of supply polarity. When the battery is connected correctly, the battery voltage (less about 0.7 volts dropped across D1) is applied to the electronics.

IC1 is the familiar 555 timer IC, connected as an astable multivibrator. When C1 charges up to 2/3 of the supply voltage, via R1 & R2, the 'high' level comparator (pin 6) detects this and sends the output high, which also shorts pin 7 to near ground. C1 thus commences to discharge via R2. When it reaches 1/3 of the supply voltage, the 'low' level comparator trips (pin 2) and C1 is allowed to recommence charging as before, since the output is sent low. This cycle repeats indefinitely, with a frequency of

 $F = 1/(0.692 \times C1 \times (R1 + 2R2))$ With the values chosen, this is about 4 Hz. This may be varied by changing C1 or R2. The output on pin 3 of IC1 oscillates between nearly OV and V+ (less 0.7 volts). It can source about 200 ma.

Consider now the circuitry surrounding the LEDs. Assume at first that the voltage

on the junction of R5 and R6 is about half the supply potential. Current will flow through the bases of both transistors via R5 and R6, hence both of these transistors will conduct. Each transistor will short out the LED connected in parallel. Thus neither LED will glow. If the voltage on resistor junction (the probe connection) were to fall below 0.6 volts, or thereabouts, Q2 would be biased off and would no longer bypass the current flowing through R7 away from the green LED. Thus the green LED would light. Similarly, if the voltage on the probe were to rise to within 0.6 volts of the unit's supply rail (i.e: within 1.3 volts of the battery supply, due to the action of D1) Q1 would be biased off and the red LED would light.

Now let us put the picture together and see what happens in practice. The output of IC1 is connected to the probe and the resistor junction of the LED driver circuit via a 60 ohm resistance made up of two 120 ohm resistors in parallel. There are two resistors rather than one 1W or larger resistor for reasons of physical size.

With no connection made to the probe, the 555 drives the probe alternately to the +ve and -ve rails, with the result that the LEDs flash alternately.

Shorting the probe to either rail of course forces the appropriate LED to stay on continuously. If a resistance is placed between the probe and ground, say, three possibilities occur:

1) The current flowing from pin 3 of the 555, via R3/R4, is insufficient to develop 0.6 volts across the resistance - this looks like a short and the green LED stays on. 2) The current develops sufficient voltage to turn Q2 on and the LED extinguishes on that part of IC1's cycle when its output is high. This allows the appropriate LED (green) to blink.

However, if the resistance is not high enough to allow the junction of R5/R6 to go far enough positive the red LED will not turn on. This gives green only blinking. 3) If the resistance is high enough (over 1k) both LEDs blink, giving the opencircuit response.

The same argument applies 'upside down' for a resistance to rail, but the voltage across it must be 1.3 V due to D1 being in the emitter circuit of Q1. If the voltage is fixed midway, neither LED can glow, as first assumed.

Resistor R7 fixes the LED current and R3/R4 limits the 555 output current to a safe level and defines the voltage 'turnover' points.

## PLESSE



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#### MN9102

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The MN9105 is a 4-decade BCD counter which counts up or down on negative transitions of the Clock input. In parallel with the counter is a 16-bit non-volatile MNOS memory into which the contents of the counter can be written. When data has been written into the memory it can be retained in the absence of applied power, and subsequently be recalled from the memory to preset the counter.

#### MN9106

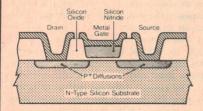
The MN9106 is a six-decade up counter in parallel with a twenty-four-bit MNOS memory which can provide non-volatile data storage of the current count position.

#### MN9107, MN9108

The MN9107 will count up to 99 hours, 59 minutes, 59 seconds, while the MN9108 counts up to 9999 hours, 59 minutes or 9999 minutes, 59 seconds.

#### **APPLICATIONS**

Applications for NOVOL are found in all forms of metering. security code storage, back-up storage for microprocessor based systems, elapsed time indicators, electronic counters. latching relays and many other general industrial areas.



\*NOVOL devices are produced using the Plessey Metal-Nitride-Oxide-Silicon (MNOS) process. MNOS transistors, as shown here in simplified form, are fabricated with a 'sandwich' structure gate dielectric consisting of a very thin layer of silicon oxide and a thicker layer of silicon nitride. In operation, a positive or negative charge injected (Written) into the nitride/oxide interface modifies the threshold voltage of the transistor. Since the injected charge is trapped within the bulk of the dielectric it is not affected by surface leakage and the difference between high and low thresholds can be detected (Read) over very long periods.



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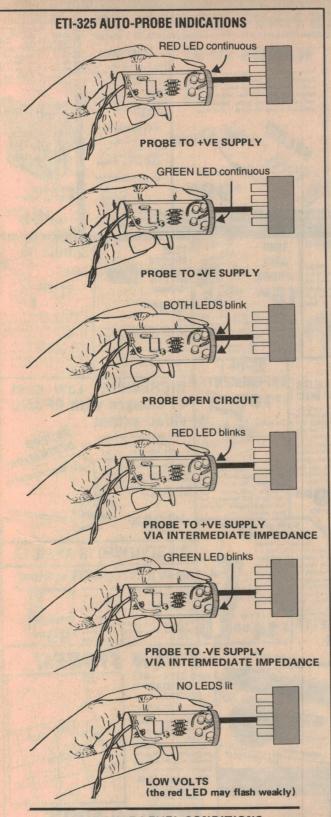
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#### IMPEDANCE LEVEL CONDITIONS

Both LEDs blink
Red LED steady
Green LED steady
Red LED blinks
Green LED blinks

probe sees impedance larger than 1000 ohms probe to +ve via impedance less than 15 ohms probe to -ve via impedance less than 6 ohms probe to +ve via imp. between 15 & 400 ohms probe to -ve via imp. between 6 & 800 ohms





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PCB STAND PACK Holds printed circuit boards off chassis, firmly & securely. Snap into place. Pack of 6, 9m Cat H-1981

BRACKET PACK

DON'T FORGET: We also have a large variety of packs containing nuts, bolts, washers, etc. They're at your nearest store!

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The 'New Decade' catalogue from Dick Smith Electronics was presented free with last month's Electronics Australia and Electronics Today. If you missed out on your copy, don't worry: there are plenty available from your nearest Dick Smith store or our mail order centre. The price is just 75c: worth that for the data specifications section alone!



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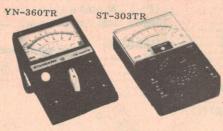
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SPECIFICATIONS
Measurement Ranges:
DC V 0-0. IV-0.5V-2.5V - 10V-50V - 250V - 1000V (20ΚΩ /V)
AC V 0-10V-50V-250V-1000V (8ΚΩ /V)
DCmA 0-50WA-2.5m A-25m A-0.25A
50WA at 0.1V DC position

Resistance

X1 X10 X1K X 10K 0.2 2 200 200K 20 200 20K 200K 2K 20K 2M 20M Range Minimum Midscale Maximum dB-10dB ~+ 22dB for 10V AC Battery: 1.5 × 2, 9V X 1

Accuracy: DC V & mA: within ± 3% F.S. AC V: within ± 4% F.S. ohm: within ± 3% Arc

Dimensions & weight 147 x 100 x 45mm 430g ST-303TR \$30.39 plus tax

SPECIFICATIONS: DC Voltage: 0.0.3, 1.5, 3, 12, 30, 120, 300, 1200 Volts 20k 42 /V. AC Voltage: 0.6, 30, 120, 300, 1200, 8k sh /V. DC Current: 0.0.06, 3, 30, 300mA, 12A. Ohms: 0.20 Megohms in 4 Ranges ± 3%. 20 ohms center Scale

Decibels: 10 to +17.

Transistor checker: Iceo (L1) 0-150 A on x 1K Range; 0-15mA on x 10 Range; hfe 0-1000 on x 10 Range; lc/18

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ST-350 \$16.48 plus tax SPECIFICATIONS.

Range of Measuren DC Voltages: 10V 50V 250V 500V 1000V (2K ℜ /V) AC Voltages: 10V 50V 250V 500V 1000V (2K ℜ /V) DC Current: 0.5mA 25mA 500mA 10A Resistance:

ST-300

X1 X10 X 1000 201 2001 10K5 5001 5K1 1M5 0.21 21 20051 Range Midscale Maximum Minimum

Volume level: 20 ~ + 22dB & + 20 ~ + 36dB Capacity: 0.0001 ~ 0.03 F & 0.01 ~ 0.6 F Inductance: 10~1000H

High resistance: 0.1—50MJUse external power Batteries. Two 1.5V dry cells (UM-3 or equivalent) Allowance. DC Voltage & Current: Within ± 3% f.s. AC Voltage: Within ± 4% f.s. Resistance: Within ±3% of scale length Size & weight. 138x96x51/mm 480g

#### ST-300 \$38.70 plus tax

SPECIFICATIONS.

SPECIFICATIONS:
Range of Measurement:
AC Amperes (AC A): 6A 15A 60A 150A 300A
AC Voltages (AC VI: 150V 300V 600V
Resistance (): 1kK (centre: 30 )
Tolerance:

AC Ampere: 3% of maximum graduation. AC Voltage: 3% of maximum graduation Resistance: 3% of Scale length.

Inside Battery and fuses of Resistance Range 1 piece UM-3 Bat-tery, 1.5 Volts 3 piece 0.1A Fuses in a Glass Tube (9.5–11.5)

SP-10D



#### SP-10D \$16.09 plus tax

SPECIFICATIONS

Measurement ranges.
DCV 0.25 10 50 250 500 1000 (4K \$\mathbb{L}\_{\text{N}}\text{/V})
DCmA 0.25 25 500 (250mV drop) ACV 10 20 250 500 1000 (4K % /V) 50

- X1 X10 K S -20 200 10K - 500 5K 1M - 0.2 2 200 Maximum

Maximum
Minimum
Battery - 1.5VX1

B - 20 ~ + 22 + 20 ~ + 36 ~ + 62

MA0.1 ~ 50

usin

uF 0.0001~0.02 0.01~0.3

Within = 2.5% fs for DCV 8 mg using external

Accuracy. Within ± 2.5% fs for DCV & mA; Within ± 3.5% fs for ACV; Within ± 3% of arc for ...

Dimensions & weight 140x95x44mm & 310gr.

#### ST-5 \$11.74 plus tax

SPECIFICATION Range of measurement

Resistance: 0 ~ 600K (7000 ohm center)

Allowance DCV and DCA: within ± 3% f.s. ACV: within ± 4% f.s. ohm: within ±.3% arc

Size and weight: 90x60x28/mm 120g.

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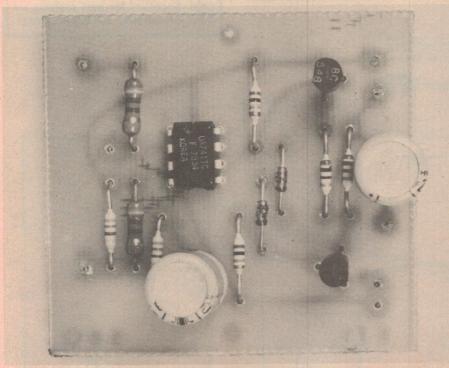
## Mains cable seeker

**Phil Wait** 

Finding mains cables hidden in wall cavities would require the X-ray vision of Superman or the divining skills of a 'dowser' . . . unless you had this project.



The sensor used for this project is a "telephone pickup coil" — the black object at the top. The inexpensive magnetic earpiece, below the pickup coil, indicates when you have located a cable.



Construction is very simple - just about foolproof if you use a printed circuit board; see over.

WHETHER YOU'RE engaged on extensive house renovations, or just want to bang in a picture hook, it's not only handy but a decided safety advantage to know where your mains wiring is located in the wall cavity.

After all, you don't want to drill straight into a mains cable and discover it by the shower of sparks . . . do you! It may well be the last thing you ever discover . . .

This simple device picks up the alternating magnetic field radiated by any cable connected to the 50 Hz mains. A simple, inexpensive "telephone pickup coil" is used as the sensor, the 50 Hz signal induced in this is amplified and applied to a small earpiece.

Commencing at any outlet or wall switch, you can trace where the cable runs by passing the pickup coil back and forth over the position where the 50 Hz hum is loudest, moving along the line of the loudest sound. The run of the cable may be marked with tape or whatever suitable method springs to mind.

Design

The design of the Mains Cable Seeker is extraordinarily simple. The pickup coil is a commercially-available unit that consists of a coil of many turns of fine wire wound on a small bobbin which is slipped over a soft-iron 'core'. This is encapsulated in a plastic container having a suction cap on one end. The suction cap enables the unit to be attached to a telephone. However, this feature is not used with this unit.

If the pickup coil is brought near any alternating magnetic field a current will be induced in the windings of the pickup coil and a small signal voltage will appear across the ends of the coil.

The pickup coil is connected to the input of a sensitive audio amplifier which raises the level of the signal such that it will drive an earpiece.

**Dowser** — user of a "dowsing rod" or "divining rod"; a person who uses a rod, wire etc holding it in a particular way that gives an indication when the user approaches water, metal etc.

### Project 560

The amplifier design used in this project utilises an operational amplifier as a voltage amplifying stage, the output of which drives two transistors operated as a low power output stage. Feedback is applied directly from the output to the input. The resistance in the feedback path determines the gain, and thus the sensitivity, of the whole amplifier. A potentiometer is placed in the feedback path to allow you to vary the gain, depending on the strength of the 50 Hz field picked up from the cable you are tracing.

#### Construction

For simplicity, and to avoid wiring errors, we strongly recommend you construct this project using the printed circuit board design given here. You can make your own pc board, or buy

#### **HOW IT WORKS - ETI 560**

This Mains Cable Seeker works by detecting the weak alternating magnetic field of any current-carrying mains wiring. This signal is amplified to drive an earpiece. A pickup coil consisting of many turns of wire on an iron core is used to locate the field surrounding the mains cable.

The weak signal induced into the pickup coil is first amplified by IC1, a type 741 operational amplifier (op-amp). This IC normally requires to be operated from a dual supply but, in this application, is biased to operate from a single 9 Vdc supply. The non-inverting input of the 741 (pin 3, marked +) is biased to half the supply via a potential divider consisting of R2 and R4. The junction of these two resistors is decoupled for ac by a 100u electrolytic capacitor, C1. The signal from the pickup coil is applied between the half-supply point and the inverting input of the op-amp (pin 2, marked —).

The op-amp, IC1, is arranged here as a variable gain inverting amplifier; that is, the output is out of phase with the input. The output of the 741 (pin 6) drives two output transistors, Q1 and Q2. These are connected as a complementary emitter follower current amplifier, driving the earpiece. Diodes D1 and D2 ensure that the bases of Q1 and Q2 are correctly biased, bias current being provided by R5 and R6. Resistors R7 and R8 are output current limiting resistors, the output being taken from their junction to the earpiece via a dc isolating capacitor, C2.

Feedback is taken directly from the output to the inverting input of IC1, via the gain control, RV1 and R1. The value of R1 sets the minimum gain (about unity).

Varying the feedback ratio, by varying R1, varies the gain of the whole amplifier.

one ready made. They should be widely available from a number of suppliers.

Commence construction by soldering the resistors and diodes in place. Take care with the orientation of the diodes. Refer to the overlay picture to make sure which way around they go. Next solder the two transistors in place — make sure you get them in their respective positions. Watch the lead orientation. Follow this with the IC making sure you get it the right way round also.

As the two electrolytic capacitors are a little cumbersome in comparison to the other components, they are soldered in last. These too, are polarised components, so watch which way you insert their leads. Refer to the overlay picture.

Once you have the pc board assembled and checked, you can

connect the external components and give the project a trial run.

Run wires from the pc board to the input and output jack sockets, to SW1 and RV1 as indicated on the external wiring diagram shown with the pc board overlay picture. The battery connector has one red lead (the positive connection) and one black lead (the negative connection). The red lead is soldered to the other pole of SW1 and the black lead is soldered to the '0V' connection indicated (on the pc board).

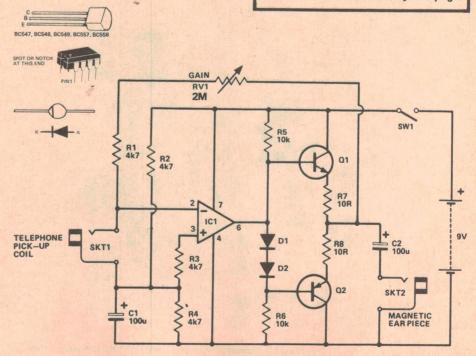
You are now ready to test the project. Plug in the pickup coil and the earpiece. Turn the unit on, you should hear a click in the earpiece. With an appliance plugged into an outlet and turned on, bring the pickup lead near the appliance's cord and advance the gain control. You should clearly hear the 50 Hz hum in the earpiece when you pass the pickup coil near the cord. Try tracing the hidden wiring a short distance.

If all is well, you can now think about mounting the completed project in a suitable box. One of the commonlyavailable plastic "zippy" boxes would

# ETI 560

#### **READERS PLEASE NOTE**

We do not sell kits or components for the projects described in the magazine. To find out who may be stocking kits or components for the projects featured in this issue, please refer to the 'Shoparound' page. Suppliers for past projects are listed on the 'Kits for Projects' page.



mains seeker

be ideal. One of these measuring 130 x 70 x 40 mm will accommodate the pc board, the other components and the battery with ease. However, any similar box would suit, just make sure everything will fit.

#### Suggestions

If you experience trouble with broadcast station pickup — where the pickup coil and input lead (and perhaps your body) act as an antenna — solder a 1n (1000 pF) ceramic or greencap capacitor across the input jack connections, as shown in the wiring diagram with the overlay picture.

You can wind your own pickup coil if you wish. We wound one on an 8 mm diameter by 30 mm long steel bolt. You must use a steel bolt. Being a ferro-

magnetic material it concentrates the lines of force of a magnetic field in which it is placed, hence you will get greater induction in the pickup coil with a steel bolt than with any other type.

We first wound a layer of sticky tape over the thread of the bolt. A coil of about 300-400 turns of a light gauge enamelled copper wire was then jumble wound on this, then covered with a layer of sticky tape to hold it in place. The wire gauge is quite non-critical. Too heavy a gauge is difficult to handle and you won't fit the required number of turns on a bolt the size we used. Any gauge from, say, 26 to 32 gauge is OK—it doesn't matter if it's SWG or B&S. Any gauge lighter than 32 g tends to break very easily.

The coil/bolt assembly may be encapsulated for protection, or fitted

into a small pill bottle or something similar. A length of shielded cable or a twisted-pair wire cable should be used to connect the pickup coil to the input jack.

#### PARTS LIST — ETI 560

 Resistors
 all ½W, 5%

 R1, 2, 3, 4
 4k7

 R5, 6
 10k

 R7 & 8
 10R

Capacitors

C1, 2 ..... 100u 16 V electrolytics

Semiconductors

 Q1
 BC548, BC108 or similar

 Q2
 BC558, BC178 or similar

 IC1
 741 op-amp

 D1, D2
 1N914, 1N4148 or similar

Miscellaneous

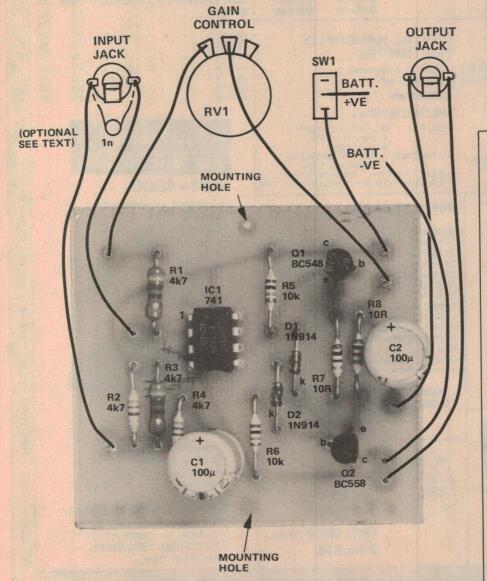
 RV1
 2M linear pot

 SW1
 SPST toggle switch

 SK1, SK2
 3.5 mm jack sockets

 B1
 Type 216 9 V battery

Zippy box to suit, battery clip, ETI-560 pc board, magnetic earpiece, telephone pickup coil or wire and bolt to wind your own.



Component overlay and external connection diagram for the project. Follow this carefully.

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Software programmable; Line and Character Formats, 16 lines of 32, 16 lines of 64, 20 lines of 80, 20 lines of variable length. Up to 165 characters, Standard Video or TTL output, 1K Bytes of screen RAM expandable to 4K Bytes, CRT Bug to replace J Bug.

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MEK 6810		 •	•	٠	•	•	•	•			•				•	•	٠	•	•	•		\$167.00	\$192.05
MEN COAO																				-	-		Ψ115.00
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1454 00 1455					•	•		-	*			•	•									\$110.00	\$126.50
MEK 6800 AI	3			11																		\$110.00	\$400 FO
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MEK 68 R2 .																						\$240.00	\$276.00
MEK CO DO										-		-	-	•		•	•	•	•	•	•		\$192.05
MEK 68 RR.		 															0	2	15	1	100	\$167.00	\$192.05
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	16 PIN															24	.28
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	<b>20 PIN</b>															26	.30
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the PET computer

The Pet has a television screen, a keyboard as simple to use as a type writer and a self-contained cassette recorder which is the source for programmes and for storing data in connection with these programmes. And it has, in its standard configuration, an 8K user memory. (This is in addition to the 14K operating system resident in the computer).

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#### 2001-16/32



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#### 2040

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The Dual Drive Floppy is the latest in Disk technology with extremely large storage capability and excellent file management. As the Commodore disk is an "intelligent" peripheral, it uses none of the RAM (user) memory of the CBM The Floppy Disk operating system used with the CBM computer enables a programme to read or write data in the background while simultaneously transferring data over the IEEE to the CBM. The Floppy Disk is a reliable

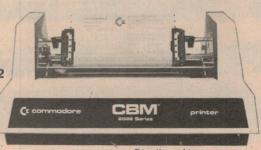
low cost unit, and is convenient for high speed data transfer. Due to the latest technological advances incorporated in this disk, a total of 340K bytes are available in the two standard 5½" disks, without the problems of double tracking or double density. This is achieved by the use of two microprocessors and memory I.C.s built into the disk unit. Only two connections are necessary — an A/C cord and CBM interface cord.

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The Tractor Feed Printer is a high specification printer that can print onto paper (multiple copies) all the CBM characters—letters (upper and lower case), numbers and graphics available in the CBM The tractor feed capability has the advantage of accepting mailing labels, using standard preprinted forms (customized), cheque printing for salaries, payables, etc. Again, the only

connections required are an A/C cord and CBM connecting cord. The CBM is programmable, allowing the printer to format print for: width, decimal position, leading and trailing zero's, left margin justified, lines per page, etc. It accepts 8½" paper giving up to four copies. Bidirectional printing enables increased speed of printing.

CONTACT YOUR LOCAL DEALER FOR FURTHER INFORMATION, PRICING AND DEMONSTRATION.



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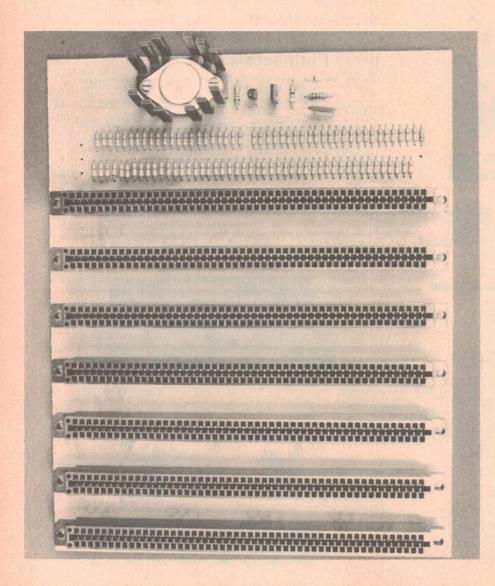
#### HANIMEX 既

Commodore Business Machines Division.

## Low cost S100 motherboard with seven sockets and active termination

#### **Barry Wilkinson**

This is the essential part necessary to link your S-100 system together. The board features active termination, additional regulated supplies and seven card capacity.



Overall view of the S-100 Motherboard. We have not mounted the extra power supply regulators and components on the board.

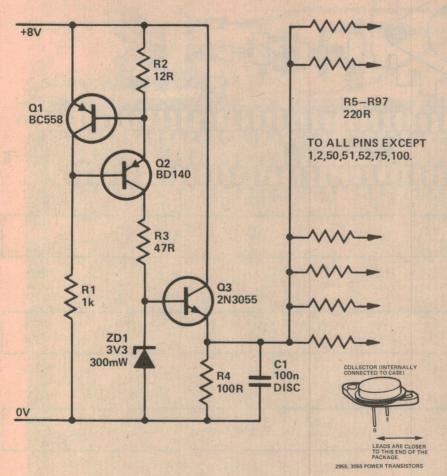
THE MOTHERBOARD described here is a low-cost 'starter' for the hobbyist who has spent all his money on more 'important' items like the CPU, VDU, etc. Mounted in a cheap case (or even standing alone) the board will connect and support up to seven (or more) S-100 cards.

Construction of this board is very simple. Once the pcb has been made, it is a good idea to use a continuity tester or ohmmeter to check for continuity along the length of the tracks. After this has been done, the sockets should be soldered in, and the continuity tester used again to check for absence of shorts between adjacent tracks. Note that adjacent tracks do not go to adjacent pins on the sockets, but instead to opposing pins.

The active termination resistors can now be soldered into place, if required, and the regulator circuitry assembled. The board should be given a final visual inspection, and is then ready for use.

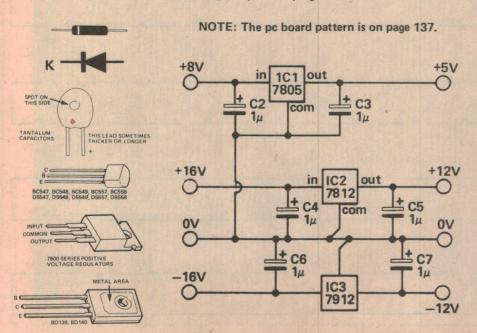
The capacitance between adjacent tracks on this board is fairly high, imposing some limitations. It is possible (in theory) to reproduce the artwork and extend the board to 14 or more sockets, but the capacitance will rise, and problems will result. For the same reason, 4 MHz Z-80 cards may experience problems with the motherboard, and if this happens, they should, if possible be switched to 2 MHz. A seven-socket board has been run without the active termination circuitry at 2 MHz with no trouble.

Ideally, the motherboard should be mounted in a card cage, with plastic card guides to either side to support the cards and reduce stress on the sockets and solder joints. It is possible to make do without a cage, but if you



are considering 'doing up' your computer with a proper, smart, cabinet, that's the time to consider the installation of a high

quality double-sided motherboard with earthed guard tracks — otherwise, you're just delaying the inevitable.



#### **HOW IT WORKS - ETI-636**

The purpose of the motherboard is to provide interconnection between as many as seven S-100 bus computer cards. Active termination of the data and address lines are provided, along with additional regulated supply rails for powering peripherals.

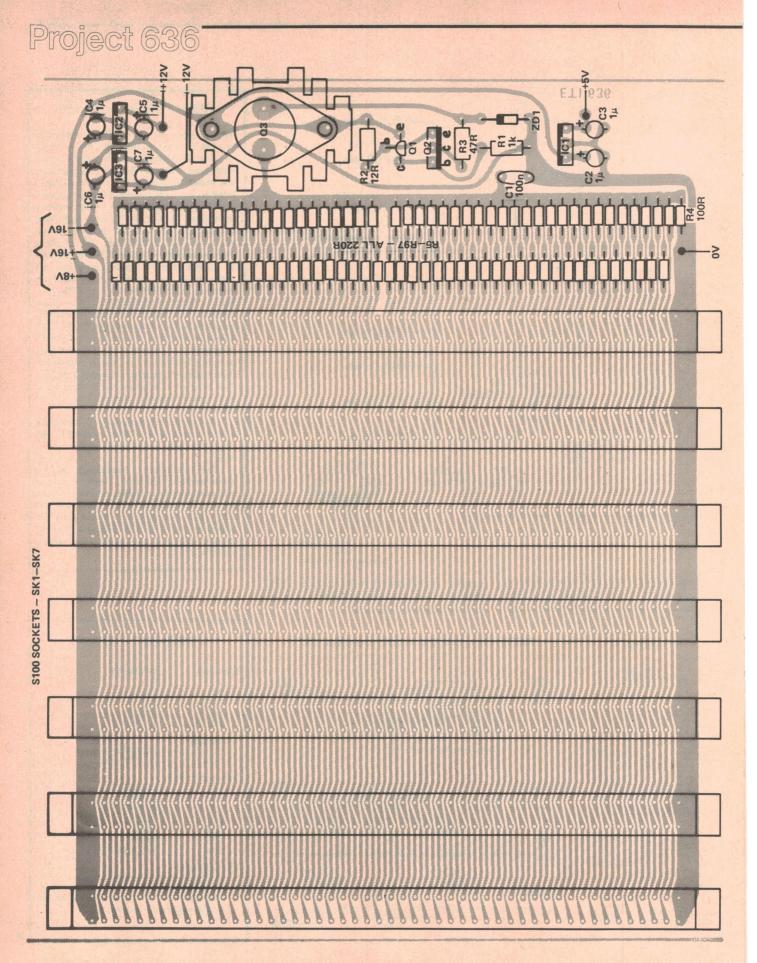
The active termination circuit involves transistors Q1, Q2 and Q3 plus associated components. Q1 and Q2 provide a constant current source for ZD1, which clamps the base of Q3 at 3.3 volts. Q3 acts as a series regulator, providing about 2.7 volts across R4. Each of the bus lines requiring termination has a 220 ohm resistor between the end of the line and a common bus (resistors R5 to R97) which connects to the emitter of Q3. Resistor R4 (and the common line of the terminating resistors) is bypassed by C1. "Open" lines will thus be held at 2.7 volts dc, but terminated with a resistive impedance at RF. The lines may be driven hi or lo at quite high clock speeds without significant reflections.

This board will operate with processor systems running at 4MHz, indeed it was originally used, sans terminations, at 2 MHz.

The additional regulators involve three-terminal flat-pack regulators, IC1, IC2 and IC3. IC1, a 7805, provides +5 Vdc at 1A; IC2 provides +12 Vdc at 1A and IC3 -12 Vdc at 1A. These are not necessary for normal S-100 cards and may be left off, but are useful with certain peripherals.

#### PARTS LIST - ETI 636

Resistors	
R1	
R2	
R3	100P
R4	
no-no	2201
Capacitors	
C1	100n disc ceramic
C2-C7	1μ, 25V tantalum
Semiconductor	
Q1	
.02	BD140
03	.2N3055
IC1	
IC2	
IC3	
ZD1	3V3, 300 mW zener
Miscellaneous	
	board, seven S-100 solder-
	(SK1 to SK7), finger-type
	r Q3, nuts, bolts and about
	ram of solder!
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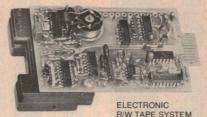
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#### INFORMATION TECHNOLOGY

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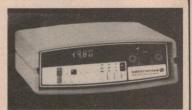
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2N5961 2N5963	.18 1.10	TIP3055 .80 VMP4 28.00	GRAPHIC PRODU FORMERS, RALM	AR PRODUCTS	TEXAS		0 ns)	64 for \$29	
2N6027 2N301		VN88AF 2.50	INSTRUMENT C	ALCULATORS	. VER-	2708 (45	60 ns) 60 ns)	1-8 for \$8.5 16-32 for \$8.3	35 ea
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AD161 AD162	.45 .90 .70 .70 .70 .70 2.00 1.70	2102 450NS 1.20 2102 650NS 1.20	tised in E.T.I., E.A.	, or A.H.A. mag	jazines.	4116 (20	0-250 ns)	32 or more \$8.6	2 ea
BC318 BC319	.18	2111 8.60 1	DM8578 3.5	0.1				THE SHAPE OF THE S	
BC327 BC328	.18 .18 .15 .17	2113 300NS 6.30   2114 450NS 5.90	AY-5-2376 19.5 MM5104N 10.0	6 VOLTAGE	REGULATO .5V 100mA	RS .40	MAN74A	3"CC Red	2.20
BC337 BC338	.20 .20 .12 .18	8 to 31 5.60 32 Up 5.40 2513 12.40	MM55106N 10.0 MM57160 7.5	0 LM341P-5	.5V 500mA .5V 1A	.8C 1.00	MAN52A MAN82A	3"CA Green 3"CC Green	3.40 3.40
BC547 BC547B BC548	.12	2516 55.00		7905 LM309K	.5V 1A .5V 1A	1.70	MAN82A MAN84A	3"CA Yellow	3.40
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BC549C BC557	.12 .18 .16	2708 8.50 2716 33.00 4116 12.00	MCT275 3.3 MCT275 1.5	0   78H05KC 0   LM341p-8	.5V 5A .8V 500mA	6.10 .80 .40	MAN8610 MAN8640	Red Red	3.30
BC558 BC559	16	5101 9.00 55101 5.50	4N28 .8	5   79L12	.12V 100mA .12V 100mA .12V 500mA	.65 .75	TIL306 DL704 DL707	3"CC Red 3"CA Red	12.00 2.20 2.30
BC637 BC638	.25	MM52030 14.50 MM5204 12.50	4N33 4N26 1.2	7812	.12V 1A .12V 1A	1.00	DL747	63"CC Red 63"CC Red	3.40 4.00
BC639 BC640	.16 .25 .36 .30 .30	MM5220 7.20 MM5303N 4.10	ZENER DIODES	7812 7912 7812KC 7912KC 7912KC 79H12KC 78CBUC	.12V 1A .12V 1A	2.15 2.60	FND357 FND500 FND507 FND800	362"CC Red	1.30
BCY70 BCY71 BD115	.85	MM5307 18.00 MM5309 6.50	E23 Range 400MW .1	79H12KC 78CBUC	121/50	6.00 2.20 2.90	FND507 FND800	5"CA Red 8"CC Red 8"CA Red	1.50
BD135 BD136	1.50 .50 .50	MM5312 9.00 MM5369 2.50	1 Watt .2	3   78CBUC   78L15	.13.8V 2A .13.8V 2A .15V 100mA	.35	SEL521	CC Red	3.40 2.80
BD137 BD138	.40	5387 MM5395 MM5740 15.60	CAPACITORS	LM341P15	.15V 100mA .15V 500mA .15V 1A	.65	NSB7881 NSN781	CC 4 DIGIT MUX Red	10.60
BD139 BD140	.40	6502 10.50 6508 5.50	Polyester 100V-250V	7915CT	.15V 1A .15V 1A	1.00 1.40 2.60	FNA5220	CC 2 DIGIT MUX Red CC 2 DIGIT MUX Red	4.90
BD235 BD234	.65	6520 5.50 6522 10.00	.001-027 .0 .033-056 .1	9 78H15KC	.15V 5A .18V 100mA	6.10	11113220	MUX Red	3.40
BD237 BD262	1.20	6532 17.00 6551 17.00	.068-1	5 7818	.18V 1A .24V 100mA .24V 100mA	1.40	S.C.R.'s		
BD301 BD302 BD263	.75	IM6561 4.50 MCM6574 19.60	.12-22 .2 0.27uf .3 0.33uf .3	0 79L24 0 7824	.24V 1A	1.10	T10681 C106B	200V 4A 200V 4A	.70 .80
BD435 BD646	1.25 .70 1.70	MCM6575 9.20 MC6800P 9.00	0.39uf .4 0.47uf .4	0   LM337T	.ADJ 1A	2.40 3.80 3.47	C106D1 C106E	400V 4A 500V 4A	.50
BD647 BD675	1.80	MC6802 13.60 MC6808 12.50 6810A 4.90	.56,.68,.82 .5 1,1.2,1.5 1.0 1.8uf 1.0	0   LM337K	ADJ 2A ADJ 2A	5.00	C122D1 C122E	400V 8A 500V 8A	1.20
BDV64B BVD65B	3.00	6810A 4.90 6820 5.50 6821 6.00	2.2uf 1.2 3.3uf 2.0	U I 78HCKC	.ADJ 3A .ADJ 5A .5V 10A	8.40 7.00 7.50			-100
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BF180 BF195	.60	7106 7107 15.00	I.C. SOCKETS	VM48	400V 1A DIL 200V 1.5A	1.00	SC141D SC146D	400V 4A 400V 6A 400V 10A	1.40
BF198 LF199 BF336	.15	7210 13.20 LS7220 6.00	8 Pin .2	0 W04 W06	400V 1.5A 600V 1.5A	.50	ST2 ST4	400 V 10A	2.00 .30 .40
BF337 BF458	.80 .80 .90	8035 27.00 INS8050 15.00 INS8080 8.00	18 Pin .4:	5   NBPOUZ	200V 3A 200V 6A	1.30	SC151D	500V 15A	2.10
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## Autostart for the RTTY system

This is the final part in Tom Moffat's series of RTTY articles. With this 'autostart' unit you will no longer have to hang around and wait for those RTTY signals to appear — completely automatic, unattended operation is possible.

YOU'VE PROBABLY HAD your teletype system going for some time now, growing in sophistication with each new article in ETI. You are now able to select some obscure signal and listen intently, waiting for it to burst into a stream of radioteletype. You've also probably discovered that you can spend a lot of time waiting for something to happen, waiting to hit the motor switch to start the system printing!

It does get boring, doesn't it?

Well, your troubles are over. As from now you can tune your receiver to some signal so as to produce a mark tone in the converter, or you can tune it to some empty frequency known to be used by amateur RTTY stations. You can then go away and leave it, and come back, perhaps several hours later to find every message passed on that frequency

nicely printed out on your teletype, waiting for your perusal. If copy has been sent for say ten minutes out of four hours, the motor has run only for those ten minutes.

This article describes a device with a deceptively simple function — turning a teletype's motor on and off. The difficulty comes in determining when to do it. Ideally, the motor should run only when the machine is receiving valid teletype copy, and should remain switched off at all other times.

This autostart circuit is able to do this without any operator intervention at all. It will not be fooled into turning on by CW signals, a constant carrier, voice, facsimile, music, or any modulation other than radioteletype of the proper shift and speed. As the circuit uses signals from the UART, the speed

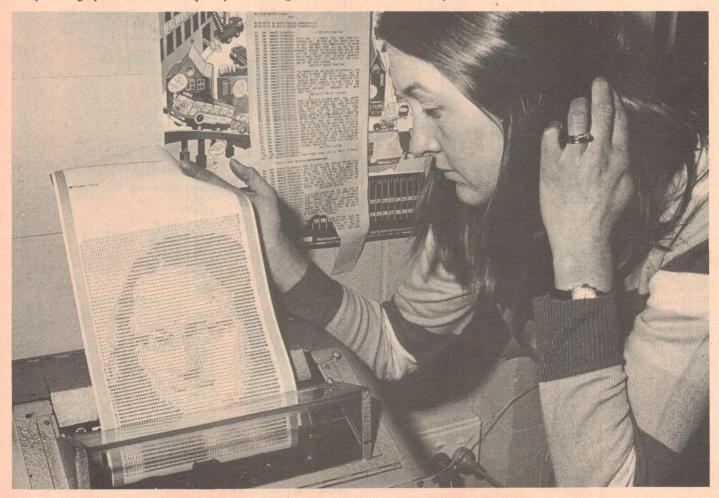
#### Tom Moffat VK7TM

converter/regenerator circuit (ETI, March 1980) must be constructed first.

#### **Features**

The autostart has two selectable modes of operation:

- The 'easy' mode, in which the teletype will turn on if: (a) a mark tone is present, (b) a character is received at least once every ten seconds, and (c) the received characters are not at the wrong speed or inverted.
- 2) The 'hard' mode, in which the teletype will turn on if: (a) all the above conditions are met, and (b) valid teletype characters are received continuously (tape sending). The machine will not start if the signals are off speed or distorted beyond certain limits.



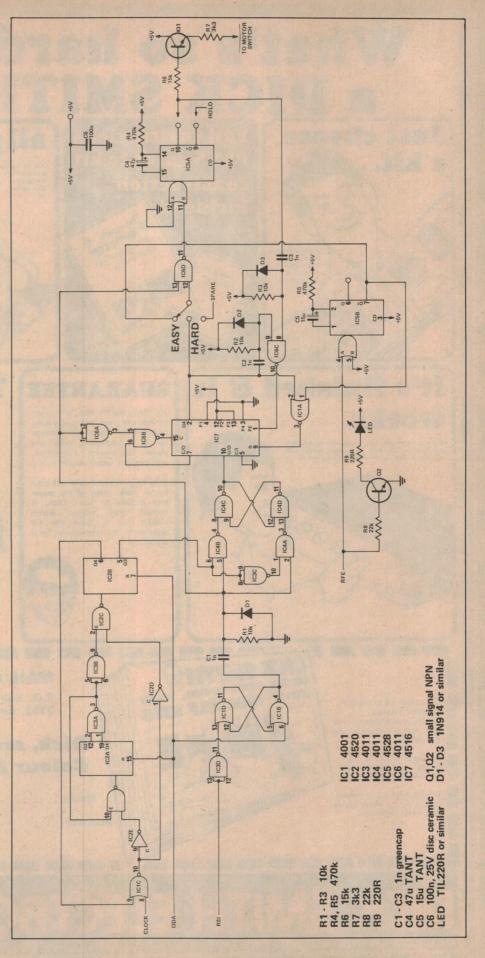
The operating speed is selected by the baud rate switch on the UART board.

The UART has an output called 'RFE' or 'received framing error'. This is generated when the stop pulse is missing and is the UART's way of saying it thinks a character may be in error. Framing error indications occur more or less continuously when no carrier is present, or when received teletype signals are of the wrong speed or 'upside down'. They are a useful tuning aid, so this circuit includes a LED to give a visible indication.

In the 'easy' mode the autostart senses the lack of framing errors to indicate a mark tone is present, with no upside-down or wrong speed characters. If this condition is present for more than three seconds it 'arms the system' so that the next character causes a motor start. False starts are possible because once the framing error detector has timed out, any circuit activity, even a noise burst, is interpreted as a character. If the noise burst is shorter than a character length (and most of them are) the signal will return to 'mark' before the stop pulse is expected and no framing error will result. The 'easy' mode is useful on VHF circuits where fading and noise bursts are not normally encountered, and on amateur HF nets where a carrier is not present unless copy is being sent.

On HF circuits a different situation exists. A steady mark tone is normally transmitted when no copy is being sent. Such a circuit can remain idle for hours at a time and then burst into life, sending copy by tape transmitter at the maximum character rate. This is where the 'hard' option comes into use. Under the 'easy' system the motor would start and run for ten seconds every time noise or fading caused any interruption to the mark tone. The 'hard' mode requires at least two characters, with no framing errors, spaced a specified distance apart, before it will cause the motor to start. It is apparently impossible for these conditions to occur 'naturally', that is from noise or non-teletype modulation. In all the hours of testing this circuit it has never given a false start in the hard mode, but it does suffer the slight disadvantage of requiring tape-speed signals for it to operate. It will also miss the first two characters of a transmission before starting on the third, but this is of little consequence.

The 'easy' or 'hard' option is selected by a three way switch. The third position is intended to be used with a code recognition circuit now being developed.



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used a pc board, matrix board construction should work equally well.

#### How it works

EASY MODE: The incoming teletype signal, taken from the RSI pin (receive serial input) of the UART, is inverted by IC3d and fed to IC1d and IC1b, a flip-flop. The flip-flop allows only the first downward transisition of a character to pass through, and then blocks everything else until reset for the next character by ODA (output data available) from the UART. C1R1 turns the upward transisition from the flip-flop into a very short positive pulse (the diode is there to soak up the negative pulses). The positive pulse is fed into one input of IC6d where it's used to indicate circuit activity.

IC5 is a dual retriggerable multivibrator. Its 'B' section has a time constant of about three seconds, set by C5R5. Application of a positive pulse at input A will cause the Q output to go high for the time period. Pulses occuring more often than the time period will cause Q to remain high continuously. It's been determined experimentally that under noise-only conditions, the UART generates at least one framing error every three seconds, so when there is no carrier the multivibrator remains operated, and stays that way until three seconds after a carrier appears and framing errors cease.

When the multivibrator times out its Q output goes low, its  $\overline{Q}$  output goes high, and this enables NAND gate IC6d to allow circuit activity pulses through to another multivibrator, IC5a. This one has a time constant of about ten seconds, and it remains operated as long as activity pulses keep triggering it more frequently than once every ten seconds.

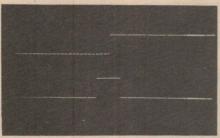
In the operated condition, IC5a's Q output feeds an emitter follower stage to operate a relay, via a switching transistor causing the teletype's motor to run. The motor will stop ten seconds after the last character is received, or 13 seconds (sum of both multivibrator times) after continuous framing errors begin. A single framing error will have no effect because IC5a remains operated during the three second time IC5b operates.

HARD MODE: Because of the way the UART operates, the next start pulse in a continuous character transmission is expected 16 clock pulses after the ODA pulse, which is in turn generated eight clock pulses into the previous stop pulse. So what we're doing is measuring the time from one stop pulse to the next start pulse, which is represented by the first RSI transisition after ODA.

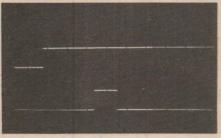
RSI signals follow the same path as before, up through C1R1, where they're

fed to one input each of two NAND gates, IC4b and IC4a. IC1c, 2a, 2b, 3a and 3b form a pulse counter that gives a low output for the first 14 clock pulses from the UART board. For the next four it goes high, and then it goes low again and stops until reset by ODA, when the sequence begins again.

Under good transmission conditions the expected start pulse will occur pretty close to 16 clock pulses from ODA, but with bad conditions it will vary all over the place. The output of the pulse counter forms a 'window' four clock pulses wide, centred on 16 which is fed into gate 4b, then inverted and fed into 4a. These gates sort the RSI pulses into two groups: those that occur within the 'window' come out of 4b, and those that miss it come out of 4a.



Autostart waveforms: Top trace shows the next start pulse — taken at pin 4 of IC1b (first RSI, inverted); lower trace is the 'window' at pin 5 of IC2. The next start pulse has made a direct 'hit' in the window.



With the same conditions as above, this shows the next start pulse missing the window badly. (Horiz. - 4 ms/div.; Vert. - 5V/div.)

The sorted pulses are fed to another flip-flop, IC4c and 4d. Its output goes high for 'good' pulses and low for 'bad' ones. The flip-flop output goes to IC7, a presettable up/down counter, which is clocked by RSI pulses. The NAND gate 6b causes the counter to count to 15 and stop (by cutting off the clock pulses) or it can count down to zero and stop, the direction being determined by the state of the flip-flop. The gate prevents the counter from 'going over the top' and starting again.

When the flip-flop is fed with a continuous string of 'good' pulses the counter will add up RSI's and stick at 15. If fed with continuous 'bad' pulses the counter will subtract RSI's until it sticks on zero. A mixture of good and

bad pulses will cause the counter to work its way up and down. If the majority are 'good' the count should stay above eight, and if the majority are 'bad' it should stay below eight. The eight (or more) count is detected, and used to enable the ten second motor timer (with the help of circuit activity pulses as described earlier). So, when most start pulses fall within the window the motor start is enabled, but if circuit conditions begin to deteriorate, the count works its way down, eventually to below eight, when the autostart switches off.

There are some other features to further this cause. As framing errors can occur spasmodically, even with the best of signals, those that occur when the count is above eight are ignored, blocked by IC1. But those that occur when the circuit is slowly failing) will operate the counter's reset and knock the count right back to zero. This tells the system the odds are against it and it would be wise to give up trying, and stop the motor.

If the count is slowly decreasing, but no framing errors occur, the count will be kicked down to six when it goes past eight in the down-hill direction. This feature prevents the counter cycling back and forth between seven and eight on the way down, and is implemented by the pin 9 input of IC6c.

The other input of IC6c comes from the motor timer. When circuit conditions are good, but the circuit goes idle, IC5a will time out after ten seconds, shutting off the motor until more copy comes along. When the timer times out it fires a pulse into IC6c that results in the count being preset to six. This means, after a pause in circuit activity, at least two characters are required to get the motor going again.

If the circuit goes idle during failing conditions, the count is again preset to six, but each fade or noise pulse will pull it down further, so more characters are required to re-start the motor as conditions deteriorate. The aim of the scheme is to make the system earn the right to continue after every shut-down. Another feature applies a 'hold' to the UART board when the timer times out, to prevent gear crunching as the motor slows to a stop.

#### **Motor switch**

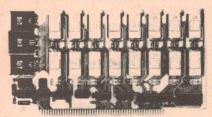
The original version of this circuit used a power control relay with a 110 Vdc coil. This was fed from the teletype loop supply through a dropping resistor, and switched on and off with a high voltage transistor.

The scheme worked very well, but as it used a relay and wasn't 'modern'

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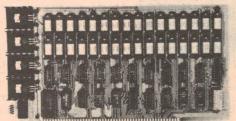
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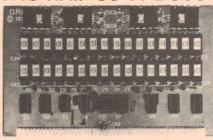
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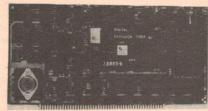
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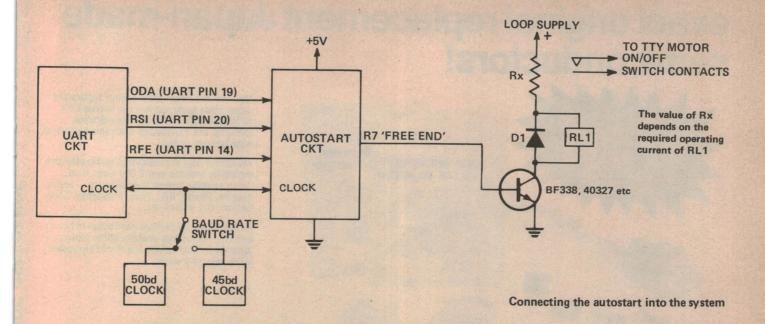
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it was decided to employ a solid state switch using a triac and several other components on a small circuit board. This also worked very well — for nine weeks, when it 'blew up' with much smoking of resistors and charring of the circuit board. The reason why this happened is not clear, although it's suspected that the triac eventually broke down under the heavy starting current of the motor.

Had this happened while the unit was unattended, it could have started a fire. So the solid state switch was abandoned, and the relay was put back in service. In the relay version, the dropping resistor equired (if any) depends on the supply voltage and the type of relay, so you'll have to select it to suit.

#### A warning

Although it may seem unecessary to mention it, remember that you now have a piece of rotating machinery that can start at any time without warning. Do not forget it's 'armed to go' and then try to change the machine's ribbon or paper. When the motor starts it will be accompanied by immediate typing, and it's best not o learn the hard way how it feels to be hit on the thumb by a flying key hammer!

Previous articles in this series appeared in the August 1979 issue (Project 730, receiver demodulator); the September 1979 issue (Project 731, transmitter modulator) and April 1980 (improvements to the RTTY system).

There has been considerable demand from readers for pc board designs for the UART etc, and no doubt the same will apply to the autostart unit described here. Boards are in preparation and we hope to publish them at an early opportunity.



TOM MOFFAT, author of the teletype articles, was born in the USA 39 years ago. He now lives at the outer fringe of Hobart, on the slopes of Mt. Wellington, with his Queensland-born wife Gael and three young children.

Tom began his career about age six — demolishing alarm clocks, as do most radio freaks.

He completed two years of a university course in physics and engineering before running out of money. Next stop was the American Telephone Company, working in the private line/television operating/teletype test section, and it's here that his interest in RTTY developed.

Two years later he signed a contract with NASA to work at Kwajalein Island in the South Pacific at a tracking station, but an 'unfortunate' change in plans resulted in him being posted to Bermuda and Hawaii instead.

Next stop was the Nevada test site, operating a tracking

radar for a couple of years. He then went back to the telephone company in Reno, taking a second job as an announcer with a local radio station.

When the news editor turned up too drunk to read the major bulletin one night, Tom suddenly found himself in radio news.

He migrated to Australia in 1968, and took a job with GTV-9 in Melbourne, first as an audio operator, then back to radio news with 3AK, and then on to television news with GTV.

After a holiday in Tasmania he decided "this was the place to live" and made the move in 1974 to set up a small two-way radio business in Hobart.

After three years of rising costs and falling income he chucked in the business and went back to television news at TVT-6, where he is still employed.

When not 'playing radios' Tom enjoys bushwalking and photography, usually both at the same time.

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	C6200.61	2SC9952.72	2SC13450.54	2SD1803.50	AN2173.07	MB37133.30	LA4032P4.83
	C6451.20	2SC10000.46	2SC135815.76	2SD1983.30	AN23911.50	UPC554C2.15	LA4050P3.91
2SA7062.12 2SC	C6740.61	2SC101116.36	2SC13640.54	2SD1995.06	AN2413.54	UPC574J1.61	LA4051P4.32
2SA7151.37 2SC	C6814.90	2SC10131.10	2SC14071.10	2SD21312.42	AN2457.59	UPC575C22.79	LA44004.95
2SA7190.56 2SC	C7100.39			2SD2341.42	AN247P6.90	UPC587C22.45	LA44304.14
2SA7250.54 2SC	C7110.37		2SC14444.97			UPC1009C6.00	LM18202.25
2SA7330.49 2SC	C7120.39	2SC10304.11		2SD2611.10		UPC1020H4.03	LM2902A3.66
2SA7404.37 2SC	C7306.44	2SC103412.65	2SC14471.58		AN3139.78	UPC1025H3.11	STK0119.66
	C7320.46		2SC14482.95		AN3154.26	UPC1028H2.83	STK01511.04
	C7330.85					UPC1032H2.25	STK01613.62
	C7340.61		2SC1472K1.25		AN71153.68	UPC1156H3.80	STK02420.04
	C7350.46		2SC14751.17		AN71504.26	UPC1185H4.58	STK43312.88
	C7380.49	2SC111411.04		2SD3581.75		TA7045M3.57	STK43919.55
	6C7410.42	2SC11161.17	2SC15202.08	2SD3590.98	HA1156W3.54	TA7061AP2.90	PLL02AG12.19
	SC7563.91		2SC15501.65	2SD3601.10	HA11993.84	TA7074P8.51	SG61313.80
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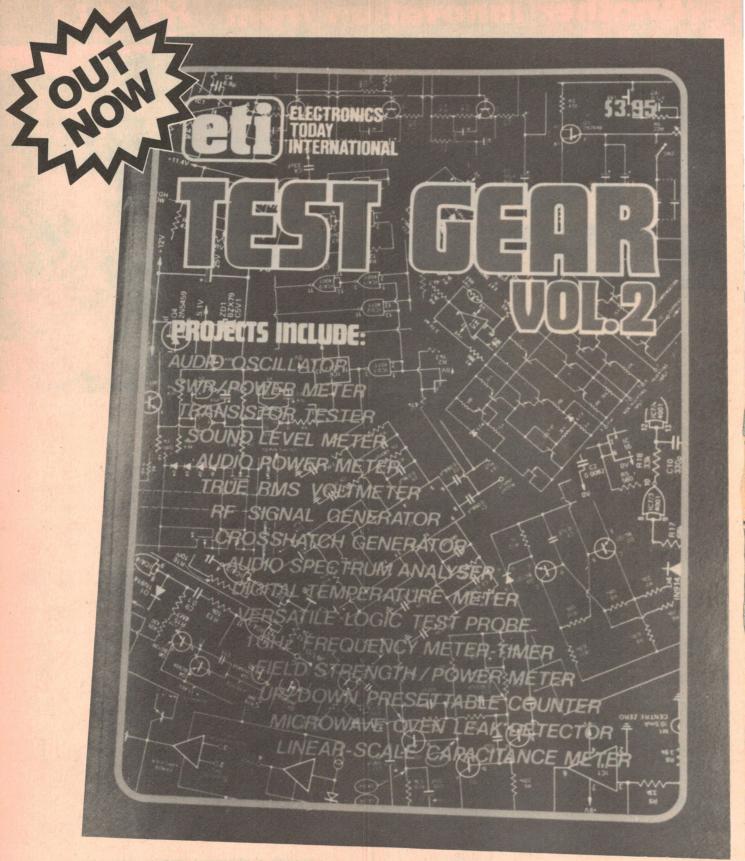
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## Lab Notes

## Walking rings . . . and other miracles

A common task facing the electronics designer is that of producing simple digital counter/divider networks which produce an output frequency or count rate that is some fixed fraction of an input frequency or count rate. Here's how to do it.

DIGITAL DIVISION, or counting, is a fairly straightforward task — providing you know how (!), chiefly involving the manipulation of circuit 'blocks' to economically or conveniently do the task required. But, as the old saying goes, there's more than one way to skin a cat...\*

#### 4013 and 4027 flip-flops

The two most basic counter/divider ICs in the CMOS range are the 4013 dual D-type flip-flop and the 4027 dual J-K flip-flop. Figure 1 shows the outlines and pin notations of these two

devices, which each contain two independent flip-flop stages sharing common supply connections. Each of these packages can be used to give division ratios or 2, 3 or 4.

A single 4013 'D' stage can be made to act as a divide-by-two counter by grounding its SET and RESET pins and coupling its DATA pin to its Q output, as shown in Figure 2a. A single 4027 J-K stage can be made to act as a divide-by-two counter by grounding its SET and RESET pins and connecting its J and K pins to the positive supply rail, as shown in Figure 2b. Both of these

#### **Ray Marston**

circuits change state on the positivegoing transition of the input clock signal, which must have rise and fall times of less than 5 us. The 4013 is veryfussy about the shape of its input clock signals and tends to be rather temperamental in operation. The 4027 is not too fussy about its clock signals and is very easy to work with.

#### **Ripple counters**

Figure 3 shows how two divide-by-two 'D' or J-K flip-flop stages can be wired in series to give an overall division ratio of four (2<sup>2</sup>). Figure 4 shows how three



Figure 1. Outlines and pin notations for the versatile 4013 dual-D and 4027 dual J-K CMOS flip-flop ICs.

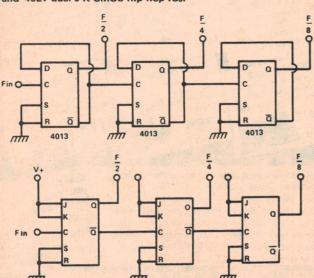


Figure 4. Two versions of a divide-by-eight ripple counter using D-type (top) and J-K (bottom) flip-flops.

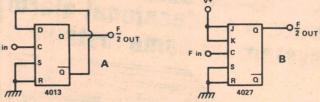


Figure 2. Divide-by-two counters made from D-type (left) and J-K (right) flip-flops.

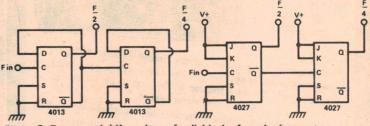


Figure 3. D-type and J-K versions of a divide- by-four ripple counter

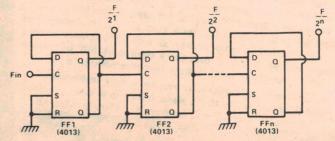


Figure 5. How a chain of D-type flip-flops can be linked to provide a divide-by-2 ripple counter.

An occasional series in which we discuss interesting circuit techniques, circuits we have tried in our own laboratory but not developed as a project, practical notes on projects, measurement techniques for hobbyists etc.

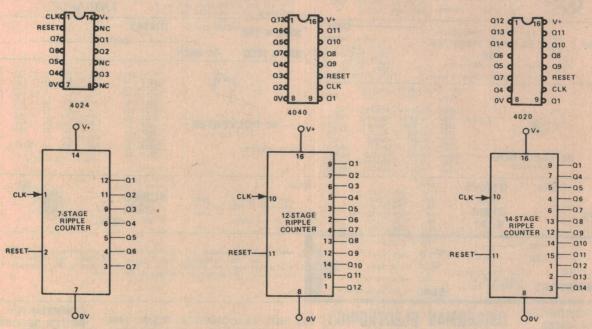


Figure 6. Outlines (above) and functional diagrams (below) of three popular CMOS multi-stage ripple counter ICs.

such stages can be wired in series to give a division ratio of eight (2<sup>3</sup>). Note that each counter stage is clocked at precisely half the rate (an octave below) of the preceeding stage, so that the clock signal seems to 'ripple' through the counter chain. Also note that, as is made clear in Figure 5, the final division ratio is equal to 2<sup>m</sup> where 'n' is the number of counter stages. Thus, four stages give a ratio of 2<sup>4</sup> = 16, five stages give 2<sup>5</sup> = 32, six give 2<sup>6</sup> = 64, seven = 128 and so on.

A detail not made clear in the above diagram is that, since the counters of a 'ripple' circuit are effectively wired in series, the propogation delays of the individual stages in the counting chain add together to give a fairly long total delay at the end of the chain. If each stage has a delay or 100 ns and there are ten stages, the total propagation delay is 1 us. Consequently, the first output signal will not change state until 1 us after the arrival of the original input clock signal that initiates that change of state. The counter states of the 'ripple' type of counter are thus not in perfect synchrony with the original clock signal and this type of circuit is consequently known as an asynchronous counter.

The 4013 and 4027 counters can be cascaded to give any desired number of ripple stages. When more than two stages are required it is usually

economic, however, to use a specialpurpose MSI ripple-carry binary counter/divider IC. Figure 6 shows the outlines and functional diagrams of three popular ICs of this type.

The 4024 is a seven-stage ripple unit with all seven outputs externally accessible. It gives a maximum division ratio of 4096. The 4020 is a fourteen-stage unit with all outputs except 2 and 3 externally accessible; and it gives a maximum division ratio of 16 384.

Figure 7 shows the outline and functional diagram of a special-purpose ripple-carry unit, the 4060. This is another fourteen-stage unit, but does not have outputs 1, 2, 3 or 11 externally accessible. The special feature of the 4060 is that it incorporates a built-in clock oscillator circuit. The diagram shows the connections for using the internal circuit as either a crystal or an RC oscillator.

The 4020, 4024, 4040 and 4060 ICs

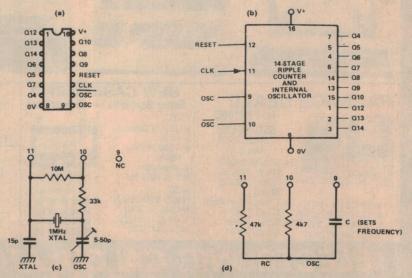


Figure 7. Outline (a), functional diagram (b) and alternative oscillator connections (c and d) for the 4060 fourteen-stage ripple counter.

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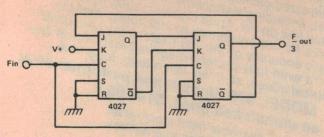


Figure 8. A divide-by-three 'walking ring' or 'Johnson' counter using J-K flip-flops,

Figure 9. A divide-by-five Johnson counter using J-K blocks.

are all provided with Schmitt trigger action on their input terminals and trigger on the negative transition of each input pulse. All counters can be set to zero by applying a high level on the RESET line.

### 'Walking ring' or 'Johnson' counters

An alternative to the ripple type of counter is the so-called 'walking ring' or 'Johnson' counter. In these counters, all stages are clocked in parallel and the stages are cross-coupled so that the response of one stage to a clock pulse depends on the states of the other stages.

Figure 8 shows the connections for making a divide-by-three counter from two J-K stages and Figure 9 shows the connections for making a divide-by-five counter.

A major advantage of the 'walking ring' or 'Johnson' counter is that, since all stages are clocked in parallel, the outputs of the completed counter are subjected to only a single stage or propagation delay. Consequently, the system gives synchronous operation and outputs give glitch-free decoding.

#### 4018 divide-by-n counter

When count numbers greater than four are required, it is economic to use MSI

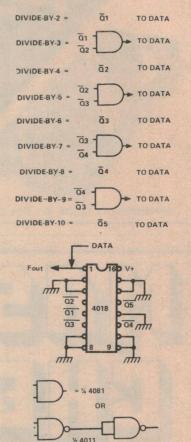
ICs such as the 4018, rather than the 4013 or 4027. The 4018 is a five-stage 'Johnson' counter that can be made to divide by 2, 3, 4, 5, 6, 7, 8, 9 or 10 by merely cross-coupling its terminals in suitable ways. The IC features a Schmitt trigger on its clock input line and clocks on the positive transition of the input signal.

Figure 10 shows the outline and functional diagram of the 4018. Figure 11 gives methods of cross-coupling the IC to give division ratios from two to ten. On even division ratios, no additional components are needed. On odd ratios, a two-input AND gate is required in the feedback network. This gate can be a single 4081 AND stage, or can be made from two 4011 NAND stages.

#### Greater-than-10 division

Even division ratios greater than ten can usually be obtained by simply cascading suitably scaled counter stages, as shown in Figure 12. Thus, a divide-by-two and a divide-by-six stage give a ratio of twelve, a divide-by-six and a divide-by-six give a ratio of 36 and so on.

Non-standard and uneven division ratios are obtained by using standard counters, such as the 4018, and decoding their outputs to generate suitable counter-reset pulses on completion of the desired count.



CONNECTIONS FOR DIVIDE-BY-N OPERATION

Figure 11. Methods of connecting the 4018 for divide-by-two to divide-by-ten operation.

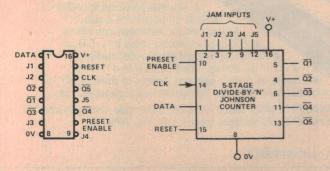


Figure 10. Outline and functional diagram of the 4018 presettable divide-by-n counter.

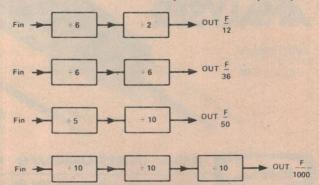


Figure 12. Typical examples of division by numbers greater than ten.





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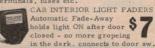


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# Ideas for Experimenters

These pages are intended primarily as a source of ideas. As far as reasonably possible all material has been checked for feasibility, component availability etc, but the circuits have not necessarily been built and tested in our laboratory. Because of the nature of the information in this section we cannot enter into any correspondence about any of the circuits, nor can we produce constructional details.

# Sound to light modulator

Modulating a light, or a bank of lights, from a sound source (such as a tape recorder or record player) is an ever-popular topic so we dragged this circuit from the depths of our files.

A high impedance input is provided by a source-follower, Q1, so that the unit may be driven from either a high or low impedance source. An op-amp (a 741) then provides sufficient gain to trigger the SCR which drives the LED. As the input varies, the drive to the LED will vary, modulating the light output. Each 'Section' (1,2,3...) drives a LED, all the LEDs being mounted in a row.

When setting up, RV1 and RV2 are adjusted so that with the maximum input voltage available, 1 V is available at pin 6 of the op-amp. Then VRX is adjusted so that the LED lights. Then Section 2 is tackled; adjust VRX for

that section so that its LED lights with 0.9 volts at pin 6 of the 741. Continue with the subsequent sections so that each LED lights at 0.8 V, 0.7 V etc at the output of the 741. The display produced is rather like a VU display; with the column lighting up as the sound rises and falls.

# **Telephone amplifier**

Have you ever had occasion where two or more people needed to listen to a telephone conversation? Normally, a 'phone conversation is a one-to-one affair. This simple amplifier, from J.P. MacAulay of the UK, solves the problem neatly.

No direct connection to the telephone is necessary. Mr MacAulay has

R1 9k1

R2 470k

R3 47k

R3 47k

R3 47k

R3 6 3n3

R4 4k7

R5 100µ

R1 1N914

R7 100µ

R7 100µ

R7 100µ

R7 100µ

R7 100µ

R7 100µ

cunningly used an ordinary 5 mH RF choke as a pick-up coil — taped to the side of the phone set. Q1 is a commonbase amplifier, the output signal on its collector driving the input of a 741 op-amp. The power output stage is driven by the output of the 741. Two complementary transistors are used and feedback is applied to the inverting input of the 741.

The gain of the op-amp may be varied by R6 and you can use either a preset pot or a standard pot and knob.

The frequency response of the amplifier is tailored to suit the voice characteristics of the telephone. Quiescent current consumption is less than 5 mA so the circuit can be run easily from a pair of PP3 9 V batteries connected in series.

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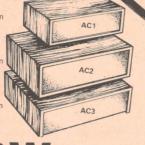
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Beat this value! Kit 60 Compact Cassette Deck Mechanism. This kit is a play-back mechanism that comes complete with stereo output amplifier. The

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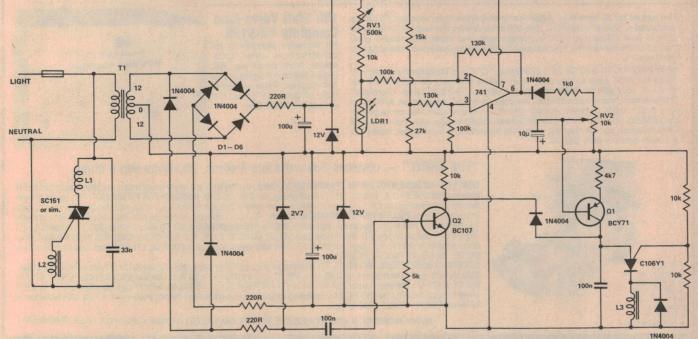
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# Porch light controller

Mr. R. Johnson from the UK has designed this auto-dimmer for turning on a porch light at dusk and then controlling the brightness such that it is inversely proportional to the surrounding lighting conditions. It sets the porch light brightness to a minimum at dusk, increasing the brightness until it reaches a maximum after total sunset. In the morning, the light is slowly reduced in brightness as the sun rises, turning it off at full daylight.

The dimming circuit uses a triac

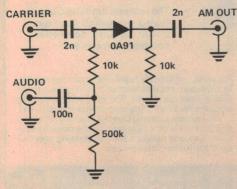
to control the brightness of the porch light, conduction angle being controlled by Q1 and an SCR pulse circuit via a transformer, L2/L3.

The potentiometer RV1 varies the light level at which you wish to have the porch light turn on. Potentiometer RV2 sets the maximum brightness (maximum conduction angle of the SC151) of the porch light. the LDR determines when the dimmer starts and ceases to operate. Its resistance varies between 600k at dusk to about 6M at dark. A suitable type might be an LDR03 or LDR04,

or similar. Note that Q1 is a BCY71, Q2 is a BC107/BC547/BC207 etc. The transformer T1 is a 12-0-12 low current type. L1 is an interference suppression choke and consists of 30 turns of 20 swg enammelled wire on a 12 mm length of 'loopstick' antenna ferrite. The transformer L2/L3 consists of 15 turns wound bifilar (two parallel wires) on a 15 mm length of loopstick antenna ferrite also.

A fuse is connected in series with the lead going to the porch light for safety.

# All-round modulator



A very handy device around any hobbyists workshop or serviceman's bench is a simple modulator. For aligning IF amplifiers, receiver front ends etc — especially with only basic test instruments, it's a must.

Reader, G.J. Armitage of Melbourne Vic, sent this circuit in. A common signal diode is used as a 'mixer'. You'll need to drive the audio input with more signal than the RF input to get good modulation depth.

The circuit will work across a very wide frequency range, from very low frequencies to well into the VHF region. The diode can be any germanium signal diode, such as OA90,

OA91, OA95, OA202 etc. The RF drive will need to be around several hundred millivolts.

A silicon signal diode, or a hotcarrier, diode may be used, but you'll need around half a volt of RF drive.

Constructed in a small shielded container, with coax input and output connectors (RCA connectors are good), prevents radiation of signals and a switched attenuator may be connected on the output.

The circuit may also be used as a product detector. BFO injection should be fed in the 'Audio' input and the resultant audio taken from the output (add a 'pi' RF filter using two 1n capacitors and a 1nH RF choke).

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You asked for it, here it is. After many enquiries from readers ETI have produced a "valve" amplifier. This will probably be the last of this type, so here is your chance to build a vintage amp and learn some basic electronics at the same time. You will also have an amp that is very durable and serviceable.

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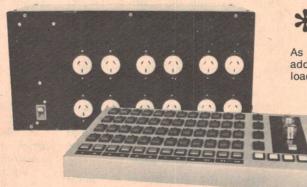
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The Stage Rack is a 12 channel unit, each channel 2000 watts. Power is 3 phase, standard 30A per

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The Desk consists of four presets of 12 pushaction switches, each with its own LED indicator. Each preset has a master switch and a flash-to-full button. Each of the 12 channels also has a flash button. A selectable chaser offers variable switch-

ing across the masters if required.
The Rack is complete with 12 solid state switch-

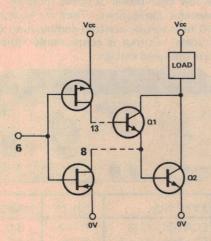
ing units, individually fused. Each unit can be easily replaced, replacement units being readily available from our agents. The solid state switching units are zero switching to minimise interference.

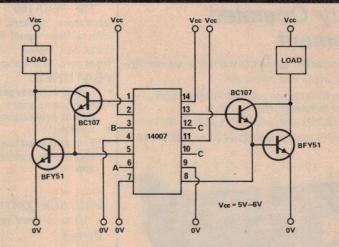
The Remote Lighting Control Board is unique and it's built with Australian touring conditions in mind. See one now at a Barratt Lighting agent or send for further information.

Distributed nationally by BARRATT LIGHTING Pty Ltd

See page 42 of this issue of ETI for a list of our agents.

# **Ideas for Experimenters**





# **Darlington drivers**

This circuit from C.J. Ramey, UK, offers a very efficient way of driving a pair of transistors in Darlington configuration from CMOS. The circuit at right shows how two loads of up to 1A may be driven from a single 14007 chip with no external resistors. Using a

2N3055 in place of the BFY51 will enable loads of up to 3A to be driven at voltages limited only by the Vceo of the transistors.

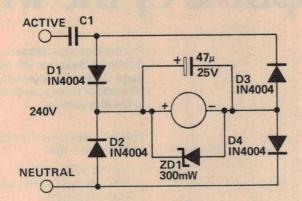
The circuit at left shows the internal circuit of one section of the 14007. A high on pin 6 switches the lower CMOS transistor on, holding Q2 off and sinking the leakage current of Q1. A

low on pin 6 drives Q1 and switches the lower CMOS transistor off and the upper CMOS transistor on.

The result is fast switch off at low

cost and efficient switch on.

A bonus is the inverter between pins 10 and 12. Note: Vcc should be 5-6 V to prevent excessive current being drawn from the CMOS chip.



# **Operating a Sonalert** from 240 Vac mains

There are occasions when it is convenient to operate a Sonalert-type piezo-electric alarm from the 240 Vac mains. The accompanying circuit, from Barry Wilkinson of Nebula Electronics, shows how it's done.

The 'ACTIVE' input is switched to activate the alarm. Capacitor C1 acts as a current-limiting device, the four diodes being arranged as a bridge

rectifier, with the alarm across the output. The zener diode across the alarm limits the maximum voltage and the electrolytic capacitor provides smoothing.

The value of C1 depends on the type of alarm used and its current drain. As an example, for the popular "Murata" make, two 33 nF, 250 Vac rated capacitors in parallel gave reliable operation. Current drawn was around 5 mA. This gave about 8 Vdc across the alarm and adequate sound output.

Not that C1 must be rated for 250 Vac operation.

# Any ideas?

Have you had a bright idea lately, or discovered an interesting circuit modification? We are always looking for items for these pages so naturally, we'd like to hear from you.

We pay between \$5 and \$10 per item — depending on how much work we have to do on it before we publish it.

The sort of items we are seeking, and the ones which other readers would like to see, are novel applications of existing devices, new ways of tackling old problems, hints and tips.

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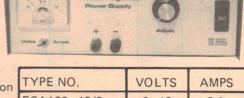
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# Catamarans-dolphins of the wind



For the first time 'Modern Boating & Seacraft' will have a huge Catamaran supplement (the first of three supplements) in the May edition.

This issue features the under-15 foot Cats with:

- Articles by Australian International Cat Skipper, Graham Candy.
- For new cat sailors a comprehensive feature on the comparison of the different cat classes.
- Results of tests on ten of the best catamarans available.



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# Shoparound

THIS PAGE is to assist readers in the continual search for components, kits and printed circuit boards for ETI projects. It also serves to bring new, special or hard to get components to the attention of the reader. If you are looking for a particular component or project from this month's issue — check with our advertisers if it is not mentioned here. Also, for a list of suppliers who stock the ETI projects published over the last few years, our "Kits for Projects" page may generally be found on the pages immediately preceeding the DREGS page (inside the back cover).

As we expected the 140W Valve Amplifier to be a popular project, we sent preliminary notification of the specialised components to kit and component suppliers early in March so that they could ensure stocks by the time this issue was published. The transformers, as you would expect, are hardly 'stock' items and the manufacturers — Ferguson Transformers Pty Ltd — indicated that, initially at least, they would only be making them to order. Substitute transformer, unless made to the same specification, should not be used, otherwise the project may

not have the same performance as our prototype.

Most of the kit and component suppliers we contacted indicated they would be stocking up for the project. You should have little difficulty locating parts, if not complete kits. We should warn you however that transformers may not be available until midto late May, depending on when suppliers may have ordered them

The ETI-325 Auto-probe should be another highly popular project. All the components can be obtained virtually 'off-the-shelf'. To house the unit, you'll either have to rat through your medicine cabinet for a suitable pill bottle, or purchase one from your local chemist.

Readers should have little difficulty locating components for the ETI-560 Mains Cable Seeker. As with the Autoprobe, all components are off-the-shelf items. Our telephone pickup coil was obtained from Dick Smith. It's listed as catalogue number C-7300.

The little magnetic earpieces are widely available. Don't make the mistake of getting a crystal type, though — it will not work in this circuit.

The S100 Motherboard ties all our

previous (and forthcoming) S100 computer projects together. All components are readily available. You might have to shop around a bit to get the best price for the S100 sockets, though!

# PRICE ESTIMATES

We must stress that the price estimates given below are just that — estimates. Instances have been reported to us of readers going into a supplier and, finding a kit priced above the estimate given in the magazine, berating the supplier for not sticking to our "recommended price", or words to that effect.

These are not recommended prices. We cannot, and would not, suggest a supplier sell a kit at the particular price given in this column.

We commenced publishing this information at the request of readers. Please keep in mind that 'typical' retail prices of components have been used to calculate project costs. Also, these may have been calculated as much as six to eight weeks in advance of publication and price movements may affect the result. We aren't infallible, and although every care is taken to see that these price estimates are reasonably correct, errors may creep in.

Please don't abuse your supplier — he's really trying to be helpful!

ETI-456 140W Valve Amplifier

\$220 to \$280

(depending on chassis and case)

ETI-325 Auto-probe \$5 to \$7 ETI-560 Mains Cable Seeker \$12 -\$16 ETI-636 S100 Motherboard \$90-\$110



To get the maximum in hum suppression in your homebrew hi-fi amp, a toroidal transformer is recommended. This one suits the Series 4000 amp (with slight mods to the power supply). It delivers 30 V + 30 V @ 2A (240 Vac pri.) and costs \$43.50 from Electronic Agencies, 115-117 Parramatta Rd, Concord NSW, 2137.

# ELECTRONICS

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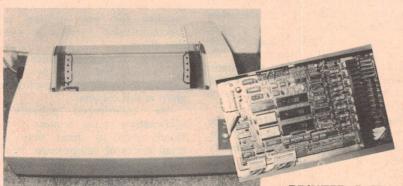
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In macroassembler and linking loader, nigner level languages and application programs.
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#### Dear Sir,

I would like to point out a serious deficiency in the design of the ETI-455 Loudspeaker Protector published in the March 1980 issue of ETI.

Protection circuits of this kind should be designed as far as possible to "fail safe". If the protection circuit fails,

- (i) it should not cause damage to the circuit being protected
- (ii) damage to the circuit being protected should be prevented, even while the protection circuit is failed
- (iii) warning should be given of the failure of the protection circuit.

While a failure of the Loudspeaker Protector will not cause damage to the loudspeakers, it will allow the speakers to be damaged and it will provide no warning that the protector has failed. Though this situation may appear no worse than not having the protector installed, the user is living in a fool's paradise having been lulled into a false sense of security by the presence of the protector. The first indication he is likely to receive of failure of the unit is a puff of smoke from his burnt out speakers!

While component failures and bad connections are possible failure causes for the protector, the most worrying cause of failure is a flat battery. The battery is permanently connected into the circuit (without switch), and it is stated that because of the low CMOS current drain the battery should last its shelf life. But how do you know when the battery needs changing — look for the puff of smoke from the speakers?

The most obvious way of making the speakers safe in the event of failure of the protector is to have the relay which controls connection of the amplifier to the speakers connected as a normally operated relay. Then a fault would cause the relay to drop out and open the amplifier-speaker connection. This would protect the speakers and provide warning of the protector failure (though there would still be some faults which could lock up the relay and prevent the protector from doing its job).

Unfortunately, the design as it stands using a battery as power supply is not suitable for continually holding in a relay. To provide best protection the Loudspeaker Protector would have to be mains powered and switched on with the amplifier. A delay of one to two seconds after switch-on before operation of the relay to connect the speakers, would protect the speakers from amplifier failure at switch-on.

David L. Craig Holland Park, QLD



Thank you for your comments on the ETI-455 Loudspeaker Protector Mr Craig, but there really isn't a "serious deficiency" in the unit, as you say, and I will let the designer, David Tilbrook, take issue on that score

Apart from the obvious first requirement of actually doing the job required, a project must be 'reproduceable' — that is, a wide spectrum of readers, with differing construction capabilities, must be able to build the project and get it working with a minimum of fuss. This is especially true of relatively simple projects and/or projects having wide appeal.

Having made that clear, I'll let David answer your specific objections.

(Roger Harrison, Editor)

When setting out to design this project, it was clear that it would have quite a wide appeal — as there was no commercial equivalent to do the job — and would probably be a 'beginning' project for many readers. It was for these reasons that I decided the circuit should be battery operated. Various protection schemes were considered actually, and rejected for reasons Roger Harrison has mentioned above — including 'signal powered' protectors, circuits powered from the amplifier's supply, etc.

Having chosen battery operation, the unit had to have minimum power consumption to obtain maximum battery life and this meant a 'normally off' relay. Whilst I agree with your sentiments expressed in (i), (ii) and (iii) in your letter Mr Craig, I cannot agree that the Loudspeaker Protector suffers from a "serious deficiency". Firstly, to check the battery one simply turns down the sensitivity control of the unit while using the amplifier at normal listening levels. If the relays operate, cutting off the speakers, the battery is obviously OK.

Problems arise if the Loudspeaker Protector is mains operated. One of the most likely times for an amplifier to go faulty is at the moment of turn on. Unless the Loudspeaker Protector has been turned on before the amplifier, it is totally useless as a protection device in this event.

With 'normally operated' circuits, a

fault condition can occur which 'holds on' the relay and it is fallacious to think that such a circuit is inherently "fail safe". Then again, 'normally operated' circuits are prone to somewhat more failures than 'normally off' circuits undoubtedly, some of those failures will be of the undesirable type.

For the conditions under which the Loudspeaker Protector will be built and operated, I think it should do its job admirably.

David Tilbrook.

#### Dear Sir,

I have been a regular reader of ETI since it first hit the newstands. I would like to congratulate the staff at ETI on the facelift given the magazine since last June.

My favourite section is Sound. It helps compensate for the demise of your sister magazine, 'Hi-Fi and Music'. However, I have one main criticism of the Sound section in ETI — lack of editorial and reviews on Australian-manufactured hi-fi equipment. The same goes for other Australian electronics and hi-fi magazines, too.

Could I suggest that ETI set aside a page or two for editorial and reviews on locally-made equipment?

Yours Faithfully R.D. Rowlands Koolan Island, W.A.

We'd be delighted to do that. However, the pages would be blank for most issues of the year! There are not too many companies producing hi-fi equipment in Australia. We have already reviewed the locally-made "Sirius" loudspeakers from the Philips organisation and have several other pieces of equipment "in the pipeline". From time to time we publish items on Australianmade hi-fi equipment in the "Sound News" pages — keep reading, items of interest will pop up in the future.

If any Australian manufacturers out there would care to submit equipment for review, we'd only be too happy to hear from you.

# Dear Editor,

I just loved the April catalogue — but what you had wrapped round it was terrible!

D. Smith North Ryde, NSW



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# ANNOUNCING 680000 DEVELOPMENT SYSTEMS

The EXORmacs Development System for 68000 has just been announced. The system includes 15 slot chassis and power supply, MPU module, memory management module, deBUG module, 128K byte dynamic memory module, and an intelligent floppy disk controller module.

Software includes Structured Macro Assembler/Linkage Editor, screen based editor, symbolic deBUG and a PASCAL compiler.

Peripherals include intelligent CRT console, a 1 Mbyte, two drive double sided floppy disk, and a model 703 (180 CPS 132 column) line printer.

A large number of support modules are also available.

# 6800/6809 EXORciser Development Systems

The popular EXORciser II Development System is now available in both 6800 and 6809 versions. For those people already owning a 6800 EXORciser or EXORterm Development System, a 6809 upgrade kit is available. Both EXORcisers may be expanded to allow development of the

MC6802/MC6808

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# Printout

# Two local firms win design awards

Two local electronic companies — BWD Electronics of Victoria and Fairlight Instruments of NSW — have been presented with design awards by the Australian Industrial Design Council.

Fairlight Instruments were presented with the Industrial Design Award for development of the Qasar general purpose computer.

This computer features dual 6800 microprocessors in the central processor which enables the machine to think at the same time as it reads or talks to the outside world or the memory. The 6800s are clocked alternately at the maximum rate of 1 MHz and share bus and memory. The resulting speed is effectively more than twice as fast as a conventional microsince delays due to interrupts

are avoided. The Qasar applications to date include small business computers, communication data processing, industrial control and music synthesis (the Fairlight Computer Musical Instrument — CMI).

The most striking application of the Qasar is in the CMI, produced by Fairlight, where the speed is fully utilised to control the pitch, harmonic content, and envelope shape of up to eight independent sounds played simultaneously. The sounds may be prerecorded natural sounds stored in the memory, or electronically gen-



Above: Kim Ryrie, a partner in Fairlight Instruments, accepts the Design Award. Below left: the Qasar twin-processor computer.





Above: John Beasley, designer of the BWD-880 Powerscope, with the award-winning instrument.

erated sounds. The CMI is designed to be programmed by a musician with no knowledge of electronics and this is achieved through the use of a light pen and video display. The musician chooses the pitch of a sound using a separate keyboard with its own microprocessor, he then draws the envelope shape of the fundamental and up to the seventh harmonic on the video screen with the light pen. This modified sound is stored in the memory and can be played on the keyboard at any pitch. The amplitude of the sound is determined by the speed of depression of the key and it repeats until the key is released (sustain").

The CMI includes 210 K of RAM, two double-sided 8" (200 mm) floppy discs, keyboard, VDU and light pen. It sells for about \$23 000.

BWD Electronics received the award for the BWD 880 Powerscope on the basis of originality of design and safety of operation.

The Powerscope is an oscilloscope designed for examining waveforms in ac and dc power supply and control circuitry. It features an insulated cabinet which has been tested to withstand over 5 kV and shrouded probes which will accept trans-

ients up to 3 kV. The BWD 880 will measure signal levels as low as 100 mV and up to 600 V RMS or in dc supplies to plus/minus 500 V across circuit components directly connected in three-phase powerlines. Maximum measurement range is from 100 mV to 1 kV, with accessories provided to extend this range to plus/minus 2 kV dc or 1.5 kV RMS continuous operation.

A unique feature of the Powerscope, according to BWD, is its ability to provide the user with digital readout of phase angle between a zero crossover reference marker and a variable marker. This can be adjusted from zero degrees to 359 degrees in one degree steps. In addition, the reference marker can be repositioned in multiples of 60 degrees to provide immediate phase angle relationships in two-three-six-phase systems. Time measurement can be made from 100 nanoseconds to 100 seconds with triggering extending from dc to 10 MHz, say BWD. Vertical input bandwidth is specified as dc to 7.5 MHz.

Since its release, the Powerscope has become widely accepted in industry and education, both in Australia and overseas.

# Micros invade the office

An exhibition of modern office products, featuring digital and computing equipment, was held in Sydney recently.

Called the 'Modern Office USA Exhibition', it was held at the US International Trade Centre in North Sydney over 18-21 March.

We went along to the exhibition armed with the knowledge that Australian companies are expected to spend \$612 million a year on office automation by 1982, nearly double the \$311 million spent in 1978. We wanted to find out why.

Our most dominant impression at the exhibition was the flood of minicomputers and word processors being sold by many of the 56 US companies and their 24 Australian distributors.



This inexpensive line printer, from MPI, was shown by Sigma International.

In addition, there were microprocessor controlled mail sorters, duplicaters, printers, filing systems, communication terminals, etc together with software to re-train the office staff for more productive work after automation has taken over the tedious repetitive jobs.

Unfortunately it's not possible for us to mention all the products being demonstrated at the exhibition. Sorry.

We were interested in the 'ultimate computer game' by Ardac Inc. of Ohio and demonstrated by Scandic International of North Sydney.



The Remington NBI System 3000 'paperwork processor' was typical of the many word processing machines exhibited at the Modern Office USA Exhibition.

The machine is an "electronic note acceptor". If you win, the computer pays you money but if you lose, you go to gaol! (DO NOT pass go, etc ...) If you are honest the \$1 or \$2 note acceptor gives you change in 10¢ pieces so you can carry on playing the pokies with the minimum interruption. But, if you are criminally-minded you are going to have a hard job 'winning'. The machine identifies good notes by two methods: first a small spot of light scans the engraving in two places about one-third and then two-thirds up the note and a photodetector produces data pulses as the spot passes over the engraved lines. The spacing of the pulses are compared with those in the memory of the microprocessor.

The notes are then scanned by an infrared absorbtion detector which checks the composition of the paper and its colour against a pattern in the memory.

We were assured that the machine always pays change for good notes and always spits out the bad ones.

Well ... we shall see, because these money changers are going to be around in many clubs, hotels etc soon, we were told

Some of the highlights of the exhibition were:

•Vector Graphics and their distributors AJ. and J.W. Dicker of Caringbah, NSW demonstrated their System B and Memorite 2 systems which allow simultaneous word and data processing from up to five independent terminals for under \$15 000 (reviewed last month).

•Commodore Business Machines and Hanimex of Brookvale NSW were playing the lunar lander game on their PET computer when I interrupted to enquire about the CBM3000 micro. This series consists of a CPU with 32K of memory plus a 1000 character display and keyboard, dual floppy disk drive and 70 lines/min dot-matrix Printer.

Aimed at small business users the 3000 series has full software support and on-site maintenance contracts will be taken by STC. It should be good value if you have \$10 000 or so to spare.

•International Computers Inc and ICL (Aust) of North Sydney were prominent with their minicomputer System 120. This system has a fast, efficient mini as the processor and new integrated front loading disc drives and microprocessor controlled VDUs and printers. This system should be of interest to medium size business users since it has expansion capabilities of up to 50 output terminals and up to 156M of disc memory.

•Mr. Arun Pande of Sigma International offered to help me, and any potential buyer, through the maze of US computer products being offered in the marketplace. Sigma is the leading US International distributor of microcomputers and peripherals and information, US export licence aid, rapid delivery from stock, spare parts, and large discounts from a very wide range of products.

•The future developments in office equipment will require even more powerful central processing than the current 8-bit microprocessors offer. Zilog had their 16-bit Z8000 series out of wraps and an evaluation board is available to prospective users

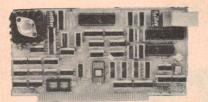
The board has the Z8000 MPU, 2K EPROM, 16K RAM, 32 I/O lines, four programmable 8bit counter/timers etc. A great deal of software has been already developed to back up the Ž8000 series and this evaluation kit should be invaluable to Australian companies wanting to keep abreast of latest developments in microprocessors.

A fascinating show.

John Pollard.

# **ELECTRONICS BY MAIL**

# Z80 SINGLE BOARD COMPUTER



#### (Offer closes 15/6/80) 20 for \$1.00. I IN914 diodes 20 for \$1.50. IN4004 diodes 10 for \$1.50. RED leds ...... 4 for \$1.00. 555 Timers 8 for \$11.25. 2102 RAMS 2 for \$10.75. 2114 - 450. ........ 4116 – 300. . . . . . . . . . . . . 8 for \$89.50.

VOLUME SPECIALS

Build your own Z80 based home computer using the ETI/DGZ80 as described in ETI November 1979. Designed by David Griffiths, this is probably the most powerful S100 Z80 magazine project described to date.

Features include on board P10 (dual 8 bit 1/0), CTC (4 channel programmable counter timer), power on jump, software write protect option, provision for 2K ROM on board, 1K RAM for stack, scratchpad (expandable to 2K) top quality solder masked plated through PCB, sockets for all IC's and comprehensive Owners Manual.

DG Z80 (kit)	\$199.25	tax paid.
(kit)	175.00	tax exempt.
(assembled)	240.00	tax paid.
(assembled)	215.00	tax exempt.

# DGOS OPERATING SYSTEM

Monitor ROM for above DG Z80 strongly recommended for use with DG 640 VDU. Powerful monitor includes tape loading/dumping real time clock, software write protect, memory examine, alter, compare, move and fill commands. 2716 EPROM with listing \$48.00.

# DG 640, VDU

This has to be the most popular VDU in Australia. Described in ETI March 1978, the DG 640 features 16 lines of characters, upper/lower case with graphics, crystal locked self contained TV scan circuits, top quality plated through PCB with Owners Manual.

50 040 /1:-1	4400 50	
DG 640 (kit)	\$139.50	tax paid.
(kit)	125.70	tax exempt.
(assembled)	149.50	tax paid.
(assembled)	134.25	tax exempt.

NOTE: ALL PRICES INCLUDE SALES TAX (Except where noted)

# **DREAM 6802**

Described in EA May 1979, this kit has been redesigned to accept the 6802 chip and eliminate the problems with the 6875 IC. The Applied Technology DREAM 6802 includes all IC's, components, keyboard modulator and power supply, together with a comprehensive MANUAL and simple program to run. DREAM 6802 (kit) \$149.50 tax paid.

# **CRYSTALS**

1MHz	\$12.50.
4MHz	7.95.
8 MHz	7.95.
12 MHz	7.95
(Small stocks of	other values.)

# ZENER DIODES 1w.

ALL VALUES 25¢. 3V3, 3V6, 4V7, 5V1, 5V6, 6V2, 7V5, 8V2, 9V1, 10V0, 11V0, 12V0, 13V0, 15V0, 16V0, 18V0, 20V0, 22V0, 24V0, 27V0, 30V0, 33V0.

# WIRE WRAP

JUST WRAP KIT	\$32.15.
WSU-30w. WIRE WRAP TOOL	8.75
WIRE WRAP WIRE 50 ft. spoo (red, black, blue, white)	ols. 2.75.
WIRE WRAP TRIPLE PACK DISPENSERS	8.75.

# MICROPROCESSOR COMPONENTS

Z80 CPU	\$15.75
Z80 PIO	9.75
Z80 CTC.	9.75
2650A.	15.75
2608 PIPBUG	15.75
2651	19.75
2708	12.50
2716 (+5V)	45.00
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2102-350	1.55
SC/MP II	9.75

# SOCKETS

	Solder	Wirewrap
8 pin	.20€	.46¢
14 pin	.25	.54
16 pin	.28	.67
18 pin	.29	.80
20 pin	.30	.92
24 pin	.35	\$1.44
28 pin	.40	1.84
40 pin	.50	1.90

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RED									
GREEN .									
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1a Pattison Avenue, Waitara 2077.

Hours: 9-5 Monday to Saturday. Telephone: 487-2711.

# Printoul

# Bar code printer

Anderson Digital Equipment have just released the Intermec 8220 bar code printer. This unit is a low-cost electronically-controlled serial impact printer which produces high quality, random, batch or sequential runs of CODE 39 (r) labels or tags.

A basic two-line printer, the 8220 prints bar code with an interpre-

tation line and one line of free text.

The highly reliable printing mechanism consists of a continuously rotating print drum and electromagnetically actuated print hammers. Solid state devices optically sense print drum position. The appropriate bar code and character images are optimally distributed around the print drum.

Labels and tags are printed by the 8220 using a dry carbon ribbon which produces printed bars with high optical contrast and sharply defined edges of maximum scanability. Data input is through an

RS232C interface.

For further information contact Anderson Digital Equipment Pty Ltd, PO Box 322, Mt Waverley, Vic; (03) 543-2077 or PO Box 294, Ryde NSW, (02) 808-1444.

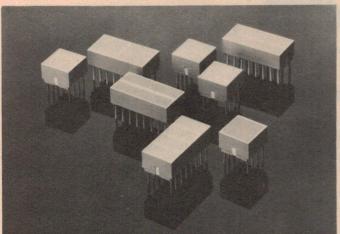


The Sord Microcomputer Users Group announced their formation recently.

They are actively seeking members with a view to getting into all the usual club-type activities.

Prospective members and interested persons are asked to

**Emmanuel Cargakis** 4/8 Clarkson Avenue **Brighton Vic 3186** 



# New LEDs from HP

area annunciator messages is now easily possible by using a new family of light emitting diode light bar modules from Hewlett-Packard.

These new modules provide large, bright and uniform light emitting surfaces and come in sizes 9 mm square and 9 mm x 19 mm surface areas. Other packages have multiple surface from Hewlett-Packard direct.

Backlighting large surface areas and come in red, yellow and green.

These modules will be useful for illuminating legends, indicators, bargraphs and switches. Prices range from \$1.96 for the small package to \$2.87 for the large one.

Further information can be obtained from Cema Electronics Pty Ltd, 21 Chandos Street, St Leonards NSW, or



# New utility for keyboard intelligence.

A new CP/M utility has been specially written to convert any keyboard into an intelligent keyboard.

The program, written by Dennis Riepon of AED, is similar to DESPOOL in that it loads automatically below the CCP. It is compatible with all versions of CP/M and operates correctly with XSUB and DESPOOL.

Price is about \$25 and further information can be obtained from Acoustic Electronic Developments Pty Ltd, 123 Military Rd. Guildford NSW 2161. (02) 632-6301.

# Perth computer club

A Perth computer club has been hiding its light under a bush.

The club has been active for about five years and has now 100 active members and 100 members who only play computer games. The club room, in the Undergraduates' Guild building of the University of Western Australia, is open about 23 hours per day and offers the

use of two computers.

Occasional classes are held on Saturday mornings for learning about software and the use

of computers.

Further information can be obtained from the University Computer Club, room 2.17 Guild Building, c/o The Guild of Undergraduates of Western Australia Crawley WA 6009. (09) 380-2297.

# **New recorder for Digital**

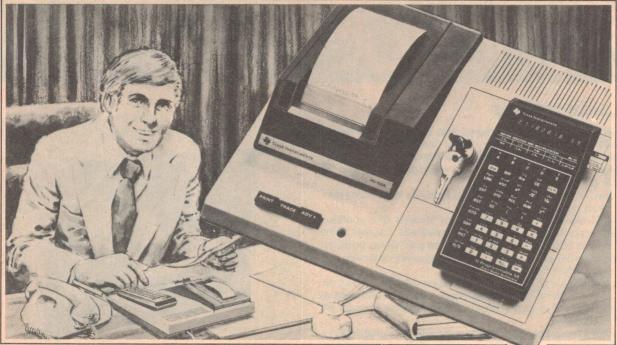
Epicom Inc of the USA has released its model EI 200 epitape recorder here through the Dindima Group.

This unit is a fully portable system capable of recording digital communications data regardless of the line discipline in force at speeds up to 960 bps. Without control and status recording the unit can handle speed up to 19 200 bps.

A four-digit tape position indicator allows precise location of

communications errors.

Further information can be obtained from The Dindima Group Pty Ltd P.O. Box 106 Vermont Vic 3133.



# Now the business professional has an extra-ordinary programmable calculator from Texas Instruments.

# Powerful but simple

The TI-59 gives you so much problem solving power it's almost like a handheld computer. Yet it's extremely easy to use.

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You can slip a pre-written programme module in your TI-59 calculator and instantly transform it into a sophisticated application computer. There's a tool kit of pre-programmed solutions to a wide variety of problems. TI's plug-in Solid State Software™ libraries have been designed by professionals for use with your TI-59.

Containing up to 5.000 programme steps TO SOLVE BOTH ROUTINE AND COMPLEX PROBLEMS THESE LIBRARIES INCLUDE:-

- ☐ Applied Statistics
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- ☐ Securities Analysis
- ☐ Real Estate/Investment

And many others. For instance Marine Navigation and Aviation are commercial programmes you can also use for your time away from the office.



# An aid throughout your business

The problem solving capacity of the TI-59 can be used right across your company. Sets of programmes for specialists in many areas are available in Speciality Pakettes and include:—

- ☐ Marketing Sales
- ☐ Production Planning
- ☐ Programming Aids
- □ Oil/Gas/Energy
- Statistical Testing
- ☐ Securities Analysis

# Programming is so simple

You can use pre-designed programmes, write your own, or incorporate both. With the TI-59's advanced technology YOU CAN MODIFY AND EDIT YOUR PROGRAMMES AND STORE THEM ON MAGNETIC CARDS FOR RE-USE.

# You'll use the TI-59 continuously in business decisions

For instance the problem solving capacity of its 100 memories or 960 programme steps is invaluable for Budgets, Statistical Analysis, Stock Options and Chain Calculations. And you can turn TI-59 into a printer-calculator which prints, lists and traces your programme with the PC-100C Printer/Plotter Accessory.

# And at \$349.00\* TI-59 costs so little

while your optional PC-100C Printer/Plotter Accessory is just \$285.\*

Examine TI-59's many remarkable features.

YOU CAN USE IT'S PROBLEM SOLVING POWER NOW





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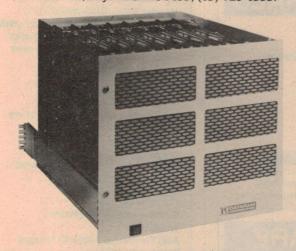


# Static ROMS from National

A complete family of static 16K, 32K, and 64K ROMS with JEDEC approved pin configuration is now available from the National Semiconductor Corporation.

All are TTL compatible and operate from a 5 V supply and are available in 24 pin packages.

Further information and prices can be obtained from N.S. Electronics, P.O. Box 89, Bayswater Vic 3153, (03) 729-6333.

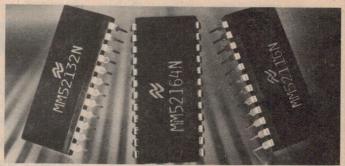


# **◆ Eight code bar reader**

A new bar code reader has been released by Anderson Digital Equipment Pty Ltd which can read up to eight popular bar codes.

The unit comes complete with an Intermac model 1236 light pen but other wands are also available. The unit is small in size to save work space (229 mm x 152 mm x 25 mm) and can be easily mounted on the underside of a work table.

The model 9300 ranges in price from \$1090 to \$1485 depending on the choice of wand or scanner and further information can be obtained from Anderson Digital Equipment Pty Ltd, P.O. Box 322, Mt Waverley Vic 3149. (03) 543-2077.



# Bulk store for the PDP-15

Anderson Digital Equipment recently announced the release of the Dataram BC-205 bulk core system for the Digital Equipment Corporation's PDP-15 series of minicomputers.

The BC-205 is compatible with the DEC RF15/RS09 fixed head disk system and is completely software compatible with the standard operating systems and RF-11 diagnostics used on the PDP-15.

The bulk core system, functioning as a fast access peripheral, can provide dramatic improvements in system handling to bring the PDP-15

more in line with the performance of currently available minicomputers.

Cost varies from \$32 125 for the minimum 256K words to \$63 500 for a full megaword (1024 x 18).

Further information may be obtained from Anderson Digital Equipment Pty Ltd, P.O. Box 322, Mt Waverley Vic 3149 (03) 543-2077.

Amateur Radio System Comproc.....

ELECTRIC PENCIL

# TRS-80 OWNERS!! FREE WITH NEWSLETTER

L2 cassette (1 Game, 1 Business) to celebrate 11/2 years. Subscription \$12/year. Write Box 105, Marrickville 2204.

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8K Expansion board, complete, less RAM. Daisy
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See March '80 ETI for price list of 47 varied software programs.

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Instructions:								
1.10	Reverse Video Instructions\$3.00							
Catalogue:								
C.1	Brief outlines of the above programs, in-							
	cluding previous list Free hints on prog-							

APOLOGY - U.8 Cursor Control was incorrectly advertised at \$5.95. It should have been \$9.95. We are sorry for any inconvenience caused by this error.

ramming and use of OSI computers are

included.....\$2.95

Notes - All tapes have two copies of the program, one on each side. Printed listing is also included. 'Tone' and 'Volume' controls may need adjusting. Both FULL 'SAVE' and 'LOAD' is usually



LOOKY VIDEO PO Box 347 Richmond, Vic, 3121 Allow postage, eg OSI Software

MAIL ORDER:

3-5 \$1.50, 6-10 \$2: 10 or more \$2.50

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6800 (Exorciser bus) SM Electronics Pennywise Peripherals

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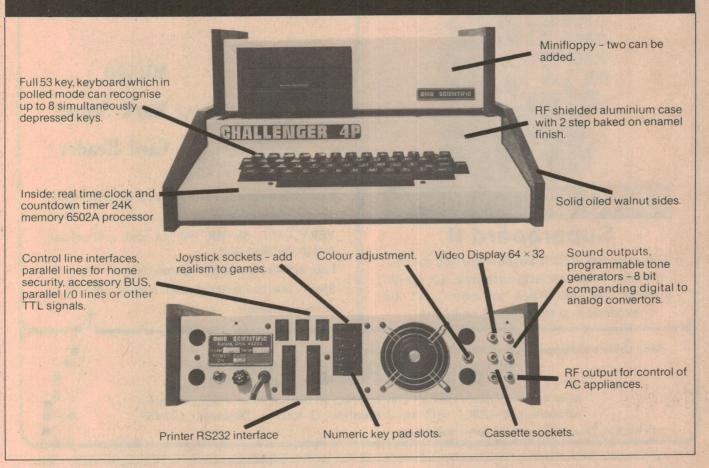
Computer Consultants, 3 Wolfe Street, Auckland. N.Z. Phone: 79-8345

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# The Challenger 4

Whichever way you look at it, no other computer offers so much for so little, and in colour!



You'd have to go a long way to get better value in a computer. It has execution speed that really separates the computers from the toys. We think the Challenger 4 is way ahead of anything you've seen so far, for a wide variety of uses including business, personal, educational and games, as well as a real-time operating system, word processor and a data base management system.

The Challenger 4 has a 2MHz 6502 processor, and if that's not fast enough we can supply the GT option with the 6502C processor, and 120 nanosecond memory which averages over one million instructions per second.

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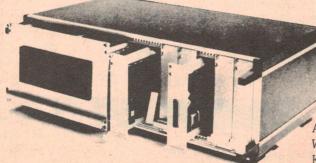
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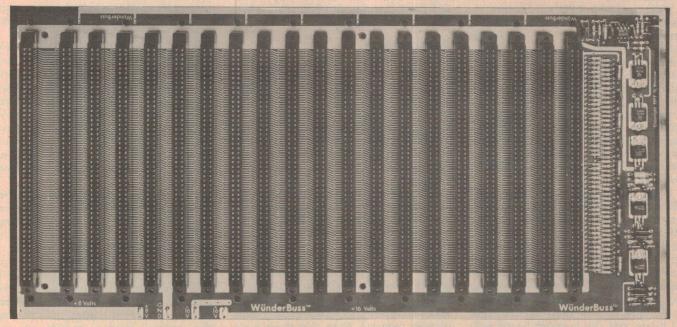




# Update on the S-100 bus

What with the arrival of 16-bit micros and the increased demands being placed on computer systems, the S-100 bus has had a grease and oil change . . . enter at sINP, exit at sOUT you you'll know what it's all about!

Les Bell



THE ALTAIR 8800, which introduced personal computers, has long disappeared from the market, but its ghost lives on in the form of the Altair (now renamed S-100) bus which linked its various printed circuit boards together. When the S-100 bus was designed, the only second-generation microprocessor available was the Intel 8080, and the bus was designed around the signal definitions and timing of this particular microprocessor.

Today, things have changed considerably. The 8080 is, itself, rather passe, and most recent processor card designs have been based on the Z-80, 8085 and 6809. In the last few months, too, a new range of 16-bit processors have appeared on the market, and manufacturers have been eager to shoehorn these big machines into what was designed as an 8-bit bus. For these reasons, in order to maintain compatibility with existing S-100 cards (why else go S-100?), it has become necessary to closely specify the functions of the S-100 signals, together with their timing, as well as extend the bus to handle the 16-bit data and 24-bit address buses of the new processors.

A subcommittee of the IEEE Computer Society Microprocessor Standards Committee, led by George Morrow (Thinker Toys), Howard Fullmer (Parasitic Engineering) and Kells Elmquist (Intersystems), has been working on the definition of the bus for some time now, and has published two reports in the IEEE Computer magazine for comment before the final proposal is submitted to the IEEE Standards Board. Reprints of the latest article, in the July 1979 issue of Computer, are available from the IEEE, 345 East 47th Street, New York, NY 10017, for US75c plus postage.

The proposed S-100 standard is listed in Table 1. Note: this is still a preliminary draft and is subject to change. The other point is that it isn't as simple as it looks — this only shows which signal is on which pin, and briefly what its function is. It does not show the protocol for interchanging between bus masters, for sixteen-bit data interchanges and the other subtleties and complexities appertaining to the bus.

# Changes, always changes

From a purely mechanical viewpoint the major change brought about by the new standard is the redefinition of some of the old S-100 signals. Pin 98, for example, is no longer SSTACK, an output from the processor that indicates when it is accessing the stack. Instead, it is an input to the processor which indicates a parity, or similar, error in the current bus cycle. Owners of old CPUs

The 20-slot S-100 motherboard from George Morrow's 'Thinkertoys' company features active termination and "guarded" microstrip interconnecting rails to eliminate crosstalk and signal propagation problems.

which generate SSTACK who buy parity-checking memory will have to disable one of these functions.

Other signals have also disappeared — and a good thing, too, as the redundancy of the old bus was the source of many of the incompatibility problems the new standard will solve. It is left to the reader to make a comparison with the old standard — if you own a system and wish to upgrade and take advantage of the new facilities you'll have to acquire a fairly thorough understanding of the bus operation anyway.

The biggest change that is obvious from the pin list is the addition of an extra eight address lines, A16-A23. These enable S-100 systems to take advantage of the large addressing range of the new 16-bit micros without inelegant paging schemes. Now systems can include multiple 64K memory boards without the need for bank select software, and memory can be accessed faster.

The next big change in the specification is the introduction of a protocol for the transfer of 16-bit words

over the bus. The old S-100 bus had two unidirectional data buses — the data in (DI) bus, over which data and instructions are read from memory, and the data out (DO) bus, which carries data to be stored in memory. The new bus still uses this system so that it will work with existing memory gards, but is extended to cope with the 16-bit processors.

When a 16-bit CPU card wants to read a 16-bit value (or instruction) from memory, it puts out the required address and control, status, etc signals, and also pulls the sXTRQ line low. This indicates to the memory card (if it is 'listening') that the CPU is willing and able to conduct a 16-bit data transfer. If the memory is able to do the same, it signals this fact by pulling the SIXTN line low. If it is an 'old' card which does not examine the sXTRQ line, then nothing will happen on SIXTN, obviously.

If the memory is 16-bit oriented, it will enable its tristate output buffers onto both the DI and DO buses, and the CPU will accept inputs from both these buses. In effect, the DI and DO buses are parallelled into a 16-bit bidirectional data bus. On memory write cycles a similar procedure is followed, except that this time the processor board will enable bus buffers onto the DI and DO buses, and the memory board will accept input from both. The combined buses, when used in this way, are referred to as the DATA bus.

If the memory is only eight bits wide, then the CPU board must split the word into two bytes and transfer them singly in the conventional manner. This is fairly simply achieved by using the bus buffers as a multiplexer, at the expense of some pcb real estate for the extra buffers and the sXTRQ/SIXTN control logic.

# Methodology

The other major change to the S-100 bus is simply the fact that it is now tightly specified, its terminology is defined and there is now a methodology for the design and implementation of equipment for the bus.

The bus is organised into eight sets of signals: the address bus (24 lines), the data bus (16 lines), the status bus (8 lines), the control output bus (5 lines), the control input bus (6 lines), the DMA control bus (8 lines), the vectored interrupt bus (8 lines) and the utility bus (20 lines). These buses carry two types of information: messages used to manage the interface system itself, called interface messages; and messages between boards connected to the bus that are not concerned with the bus itself (i.e.: data). These are called device

dependent messages.

The bus connects two different types of device: a bus master, and a bus slave. The master has control of the signals on the bus and is able to address slaves and communicate with them. A slave on the other hand, monitors all bus cycles, can be addressed by a master, and can communicate with masters. In general, a slave can communicate only when addressed (i.e. 'speak when it's spoken to').

# Addressing

Not only has the address bus been extended to 24 bits for memory accesses, but the I/O addressing range has been extended to 64 K, since the extended I/O device address bus is 16 bits wide. Note that processors are not obliged to make use of the extended address range — they can supply only the standard (i.e: 'old') address bits if required.

The eight status lines indicate what kind of bus cycle is in progress. The mnemonics for status lines always begin with a lower case 's'. They are: sMEMR (memory read), sM1 (opcode fetch), a sINP (input), sOUT (output), sWO (write — true on both memory and output writes), sINTA (interrupt acknowledge), sHLTA (halt acknowledge) and sXTRQ (16-bit data transfer request). Note that there is no memory write signal, and this must be derived by the following logic equation:

# sMemory Write = sOUT.sWO

That is, status memory write is true when sOUT is false and sWO is true (sWO is at logic 0).

The five lines of the output control bus are: pSYNC (start of a new bus cycle), pSTVAL (indicates stable address and status signals), pDBIN (read strobe), pWR (write strobe) and pHLDA (hold acknowledge). Note that the names of the control output lines all begin with a lower case p.

There are six input control lines. RDY and XRDY are inputs which cause the processor to generate wait states until both these inputs are asserted, to wait for slow memory for example. INT and NMI are the interrupt inputs to the processor. The HOLD line is used by temporary bus masters to request control of the bus from permanent bus masters. The sixth control input is SIXTN, which has been covered earlier.

The eight vectored interrupt lines are used in conjunction with the vectored interrupt request, INT, to arbitrate among eight levels of interrupt priorities. This can be done by a vectored interrupt controller either on the CPU board or on a separate card.

Eight lines are used for control of

DMA (direct memory access) operations. In a DMA data transfer, the CPU relinquishes control of the bus to another (temporary) bus master, which performs the data transfer and then returns control to the CPU. Some types of floppy disk controller, for example, use DMA data transfer, and therefore qualify as temporary bus masters. Under the S-100 bus DMA protocol, a temporary master which wants to gain control of the bus will examine the four bus arbitration priority lines (DMA3 -DMAO) to see if another temporary master is already asserting a higher priority - if one is, then no attempt should be made to gain the bus until the higher priority temporary master has been serviced. Otherwise, it should output its priority on the bus and assert the HOLD line. The master will then return the pHLDA signal, and the bus can be transferred to the temporary

The transfer of bus control is a rather tricky procedure, as both the permanent bus master and the temporary bus master must drive the bus at the same time, in a defined manner, so as not to generate false bus cycles. The bus transfer control circuit asserts ADSB, SDSB and DODSB, thus disabling the address, status and data output buffers of the permanent master and enabling the control output buffers of the temporaty master. Both masters are now driving the control output bus at at the same time, in a predefined state. Finally, the bus transfer circuit asserts CDSB, disabling the permanent master's control output buffer, and the temporary master now has control of the bus.

Once the temporary bus master has completed its business, bus control is transferred back to the permanent master by, basically, the mirror image of this process. The bus definition allows for up to 16 temporary masters on the bus, so there is plenty of scope for multiprocessor schemes!

# The utility bus

The utility bus includes all the other unrelated signals. There are the power lines, which are the same as before, with the addition of some extra ground lines. The system clock is no longer split into two phases, and is always generated by the permanent master. This clock controls the timing bus cycles, whether controlled by a permanent or temporary bus master.

The CLOCK signal, on the other hand, is a 2 MHz signal which bears no relation to any other bus signal, and is intended to be used by clocks, timers, baud rate generators, etc.

There are three system reset

# Table 1 — The S-100 Bus Signal Definitions

Pin No.	Signal Name and Type	Polarity	Description
1 2	+8 V (B) +16 V (B)		Supply
3	XRDY (S)	Н	Supply Ready input to bus master
4 5	VIO (S) VII (S)	L O.C. L O.C.	Vectored interrupt line 0
6 7	VI2 (S) (S)	L O.C. L O.C.	" " 2
8	VI4 (S) VI5 (S)	L O.C. L O.C.	" " 4
10	<u>V16</u> (S)	L O.C.	" " 6
12	NMI (S)	L O.C.	" 7 Non-maskable interrupt
13 14	PWRFAIL (B) DMA3 (M)	L O.C.	Power fail bus signal Temporary master priority bit 3
15 16	A18 (M) A16 (M)	H	Extended address bit 18 Extended address bit 16
17 18	A17 (M)	Н	Extended address bit 17
19	CDSB (M)	L O.C. L O.C.	Status disable control Control signals disable
20 21	GND (B) NDEF		Common with pin 100 Not defined
22 23	ADSB (M) DODSB (M)	L O.C. L O.C.	Disables 16 address bits Disables data out bus
24 25	φ (B) pSTVAL (M)	H	Master timing signal Status valid strobe
26	pHLDA (M)	H	Hold acknowledge
27 28	RFU RFU		Reserved for future use Reserved for future use
29 30	A5 (M) A4 (M)	H	Address bit 5 Address bit 4
31 32	A3 (M) A15 (M)	H	Address bit 3 Address bit 15 (most significant bit if non-extended)
33 34	A12 (M)	H	Address bit 12
35	A9 (M) DO1 (M)/DATA1 (M/S)	H	Address bit 9 Data out bit 1, bidirectional data bit 1 DAta out bit 0, bidirectional data bit 0
36 37	DOO (M)/DATA0 (M/S) A10 (M)	H	DAta out bit 0, bidirectional data bit 0 Address bit 10
38	DO4 (M)/DATA4 (M/S) DO5 (M)/DATA5 (M/S)	H	Data out bit 4, bidirectional data bit 4 Data out bit 5, bidirectional data bit 5
40 41	DO6 (M)/DATA6 (M/S) DI2 (S)/DATA10 (M/S)	H	Data out bit 6, bidirectional data bit 6 Data in bit 2, bidirectional data bit 10
42	DI3 (S)/DATA11 (M/S)	Н	Data in bit 3, bidirectional data bit 11
43	DI7 (S)/DATA15 (M/S) sM1 (M)	H	Data in bit 7, bidirectional data bit 15 Machine cycle 1 (op-code fetch)
45 46	sOUT (M)	H	Output data transfer cycle Input data transfer cycle
47 48	sMEMR (M) sHLTA (M)	H	Memory read cycle Halt acknowledge
49	CLOCK (B)	N 10 10 10 10 10 10 10 10 10 10 10 10 10	2 MHz clock
50 51	GND (B) +8 V (B)		Common with pin 100 Common with pin 1
52 53	-16 V (B) GND (B)		Supply Common with pin 100
54 55	SLAVE CLR (B) DMAO (M)	L O.C. L O.C.	Resets bus slaves. Must be active with POC Temporary master priority bit 0
56 57	DMA1 (M) DMA2 (M)	L O.C. L O.C.	Temporary master priority bit 1 Temporary master priority bit 2
58	sXTRQ (M)	L O.C.	Request for 16-bit data transfer
59 60	A19 (M) SIXTN (S)	H L O.C.	Extended address bit 19 16-bit data transfer acknowledge by slave
61 62	A20 (M) A21 (M)	H	Extended address bit 20
63 64	A22 (M) A23 (M)	H	" " " 22 " " 23
65 66	NDEF NDEF		Not to be defined Not to be defined
67 68	PHANTOM (M/S)	L O.C.	Disables normal slaves and enables phantoms pWR.SOUT
69	RFU	-	Reserved for future use
70 71	GND (B)		Common with pin 100 Reserved for future use
72 73	RDY (S)	H O.C. L O.C.	Interrupt request
74 75	HOLD (M) RESET (B)	L O.C.	Control signal to co-ordinate bus master transfers Resets bus masters. Must be active with POC
76 77	pSYNC (M) pWR (M)	H	Identifies BS1 Signifies valid data on DATA or DO bus
78	pDBIN (M)	H	Requests data in from slave
79 80	A0 (M) A1 (M)	H	Address bit 0 (least sig.)
81 82	A2 (M) A6 (M)	H	" " 6
83 84	A7 (M) A8 (M)	H	" " 7
85 86	A13 (M) A14 (M)	H	" " 13 " " 14
87	A11 (M) DO2 (M)/DATA2 (M/S)	H	" " 11 Data out bit 2, bidirectional data 2
88 89	DO3 (M)/DATA3 (M/S)	Н	Data out bit 7, bidirectional data 3 Data out bit 7, bidirectional data 3
90 91	DO7 (M)/DATA7 (M/S) DI4 (S)/DATA12 (M/S)	H	Data in bit 4, bidirectional data 12
92 93	DI5 (S)/DATA13 (M/S) DI6 (S)/DATA14 (M/S)	H	Data in bit 5, bidirectional data 13 Data in bit 6, bidirectional data 14
94 95	DI1 (S)/DATA9 (M/S) DI0 (S)/DATA8 (M/S)	H	Data in bit 1, bidirectional data 9 Data in bit 0, bidirectional data 8
96 97	SINTA (M) SWO (M)	H	Interrupt acknowledge Write cycle
98 99	ERROR (S)	L O.C.	Indicates error condition Power-on clear signal for all bus devices
100	POC (B) GND (B)		System ground

functions — RESET clears all bus masters, SLAVE CLR resets all bus slaves, and POC, which also asserts the other reset signals, indicates a power-up condition.

The PHANTOM line is used to locate two slaves at a common address — for example, a small block of ROM in the middle of a 64K RAM card. When PHANTOM is asserted, the RAM would be disabled and the ROM enabled, although they share the same address.

The PWRFAIL line indicates an impending power failure, enabling the processor, if suitably equipped, to save its status in a backup store such as CMOS RAM.

Three lines are not to be defined, and these are available for use by manufacturers, provided they are only implemented as options and provided with jumpers to eliminate possible conflicts.

# **Timing**

The bus is specified at up to 6 MHz clock speed, but most users will be pushing to get there. Some microprocessors are specified up to 8 MHz clock or higher, and these will probably use single-board computer configurations.

The basic bus cycle timing was originally derived directly from that of the 8080 processor, and so a basic understanding of the bus timing can be obtained from the relevant sections of the 8080 Microcomputer Systems User's Manual. In fact, almost all current 8080-based boards meet the timing specs without modification (excepting the bus master transfer and 16-bit operation, of course)

The bus is pseudo-synchronous in operation; the timing of the control signals bears a specified relationship to the master system clock. Each bus cycle accomplishes the transfer to one word (16- or 8-bit) between a master and slave, with the exception of master transfers. The beginning of a new bus cycle is indicated by the rising edge of the pSYNC signal, and shortly after this, the address and status buses will change their values for the new bus cycle. Shortly after they stabilise, the status valid strobe, pSTVAL, will indicate to all bus slaves that the address and status may be picked up from the bus.

Generally, bus cycles are either read or write cycles. There are four types of read cycle — opcode fetch (M1 in 8080 terminology), memory read, input and interrupt acknowledge. These cycles are all similar in timing but use the status bus in different ways. Write cycles — output or memory write — are basically similar.







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# **Bus Hardware — and Some Notes on Logic Design**

ALMOST ALL MICROPRO-CESSORS are manufactured using an n-channel MOS process, and this means that their on-chip output buffers are only capable of driving one TTL load and a few pF of capacitance. While this is sufficient to drive the inputs of a few memory and I/O chips directly (provided they are also MOS), it is certainly not adequate for bigger systems. A typical single-board controller based on the 8080A is shown in Figure 1, which shows that the low-order address lines only go to four MOS devices while the top six address bits go only to one address decoding device (although even this is redundant in such a small system).

When the processor, RAM, ROM, I/O and special functions are on separate cards, joined by a TTL-level bus of fairly large physical dimensions, several problems arise. Firstly, in a 22-

slot motherboard, the processor card may have to drive up to a theoretical maximum of 640 memory chips (assuming 20 cards each carrying 32 memory ICs). While this is an extreme example, someone, somewhere will probably want to do it!

Secondly, a large motherboard is around 460 mm long, which results in fairly large capacitances between adjacent tracks. In addition, this capacitance, coupled with the inductance of the tracks, will make the bus behave like a transmission line, with reflections from the end opposite the processor. Perhaps, as processors get faster, an SWR meter will become a standard part of the computer hacker's tool kit?

For these reasons, it becomes necessary to buffer the outputs from the processor, as well as the inputs to memory and other cards.

However, you can't just

connect the straight TTL outputs of the various cards directly onto the bus in a parallel arrangement. It is not sensible to connect together the outputs of two TTL gates; if one goes high and the other goes low, the output voltage will be indeterminate, and even worse, a large current will flow through the totem-pole output circuitry of both devices, resulting in the possible destruction of one or both.

Two types of TTL devices do not suffer from this limitation. The first is open-collector TTL, in which the output circuit of the IC is an open-collector transistor. With this type of chip, several collectors can be tied together, to a common pull-up resistor, which is typically 2k2 in value. In this case, the gates can only pull the output down, not up, and the output will only be high if none of the gates is pulling down. This is actually a NOR function, and the circuit is sometimes called a 'wired-OR'.

Open-collector logic was very popular with logic designers in the early seventies, but has now fallen from grace because of its three problems. Firstly, it is slow. When the output transistor is off, its collector junction looks like a capacitor and this has to charge up through the pull-up resistor on a zero-to-one transition. Secondly, noise increases as gates are wire-ORed. And thirdly, it is difficult and frustrating to fault-find, as one defective gate will make the whole circuit appear faulty.

The best type of logic circuit for bus circuitry is Tri-State logic (commercial break — Tri-State is a trademark of National Semiconductor). The output of a tri-state IC can assume three different states — logic 0, logic 1 or a high impedance state, in which the output is effectively disconnected from the following circuitry. Apart from the 'normal' complement of inputs, tri-state gates also have an output enable pin (usually pulled high to assert it true, i.e.: OE). When

this pin is at logic 1, the output is enabled and the IC behaves like 'normal' TTL 9 usually LS TTL), but when it is low, the output goes to the high impedance state.

The OE pin of the data out buffers on memory cards is usually driven by a signal derived the address decoder circuitry of the card in conjunction with the control bus indicate that a signals which memory read cycle is in progress. The control signals for buffers on other cards are derived in a similar way. On the processor card, the data, address and control bus buffers must be tri-stable to enable temporary bus masters such as DMA controllers to take over the bus.

Some bus signals are negative logic signals, that is they are true when the signal line goes to logic O. The reason for this is largely historical, and derives from the fact that negative logic on bus lines can then be implemented using open-collector logic. This also gives slightly better noise margins, and improved timing leeway, since inverting buffers are slightly faster than non-

inverting types.

In order to correctly terminate a transmission line data bus, it is usual to use a 180R resistor to Vcc and a 390R resistor to ground on each line. This gives an resistance of equivalent approximately 120R and a no-load voltage on the line of 3.4V. Some mother boards termination include active circuitry which uses a regulated supply and only single resistors to terminate the bus. Bear in mind though that the power supply lines, and certain other lines such as the reset line, should terminated. be termination is not necessary with buses less than 180 mm in length.

Several different types of buffer IC are available. Older cards use quad or hex tristate buffers, such as the 8T97. However, some excellent 20-pin octal parts are available now, but beware that there is a shortage of TTL throughout the octal and although the industry, seems to be situation now improving anything eight bits wide can be difficult to obtain.

Check out the DM8097 octal tri-state buffer (National Semi-conductor), the 74LS240 (octal inverting bus driver), the 74LS241 (non-inverting) and the 74LS245 (octal bus transceiver). These ICs save quite a bit of space on boards and simplify design quite a bit.

Hopefully, with the aid of all the foregoing you should now be able to tackle the design of the bus interfacing for cards in your computer system.

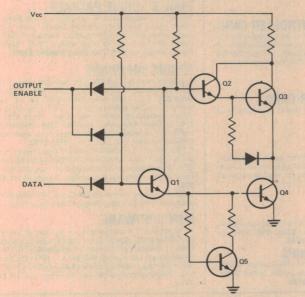
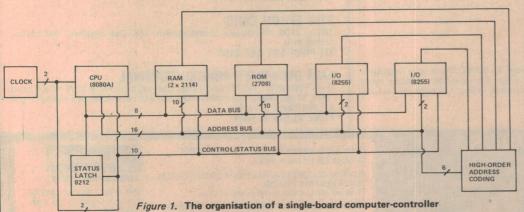
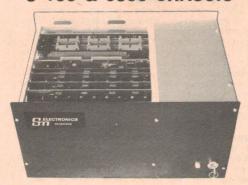


Figure 2. A typical tri-state buffer output stage. When OUTPUT ENABLE is brought low, both Q1 and Q2 are turned off, disabling the totem pole (Q3 and Q4).



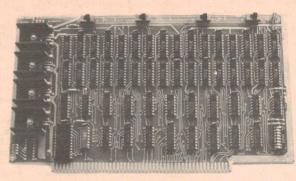
# **'THE S100 BUS STOP!**

# S-100 & 6800 CHASSIS



11 slot backplane, fully card guided. 15 amp power supply, fan, key switch, bench mount, rack mount, annodised aluminium. 5 edge connectors standard. S-100 Bench Kit \$345. S-100 Rack Kit \$306. 6800 Bench Kit \$370. 6800 Rack Kit \$330. Assembled prices add \$100.

# ETI 642 S-100 16K STATIC RAM



Features: - 2114 low power static RAM's, 4K addressing, 4K write protect, bank select, wait state gen., plated through hole, solder resist mask, 300 or 450 nS speed, ETI 642.

Kit \$315. Ass. \$380. Add \$32 for 300 nS.

# 2708/2716 EPROM CARD

Features:- holds up to 16 2708 or 2716 (single supply) EPROMS, on board wait state gen. Unused locations may be blanked. Plated through holes, solder resist mask

PRICE:- Kit \$115. Ass \$155.

# **EPROM PROGRAMMING CARD**

Features:- ability to programme triple supply 2708's and single supply 2508, 2716, 2732 etc. Zif. Socket. On board 26V generator. Port driven.

Price:- Kit \$175. Ass \$205.

# Z-80 CPU CARD

Features: 4 MHz operation, power on jump, wait state generators, provision for on board 1K EPROM, front panel socket for reset, and data lines etc.

Price: KI \$156. Ass \$196.

# **Z-80 SINGLE BOARD COMPUTER**

Features:- 4 MHz operation, 1K static RAM, 8K/16K EPROM, serial/parallel ports, power on jump, timer, vectored interrupts, software selectable buad rates. With 2716 EPROM. Price:- Kit \$295. Ass \$370.

# 80 X 24 VIDEO DISPLAY CARD

Features:- on board Z-80 and CRT 5027 controller chips, parallel keyboard interface, 2708 driver chip, and 2708 character generator chip, special effects and extended character set available.

Price:- Kit \$290. Ass \$370.

# 64 X 16 VIDEO DISPLAY CARD

Features:-memory mapped 1K board, with reverse video and cursor control. RCA video connector, plated through holes and solder resist mask.

PRICE:- KIt \$155. Ass. \$180.

# FLOPPY DISK CONTROLLER CARD

Features:- single density, mini or full size disk drives with FD 1771 controller chip, can be interrupt driven, syncs with CPU in data transfer, Shugart/Remex compatabile.

Price:- KIt \$195 Ass \$235

# **DD FLOPPY DISK CONTROLLER CARD**

Features:- controls mini and full size, single/double sided single/double density and all combinations of each. Crystal locked, PLL data recovery, Shugart/Remex compatible software (CP/M / SDOS) for above controllers available.

Price:- Kit \$285. Ass \$345

## STANDARD EXTENDER CARD

Features:- double sided f/glass board, numbered test points reflow soldered.

Price:- Kit \$33. Ass. \$48

# WIRE WRAP CARD

Features: double side f/glass board, ground plane and supply rails run on both sides, 3M type connector patterns on top of board, provisions for regulators on all rails, holes are on .3" pitch, by .1" pitch.

Price: Bare board \$28.50

# **6800 PRODUCTS**

6800 Extender Board \$33. 6800 11-slot backplane \$36. 6800 11-slot chassis, rack mount \$330. 6800 Extender Terminator Board, Kit \$80. Ass \$105.

# **EPROMS AND RAM CHIPS**

2708 450nS guaranteed \$12. 2716 450nS single supply ex-stock \$47.50. Hitachi 2114 low power 450nS \$7.50. Hitachi 2114 low power 300nS \$8.50.

#### **DISK DRIVES**

Shugart SA400 \$410. Shugart SA801 \$710. Remex 8-inch double sided \$795.

# **DUAL 8" DRIVE PACKAGE**

Features:- contains dual 8" single or double sided disk drives either Remex or Shugart. Inbuilt power supply, cooling fan, modular construction, keyswitch, fused on mains, all aluminium 19" rack mount (10-½" high).

Price:- single sided \$1750. Double sided \$1950.

## **EPROM SOFTWARE**

Z-80 monitor in 2708 EPROM, has 16 functions, three versions available to drive TTY. TTY/VDU, KBD/VDU.
 Price \$25. 2. ETI 640 video driver EPROM, makes the memory mapped video card look like a terminal, has XY cursor addressing, home clear screen. Price \$25.
 6.25K Basic interpreter, in seven 2708 EPROMS, has

3. 6.25K Basic interpreter, in seven 2708 EPROMS, has trig functions, dimensions, command level input ability. EPROM resident at OC000 hex. Price \$180.

4. Disk control EPROMS, contain I/O routines to handle

 Disk control EPROMS, contain I/O routines to handle our disk controller with CP/M, 2 EPROM set with second EPROM containing inbuilt video driver and I/O routines for all external devices like printers, terminals etc. Price \$50.

Customised version available (I/O and relocation) for an additional charge depending on the programme.

# **DISK SOFTWARE**

CP/M version 1.4 customised for our controller. \$145. CBASIC II \$125. Wordmaster, wordprocessing package \$140. TEX writer, letter and text formatter \$50. CP/M user group library (33 vols) at \$12 per vol. RAM Diagnostic, reports errors and likely causes \$25. Available on 8" and 5-¼" single or double density. Above prices are for 8" disks.

#### 64K DYNAMIC RAM CARD

200nS access time, bank select, wait states, 4116 RAMS.

32K - kit \$525. A&T \$605.

48K — kit \$670. A&T \$750.

64K - kit \$815. A&T \$895.

#### MPB-100 CPU BOARD

Z80 CPU Board with 2K single supply EPROM provision, power on jump, 4 MHz, front panel socket, wait state.

KIT PRICE \$260. A&T \$310.

## 2708 EPROM CARD

16K of 2708, 4K address boundary, 8 or 16K area required, wait states, plated thru.

KIT PRICE \$98. A&T \$128.

# LA34 DECWRITER PRINTER/TERMINAL

Desk Top printer, full 128 ASCII character set, switchable 110 and 300 baud rates, 30 cps speed, adjustable character widths, adjustable line spacing, 9 x 7 dot matrix printing.

PRICE \$1,545 ex stock.

# **Z80 STARTER KIT**

Hex key pad, hex address & data displays, 2 x S100 sockets, wire wrap area, PROM programmer, parallel port, Kansas City cassette interface, timer chip (Z80 CTC), 2K monitor PROM, monitor listing, 120 page manual, 2K RAM, 4K PROM.

KIT PRICE \$350. A&T \$420.

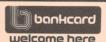
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# S-100 VO PORT BOARD



DUAL SERIAL I/O CARD Features:- dual independantly controlled serial ports with TTY and RS232 outputs and inputs. Nine programmable parallel ports, crystal controlled baud rates fully buffered and address decoded. Plated through holes & solder resist mask Price:- Kit \$189. Ass. \$225.

#### **UV EPROM ERASER**



New product range. Model LEE/T 15W tube, 120 min timer, up to 40 EPROMS will erase in 10/15 mins. Model MEE/T 8W tube 120 min timer, up to 10 EPROMS will erase in 20/30 mins. Model MEE is same as MEE/T but with no timer. All erasers are fully assembled and have a safety switch. LEE/T \$105. MEE/T \$93.50. MEE \$74.

## S-100 EXTENDER/TERMINATOR



EXTENDER TERMINATOR CARD — features:true active termination of the bus with inbuilt extender connector on top of board, fused rails to extended board. Test points numbered, solder resist, plated through. Price:- Kit \$70. Ass.

# **TEXAS KSR 820** PRINTER/TERMINAL

Desk top printer with 150 cps printing speed, 9 x 7 dot matrix, numeric key pad, tractor feed, RS232 interface, 132 characters wide, 110 to 9600 baud rate, 640 character buffer. **Price** \$3,000.

# **TELEVIDEO TVI-912 TERMINAL**

80 x 24 display, upper and lower case, 110 to 9600 baud rate, dual intensity, numeric pad, cursor controls, XY addressable cursor, block mode, self test, microprocessor controlled Price \$1,295.

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Note: Some Common BASIC Programs are available on cassette for the Commodore PET and Radio Shack TRS-80 at a list price of \$15.00 per cassette.

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- PROGRAMMING THE Z80 330 pages The basic introductory text on programming the Z80. \$11.95
- MICROPROCESSOR INTERFACING TECHNIQUES

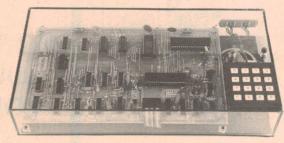
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# COMPLETE KITS \$135

inc. cabinet

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Modulator \$3 extra. Insured post \$2.50

C.O.D. \$2 extra. Phone C.O.D.s accepted

- The high quality "Digitran" keyboard has an 'over-centre' action to give positive contact and excellent tactile response. This greatly reduces keying errors, which will be especially appreciated towards the end of a long program! Since the keyboard greatly influences operator enjoyment, we believe that anything less is false economy.
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# "UFO INTERCEPT"

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#### POWER SUPPLY KITS (1 AMP) \$29

Contains all components, a heavy gauge aluminium chassis (undrilled), and a Marviplate cover. Compact size 171 x 130 x 70mm.

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Complete kit with cabinet as above. Power supply kits are post free with DREAM kits and are not available separately

- Pre-tinned fibreglass PC board with a COMPONENT OVERLAY for easy assembly.

- Programmed EPROM.
   Full instructions supplied.
   Provision for extra PIA's, ACIA's,
- etc, without additional logic.

  The PCB has been modified to accept a 6802 chip, which includes a clock, thereby eliminating the hard-to-get 6875. The 6802 was not available when the DREAM was designed, and the modification has been approved by the designer (Michael J. Bauer of Deakin University).
- When comparing prices, it should be noted that our kits are guaranteed contain only prime quality, guaranteed components
- Service is available.
- Overseas sales insured airmail cost covered by sales tax saving.



# MONEY-BACK GUARANTEE

Examine your purchase for 7 days (without removing the IC's from their packing) and if not satisfied, return it for a full refund. Please mention 'Electronics Australia' on your order. For further information see 'EA' May to August '79.

Phone for details of Sydney counter sales.

Please not	te new phone number.					
All mai	orders to J.R. Components.					
Please send me the following items:						
☐ Dream 6802 at \$135	Name					
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Post and Pack \$2.50	Postcode					
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PO Box 128, Eastwood, NSW. 2122. Ph (02) 85 3385 Tasmanian Agents AERO ELECTRONICS, 123A Bathurst St. Hobart

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Head band positioner gives 5 ms track to track access - 5 to 7 times faster

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than other drives, Fully closing front door and 1/2" Clutch Cone for media protection, Double Density Heads, Shugart Compatable, only 10 moving parts due to non-mechanical switching.

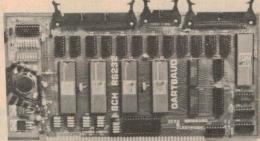
AVAILABLE

TWO MODELS • Model 51 Single Head 250k Bytes DD Model 52 Double Head 500k Bytes DD

52 \$450.00 (517.50) PRICING: 51 \$350.00 (402.50) Inc. tax. Inc. tax

Write or call for technical description. Power supply/case available May Since we are the Australian Distributors OEM discounts are available.

DARTBAUD



### FEATURES:

- 8 Independently selectable 1/0 channels
  2 Eight bit parallel ports
  RS-232 Interface levels
  Async or optional synchronous channels
  Baud rates 50-19, 200 independently selected for each channel

### SPECIFICATION:

Serial Ports:

Baud Rates:

8 Independent ports using Zilog D/ARTs (sync) or optionally S10/0 (may be retrofitted for synchronous parts, for any pair (S10 and DART are dual devices).
6 Independent, crystal-controlled, software selectable rates for each port selected from the 16 standard rates between 50 and 19,200 baud.

2 Independent ports using Zilog P10, selectable as either input or output.

Interrupts: Full on-board interrupt control provided. On-board devices daisy chained. Rotating priority control provided for running multiple boards (through top connector). Jumper selection of interrupt control (local, rotating, vectored). PRICE: POA & MANUAL AVAILABLE

THE CLARE MODEL C70/MGP - by far the best value in keyboards we have seen to

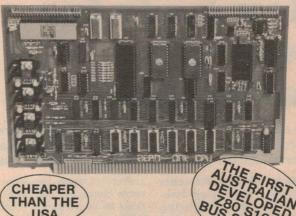
 70 key full upper and lower case with non mechanical Capacitive Keyswitch - fully encoded Microprocessor control with RS232 or 20ma serial options — parallel output standard single 5V Supply, Serial baud rate jumper from 110 to 9600 baud.

PRICE \$160 ea Connector \$3.00

MOULDED ABS plastic case to suit \$26.00

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- 8/Slot
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To accept \$100 or EXORCISER mother board/ power supply and has provision for Fan and 19' rack mounting

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- Supplied on minimum of 1 x16k Blocks expandable by merely plugging in extra

Price 16k kit \$255.00 All sockets supplied. each 16k add \$100.00 Assembled and tested add \$60.00

ETI 640 VDU kit fully socketed \$139 Please note that 200ns memories are required for VDU 4MHZ operation at \$6.00 extra or 10 x 21L02-2 for \$26.00 separately.

Z80 CPU CARD **FEATURES** 

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- ATURES —
  Comes with full assembly instructions and card documents.
  Power on jump for automatic execution of monitor program on startup.
  Front panel-less operation allowed by on board 2k monitor which is too good to explain here; 19 commands all unique abbreviations allowed.
  Full S100 DMA Capabilities.
  Sockets supplied for all major devices.
  Clock speed, 2MHZ Standard, 4MHZ Option.

- Clock speed, 2MHZ Standard, 4MHZ Option. 1/0 Z80 P10 2 x 8 bit programmable parallel 1/0. RAM 256 Bytes scratch pad (Monitor). Onboard 2100 baud Tarbell Cassette Interface (Software Controlled) with cassette recorder remote motor control Test Cassette supplied with CPU kit contains set up procedures for cassette interface as well as software to allow the cassette interface to read and dump 300 baud CUTS (Kansas City) format. Keyboard input direct onto card in parallel ASCII. Monitor performs all functions to drive

- Keyboard input direct onto card in parallel ASCII.

  Monitor performs all functions to drive ET1640 VDU as an ASCII terminal. Entry points for cursor control etc.

  The spare socket onboard is to allow the National MM57109 to be fitted which works in conjunction with the CPU to give a full floating point RPN arithmetic unit.

  Functions as a general purpose Z80 single board computer or as the heart of a fully expanded system to 64k Bytes of memory and a multitude of 1/0 devices.

  Plated thru solder masked printed circuit board with components screened overlay.

  Description Manual Construction manual \$1.00 refundable with purchase.

  PRICE KIT \$199.50 2MHZ
  \$225.00 A MHZ
  \$225.50 Number Cruncher Option Assembled and tested add \$50.00

BOOKS

U Technical Description \$10.00

posted Z80 P10 Technical Description \$6.50 posted Z80 CTC Technical Description \$6.50 posted Z80 CPU Programming and Assembly Lan-guage Manual \$10.00 posted

CARDS IN DEVELOPMENT

ard; with serial parallel ports, extra 1/0 Card; with serial parallel ports, extra ROM etc. Eprom Card; Holds 8 ROMS with Eprom

Programmer Floppy Control; Minifloppy or Floppy, CP/M Compatible Exorciser Mother Board/Power Supply Stand alone 80 column 125 CPS Tractor Feed Plain Paper Printer

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RS30 to \$100 Interface
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KT9500

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8.30am to 12 noon.

# GUMMUNICATIONS

## New body for two-way radio users

The electronic and appliance service industries are a major user of two-way mobile radio, using it as a means of communicating with service personnel on the road.

But, in common with other industries employing two-way radio, they are being subjected to outmoded laws, delays, and inconsistencies in interpreting regulations by government bodies, says a new national association set up to represent business radio users.

The association, ABIRA (Australian Business and Industrial Radio Association) this week launched an appeal for members. It is hoping for a good response from two-way radio users in the service industries.

ABIRA's immediate task is to press for a reduction in Commonwealth Government licence fees, which were doubled from July 1, 1979, from \$25 to \$50 per operating unit.

As examples of problems for users, ABIRA points to: • A restriction preventing transmission over more than 32 kilometres, which is much less than the range of most transmitters. • A requirement that

communication between remote controllers and base stations be by telephone landline. ABIRA wants users to have the option of controlling base stations by radio remote control, in case of landline failure. • Restrictions against one base station talking to another.

ABIRA also says that applicants for a business radio frequency sometimes have to wait up to six months before the frequency is allocated.

If sufficient support is received from potential members, ABIRA organisers plan to set up a full-time office in Canberra to lobby on members' behalf.

Further ahead, ABIRA plans newsletters to keep members up to date on legislation, regulations, technical developments and other items of interest: opportunities of attending meetings and workshops; and technical assistance to members.

Inquiries may be made to AB-IRA, P.O. Box 1582, Canberra City 2601 ACT.

### Special baluns for HF radar

Special HF baluns have recently been supplied to Defence Research Centre, Salisbury South Australia, for the "Jindalee" over the horizon radar (OTHR) project.

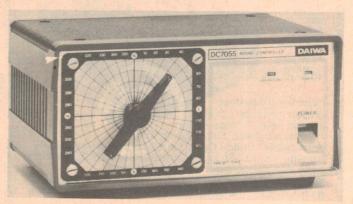
Designed and Manufactured by Antenna Engineering Australia Pty Ltd, of Kilsyth in Victoria, the baluns were required to meet the exacting specification issued by DRCS.

Rated at 25 kW, the baluns had to hold phase shift differences to less than two degrees from the reference balun over the frequency range 5-30 MHz. The AEA baluns exceeded the requirements, varying less than 0.6 degree.

Impedance of the baluns is

50 ohms unbalanced input and 300 ohms balanced output. VSWR was quoted at better than 1.2:1.

AEA manufacturers a wide range of baluns and terminations for both low and high power applications. Other main products include: antennas for communications, TV, FM, and navaids for HF, VHF, and UHF applications, as well as filters, diplexers, multicouplers and combiners.



### New antenna rotators

Daiwa has released a new range of antenna rotators which incorporate a map of the world — centred on Australia.

Two new control boxes are available for both the heavy and medium duty rotators. With the "pre-set" type of controller the antenna direction is set by turning the knob to the correct bearing for the country concerned. The rotator then turns to the desired heading.

The other type of controller uses the traditional method of pressing a button until the direction pointer stops at the correct bearing.

The Daiwa range of rotators are distributed in Australia and the Pacific by Vicom and are available at most ham dealers.

# Sunspots — countdown to a maxima

The Swiss Federal Observatory at Zurich maintains a continuous watch on the sun, monitoring sunspot activity and issuing reports on daily figures, monthly mean and smoothed mean parameters.

From their bulletins, numbers 7 to 12 for 1979, and number 1 for 1980, you can see the progress of the maxima, which should peak during the first half of this year — that's now!

Smoothed mean sunspot numbers for January to July last year are as follows:

Jan. 123.8

Feb.	131.0
March	136.7
April	141.5
May	147.8
June	153.8
July	156.2

The provisional mean for December 1979 was 182.2 and for January 1980, 162.2

The bands are jumping — get amongst it!

# CB for UK, maybe: 27 MHz? — No!

The British Home Office is delaying any decision on CB for the time being . . . but whatever happens, 27 MHz is definitely out!

Meanwhile, the Irish government has taken a hard line and outlawed CB radio, saying that illegal users will be prosecuted.

A National Committee for Legalisation of Citizens Band Radio has been formed in the UK in an effort to draw attention to the growing band of enthusiasts. Already a British CBers book has appeared on the market and a petition has been circulated and presented to the Government.

Some of the British electronics magazines are carrying short columns on CB . . . naturally not inciting anyone to break the law! One suspects it could be a long, hard grind.



### Airband receiver covers new frequency range

GFS Electronic imports. recently announced that their handheld airband receiver, the Sky Ace R-517. is now available with new frequency coverage.

This latest version covers 108 to 140 MHz, allowing users to take advantage of the many Aerodrome Terminal Information Services (A.T.I.S.) that are transmitted within the navigation band (108-118 MHz) by major aerodromes throughout Australia.

Up to three crystal-locked channels may be installed or, if desired, across the band. A fine tuning control is also included.

Sensitivity and performance are high, according to GFS. The unit is priced at \$104 plus \$2.50 post. Crystals (if required) are \$7 each for standard frequencies or \$17 each for special frequen-

For more information on the



Electronic Imports, 15 McKeon Road, Mitcham Vic 3132. (03)

### Sky Ace R-517 contact GFS

### Field day success

The Central Coast Amateur Radio Club's 23rd annual field day, held on Sunday 17 February, was a great success.

The registered attendance was 790. The contests and events were keenly contested and this year saw a noticeable trend towards younger contenstants - with junior competitors taking out open as well as junior prizes!

Overall first for the day's events was a tie between Dave Andrews VK2AWZ and Athol Tilley, VK2BAD. Overall first in the junior section was young Craig Smith.

The amateur television display at the field day provided a telecast of the WIA NSW Division's Sunday morning news broadcast, with John Williams VK2BUI as news reader, and a live cross to the Gosford Showground venue for a report from the field day.

The ever-popular 'disposals market' - where everyone gets rid of unwanted equipment (including the gear they brought at last year's disposals market . . . Ed!), was a raging success, becoming instantly crowded immediately it opened. Some 503 items changed hands.

The CCARC wishes to acknowledge the generosity of the following companies and individuals who provided prizes for field day events and/or display stands: Applied Technology, ANARTS, Dick Smith Electronics, Emtronics, Ferguson transformers, Hy-Q Industries, Lyle Patison VK2ALU, NSW QSL Bureau, Scalar Industries, Sideband Electronics Engineering, Sideband Electronics Imports, Sideband Electronics Sales, Trio-Kenwood (Aust.), Union Carbide (Aust.), Vicom International, Westlakes Radio Club, WIA NSW Division, YRS Education Service.

See you there next year.

### Security for radio transmissions

In the past, users of radio communications could rely on a reasonable degree of privacy as a matter of course. However, this is no longer the case.

The ready availability of monitoring equipment, such as the scanning receivers, plus the general interest and desire to eavesdrop, has significantly impinged on the privacy of these communications media.

Today, radioteletype and data communications are being used at an accelerated rate for the exchange of confidential information. Public safety agencies, utilities, law enforcement and private and industrial institutions are transmitting increased volumes of sensitive information.

Privacy devices' for radio communications provide assurance against compromise. To be worthwhile, a privacy de-

vice must be effective against determined efforts to "break" its security. Equipment that is made useless by easy decoding defeats its basic intent.

With this object in mind, Vicom International, Professional Products Division, is to release a range of digital and analogue security devices providing a wide range of security codes. Many of the units are simple and the devices can be fitted with only minimum modification to the radio set. For further information, contact Vicom International, Professional Products Division, 68 Eastern Road, South Melbourne.

### **UHF** frequency counter

The Sarrosa Model 261 UHF frequency counter has been designed as a compact, rugged, easy to use instrument for the frequency range 20 Hz to 600 MHz.

With optional battery pack fitted, the unit is ideal for field use. Selection of all functions is by front panel push buttons.

A high contrast, nine-digit LED display is provided, with full memory, and decimal point placement is automatic with range and gate time selection.

For low frequency (under 5 kHz) signals, such as are used in selective calling systems, the input frequency is multiplied by a factor of 100 in a phaselocked loop, enabling measurements with 0.01 Hz resolution to be made with one second gate time, according to the specifications.

The instrument features 20 mV sensitivity over its entire range and may be overloaded with up to 250 Vac. The instrument can be supplied in a bench case version or with or with standard rack mounts.

For further details contact The Dindima Group Pty Ltd P.O. Box 106 Vermont Vic 3133.

### RF power analyst with calculator.

A new RF wattmeter from the Bird Electronic Corporation has its own built-in calculator to give direct digital readings of its nine functions.

It operates at power levels from 100 mW to 10 kW and from 500 kHz to 2.3 GHz. The model 4381 RF Power Analyst calculates its various functions continuously and displays the answers at a touch of a button. It will calculate and display voltage standing-wave ratio (VSWR), the continuous-wave or frequency modulation power (both forward and reflected) in dBm or watts, peak envelope

power, percent modulation and delta function. It also features a memory which shows the maximum and minimum optimum values for when making adjustments.

Other models in the 4380 series can handle up to 250 kW and further information can be obtained direct from Bird Electronic Corp. 30303 Aurora Road Cleveland (Solon), Ohio 44139

### **Amateur Radio Book Stock Clearance**

We're wildly overstocked with many of our popular Amateur Radio books. So much so that we've got to clear space for new stock arriving for our new catalogue. Here's your chance to SAVE on many titles: many of these prices are lower than those in our new catalogue! But remember: these prices are current only while current stocks last. HURRY!

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Big savings on 1979 world callbooks: Yes: great value for the ham or swl on a budget. Last year's callbook maybe, but the contents don't change all that much from year to year!

US Callbook (B-2260) All the amateurs of continental US, Hawaii, its posessions etc. Was \$21.95, now reduced to only \$17.50

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# shortwave loggings

### **Dubai tests**

The small but rich Persian Gulf state of Dubai, in the United Arab Emirates, has commenced test transmissions from their newly installed shortwave transmitters.

Dubai's plan for an international shortwave service was mentioned back in October ETI, when the station was in the process of recruiting technical and programming staff from around the world.

Radio and TV Dubai has installed three shortwave transmitters of 300 kilowatts each. Since early in March they've been heard testing on 21 500 between 0600 and 1000, with programming in Arabic relayed from the Home Service. Broadcasts have been directed to Europe, but have still been well heard in eastern Australia.

Dubai plans to start an English service once tests are completed and regularly scheduled programmes are introduced. Most programmes will be directed to listeners in either the Middle East or Europe, but if the recent test transmissions are any guide these broadcasts should still be easily heard here, with the 300 kilowatts of juice helping matters along. The plans of Dubai to mostly use higher frequencies, from the 25 metre band up-

wards, should also be a big factor in ensuring reliable reception in Australia.

The station has registered a number of frequencies with the International Telecommunications Union (ITU) in Geneva, which has the task of coordinating usage of channels in the crowded shortwave broadcast bands. Dubai's current registered frequencies are: 7105, 9590, 9680, 9755, 11 730, 11 830, 15 110, 15 115, 15 160, 17 710, 17 790 and 21 480. Interestingly, although the first tests took place on 21 500, this frequency has not been registered with the ITU! Nevertheless, the above frequencies are the outlets to watch for further Dubai broadcasts, with most broadcasts probably taking place between 0600 and 1630.

If you hear any of the test broadcasts from Dubai, why not let them know about reception conditions in your location? You can write to P.O. Box 1695, Dubai, United Arab Emirates. Address reception reports to the Chief Engineer, Dubai Radio and Colour Televsion.

### Latin African Log

The 1980 edition of the Latin American and African Radio Log is now out.

The 1980 Log contains a full listing of all stations, in frequency order, which have been heard in east Australia since March 1979 and are located in Africa or Latin America.

The Latin American section covers the full shortwave range from 2 MHz through to 30 MHz, while the African section concentrates on stations heard from east Australia in the tropical bands 2000-5900 kHz.

A special feature of the 1980 Log is the full list of QSLs received over the last 14 months from Latin American and African regional stations. This provides such information as to how long a station has taken to reply to a reception report, whether the station will answer reports written in English (most do!), and if the station sends a card, a letter or other goodies such as pennants etc.

The 1980 Latin American and African Log is a 16-page booklet available from the ARDXC for \$2. Just write for your copy to the address in this column. This is an invaluable reference for all the DXers seeking to identify the exotic stations to be heard during the coming winter months.

# Agradecemos a sua sintonia. OM 680 KHZ 49 m 6.135 KHZ 25 m 11.915 KHZ Thank you for your syntonization.

### International schedules

Unlike stations on the mediumwave band, international shortwave broadcasting stations do not have fixed frequencies. Instead, frequencies are changed at regular intervals throughout the year to take advantage of seasonal propagation factors.

Most international shortwave stations prefer to use higher frequencies during the summer months, and then switch to lower frequencies in the winter months when less sunlight means the ionosphere supports generally lower frequencies.

Right now, international stations have just adjusted frequencies at the start of the J-1980 transmission period, and the J-80 period will last until the first week in September, when the S-80 period commences. Other transmission periods begin on the first Sunday in November (period D), and in March (period M).

International stations are usually pleased to forward their schedule to listeners on request, free of charge. As we approach September, why not try writing to the international station you are most interested in and request a copy of their S-80 schedule? You can write to most of the better-heard stations in the capital cities of the country where they are located. You will then be able to keep track of the frequencies of the station when the changes occur in September.

Another good idea is to write a reception report to the station telling how well you are hearing their new frequencies. International stations are especially keen to know of any interference to their broadcasts, and the name of the interfering station if you can identify it.

All this is called "feedback" and is an important part of the DXing hobby. Such feedback from the listener to the station makes DXing the active hobby that it is today, being a step up from the passive SWLing pastime. A bonus will come to you in the form of QSL cards from the broadcast stations to whom you report.

### Bhutan

Some time ago, at the suggestion of ARDXC, the National Youth Association of Bhutan introduced an overseas service, at a time which would allow propagation over long distance paths.

The transmitter used is, in fact, one operated for amateur applications at other times, and the current schedule is as follows: 7040 0600-0900 (Sundays); 4690 1100-1400 (Wednesdays and Fridays). English is at 1300-1400.

The station issues a QSL, but only does so for specific, fully detailed DX reports, and for this reason is regarded as one of the rarest SW stations currently operating.

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82/C/1up to 82/C/7	69.01 27.25 51.47
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### shortwave logging

### Laos good

Shortwave broadcasting in Laos is very extensive, with most of the main towns possessing a shortwave transmitter.

Nevertheless, broadcasting in Laos has a touch of the exotic, with most transmitters being of low power, apt to drift in frequency, and tending to operate on odd-ball frequencies well away from the mainstream of the shortwave bands.

The Vientiane National station operates on a conventional 49 metre band outlet of 6130 and usually gives good signals after HCJB in Ecuador leaves the frequency at about 1130 nightly. Vientiane has a major news bulletin at 1200 preceded by clock chimes, and this programme is usually relayed by all other shortwave stations across the country.

Best heard of the regional sta-

tions at present is Savannakhet on 7385, sometimes drifting down towards 7380. This station usually opens by 1100, but try them a little later for, by 1200, signals should be much improved.

Also showing at present is Luang Prabang on 7000, which is either a recent deliberate shift in frequency, or just a drift from 6997. The recent change of frequency, whatever the cause, is helpful for it means Luang Prabang is now relatively free of interference from the strong China station on 6995.

Pakse is another of the regional stations which is frequently well heard, and the last monitored outlet from them was 6600. But just as signals became quite good, it has become inactive recently, although this may be only a temporary silence.

### Brazilian signals peak

Autumn in east Australia is the best time to listen for Brazilian stations.

The Brazilian shortwave broadcasting set-up is quite unique and exciting, with hundreds of stations on the shortwave bands from 60 metres right up to 16 metres. Probably the best reception is on 49, 31 and 25 metres. These are best heard at their local sign-on times, around 0800 or 0900. Signals travel almost directly across the South Pole from south eastern Brazil. A great circle map is most useful for studying propagation paths, and retail outlets, such as Technical books in Melbourne and Dick Smith stores, make these available. Some of the stronger Brazilians this year have been: 5965, Radio Guaiba in Porto Alegre, which has a lively musical format up to 1000 after opening at 0900, then has a news programme called "Radio jornal da Guaiba" from 1000. 9675, Radio Marumbi Limitada

at Florianopolis, which can be heard from about 0830. They have music up to 0900, then often have religious segments. Listen for the drum roll and identification announcement just before 0900.

On 9545, Radio Universo at

Curitiba. This station has in previous years been a tough DX catch, but has been strong on a clear frequency of late. The station opens at about 0850, and also seems to favour religious segments at 0900.

On 11 765 is Radio Tupi in Sao Paulo. This one can be heard from about 0820 and has some very wild DJs, plus some great Brazilian rhythm bands.

On 11 780, Radio Nacional at Brasilia, is the national network. and often carries news reports from 1000 which are relayed from stations across the country. This one often shows up in the mornings also, at around 2100 to 2200, and is heard in parallel with the other Brasilia outlet of 15 445.

Although all these stations broadcast in Portuguese, most will reply to reception reports written in English. Some of these stations also send colourful stickers or pennants, in addition to verification cards or letters. The addresses of all these Brazilian stations, and any others you may hear, are given in the World Radio and TV Handbook.

### Belgian Radio in French

Radio Television Belge in Brussels, the French network of Belgian broadcasting, has announced their schedule effective up to the end of September.

The station will operate continuously on Sundays, from 0500 to sign off at 2000, using 21 460 and 15 210.

Monday to Saturday transmissions are broken into 5 separate blocks after which frequency adjustments are made: 0400-0515 Brussels will use 11 880 and 15 210. 0515-0615 they will be on 21 460 and 15 210.

The next segment, 1030-1230, will be broadcast on both 21 460. and 15 210. The next programme block from 1400-1545 is listed to use 5965 and 21 460. The final segment is on air from 1600 to close down at 2030, and is to be broadcast on 21 460 and 15 210.

RTB will be happy to supply listeners with a frequency schedule and programme details. Should you wish to receive a copy of the English language schedule then you will need to write to BRT which is the Dutch language network. BRT has not made the schedule available as yet, but you could write requesting a copy to: BRT, P.O. Box 26, B-1000, Brussels.

### African news

With our winter approaching, DX signals on the lower frequency bands improve, in particular around our breakfast period, on 5 MHz.

Interesting African signals to watch out for, which have been

heard around Eastern Australia recently, include: 5020 Niamey (Niger) with North African vocals, French programme at 2040:

5010 Garoua (Cameroon). Local music, French 2045;

5005 Radio Ecuatorial, Bata (Equatorial Guinea). Spanish and local dialects 2030-2100:

4990 Lagos (Nigeria). Home service, with English and Vernaculars, from around 1900;

4976 Kampala (Uganda). Recently reactivated channel, Swahili service around 2040:

4911 Lusaka (Zambia). High powered outlet, brought back into use recently. often has telephone phone-in programmes from local listeners around

4820 Luanda (Angola). Portuguese programming around 1900-2100

### Radio Thailand in clear

Although close to Australia, and with a regular international service on shortwave, Radio Thailand is not one of the better heard Asian stations.

Currently Bangkok's English service is on a clear frequency during the evening programme.

The English service is heard on 9655 from 1055 to 1155, with news at 1100. The English programme is also listed for broadcast at this time on 11 905 but reception of this outlet is virtually impossible in Australia at present due to the Central Broadcasting System in Taiwan using the frequency in our evenings for programmes to China.

Most Radio Thailand programmes feature interesting talks about the country together with local music.

Meanwhile, the Home Service from Bangkok, in Thai, is often audible on 4830 from fade in at about 1300 through to sign-off at 1600.

NOTE! All times are given in Greenwich Mean Time (GMT). To convert to Australian Eastern Standard Time, add 10 hours (11 hours for Daylight Saving Time). To convert to Central Time, add 9.5 hours and for Western Time add 8 hours. All frequencies are in kHz.

Shortwave Loggings is compiled by Peter Bunn on behalf of the Australian Radio DX Club (ARDXC). Further information on DXing or the activities of ARDXC may be obtained from either PO Box 67, Highett Vic 3190, or from PO Box 79, Narrabeen NSW 2101, for a 30c stamp.



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L.E.D. DISPLAY (LIGHT EMITTING DIODE) READ THE TIME IN THE DARK — BETTER THAN L.C.D. DISPLAY.

### 10 DISPLAY FUNCTIONS

The Sunwatch is capable of displaying, the following information.

- Hours
   Minutes
   Seconds Months • Dates • Leap Year • Speed calibration . AM/PM indicator
- Seconds count off Easy to read
- · A natural side view display.

### SOLAR AGE EFFICIENCY

LENGTH The power source: Tiny silicon power cells which are constantly being energised by natural sunlight, daylight or an ordinary light bulb, keep the Sunwatch storage system charged. Should the watch not be exposed to light it will continue to operate for months on stored power.

### INDESTRUCTIBLE

The Sunwatch is shock resistant to 5,000 Gs. Wear it while doing heavy work, exercise, hammering nails, place it in boiling water for 30 minutes, freeze it in a block of ice for a year.
Imagine Split Second accuracy for the

rest of your life. Sunwatch is virtually

PERMANENTLY SEALED TO WITH STAND ABUSE AND THE ELEMENTS

MAGNETIC SLIDE SWITCHES

### NEVER REPLACE BATTERIES

The Solar cells last virtually forever, so you will never replace a watch battery again. Four varying light intensities are built into the viewing display.

The Sunwatch adjusts automatically to any light, you can always read it, even in the brightest sunlight.

### 100% COMPLETELY WATERPROOF

Sunwatch can be left in salt water for months, dive with it, shower with it. There are no openings, no 'O' rings or seals to leak. There are no air spaces inside the Sunwatch therefore it is not susceptible to high pressures - water proof to 750ft.(230m)

PROGRAMMED TO THE IYEAR 2100

The built in computer on a chip will always display the correct time, date and month. Also it automatically adjusts the watch calendar for long and short months, and leap years and is programmed to the year 2100 - years ahead of its time.

### WARRANTY

The Sunwatch is covered by a 2 year warranty issued by the makers in U.S.A. A copy of the warranty comes with every

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# YOUR GRADO

Grado cartridges have more than left their mark in the minds of many serious hi-fi enthusiasts.

But while these audiophiles have spread the Grado's reputation of cartridge excellence throughout most of the world, there still exists one group of people who have yet to experience the Grado difference: Australians.

It is Audio 2000's intention to correct this oversight.

Hi-fi enthusiasts are a diverse lot, owning everything from a modest set-up costing a couple of hundred dollars to the serious types who control systems costing many thousands

Subsequently, Grado has developed a range of cartridges that satisfy the individual requirements of each.

All Grado cartridges, from the \$850 Signature 3 to the \$18.50 FTR+, have Grado's cartridge engineering excellence in common:

1. All have a lower tip mass which vastly improves tracking ability, thereby also reducing groove distortion.

2. All have a cantilever assembly which is robust.

3. All have user replaceable stylus assemblies.

While all this may be music to your ears, the real Grado difference stems from the ability to overcome many of the electromechanical distortion products found in other modern cartridges (by the Flux Bridger Principle), and the ability to deliver correct tonal balance with its very extended top end and tight bass.

For more information about your next cartridge contact Audio 2000: P.O. Box 107 Brookvale, NSW 2100, phone (02) 939 2159.

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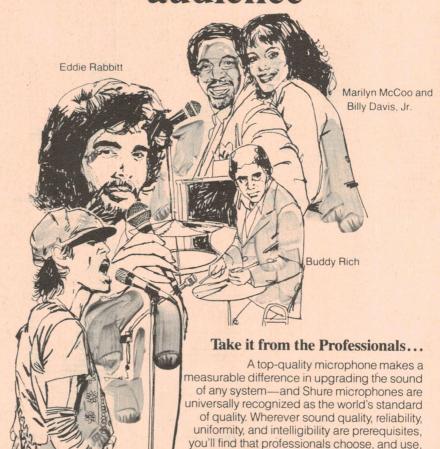
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anywhere that sound excellence is a prime consideration. They are the reliable, professional connection between you and the people you're trying to reach. Send for complete literature. Please let us know your microphone application.

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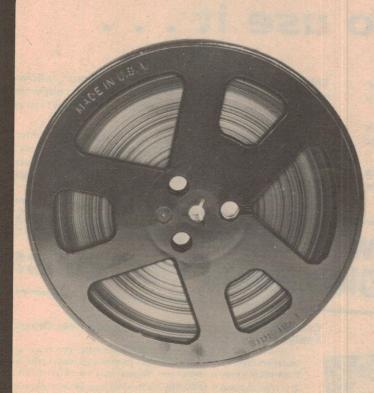
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# Top AMPEX REEL to REEL TAPE at one-third normal price!



The USA Ampex Corporation has made available a substantial quantity of 'off-cut' tapes from their highest grade material. All tapes are 1800 ft (549 m) by ¼", 1 mil ferric oxide on standard 7" reels

There's a slight gamble involved — but one in which you either win a lot — or a hell of a lot!

Here's why:

The tapes offered are of differing types and you take pot luck on which you receive.

BUT, The lowest quality is Ampex' superb Ampex Plus series! The highest is Ampex' Grand Master series!

SO. If you draw the Ampex Plus' you'll be paying about one-third the usual price. If you score the Grand Masters you'll be paying about a quarter usual price.

YOU CANNOT LOSE. If you are not totally and completely satisfied with your purchase, Dindy guarantee to return the full purchase price without question provided the tapes are returned within 14 days in the original packing.

Identical tapes to those offered are marketed in the USA by Ampex, using the trade name 'Shamrock'. This trade name is also used for those offered here.

NOTE: This offer is made by Dindy Marketing (Aust.) Pty Ltd and this publication is acting as a clearing house only. Cheques should be made payable to 'Ampex Tape Offer' and sent, together with the order form or accompanying letter, to 'Ampex Tape Offer', c/o ETI Magazine, 15 Boundary Street, Rushcutters Bay NSW 2011. We will then process your order and pass it on to Dindy, who will send you the goods. Please allow up to four weeks for delivery.

Owing to the exceptionally low offer price, the minimum ordering quantity is ten tapes (total \$39).

# \$39 for 10 reels Plus \$2.00 for post and packing.

Please supply .....tapes at \$39 for ten \$ .....

Plus post and packing, any quantity:— \$2.00

TOTAL \$ .....

Name ......

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······

Hands up if you own a graphic equaliser.



# Hands up if you kn how to use it

It's a fact: thousands of people have bought or built graphic equalisers recently, but only a tiny percentage have any idea how to use them.

Sure, it's fun to listen to the sound change its character as you play with the knobs - but after that, what?

Those 'in the know' have known about a device which would allow you to get the most from your graphic equaliser.

This device, called a 'Graphic Analyser', allows you to obtain a virtually 'flat' frequency response from your audio system - which is what hi fi is all about, isn't it?

Trouble was, graphic analysers weren't all that common. That was, until March Electronics Australia magazine described a particularly good graphic analyser: ideal for the hobbyist to build, and at low cost!

# Here it is: the new Playmaster Graphic Analyser kit from Dick Smith Electronics



You win three ways with this superb new Graphic **Analyser from Dick Smith:** 

- 1: It is more than just a graphic analyser. After you've set your equaliser levels, it doubles as a peak level meter, reading the level from each stereo channel and displaying it via LED indicators.
- 2: It is priced under \$100.00! It's this low, low price because it is supplied as a kit: you supply the labour to put it together (a very easy task) and save hundreds of dollars by doing so!.
- 3: It comes complete with full instructions, both how to put it together, and how to get the most from your system. When it's finished, you'll be proud to say 'I built it!'.

The Playmaster Graphic Analyser/Level Meter was designed to match any graphic equaliser - not just its partner, the Playmaster Graphic Equaliser. So even if you bought your equaliser 'off the shelf', have no fear: this analyser will still help you!.

**Playmaster Graphic** Analyser/Level Meter

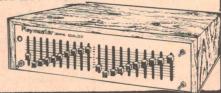
Simulated Walnut Sleeve, as above:

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DON'T OWN A GRAPHIC EQUALISER EITHER?

Why not build both! The Graphic Analyser and the Graphic Equaliser. They're a great pair: perfectly matched to each other. You'll really get the most from your hi fi system Imagine - being able to contour the frequency response to the way you

Cat K-3500



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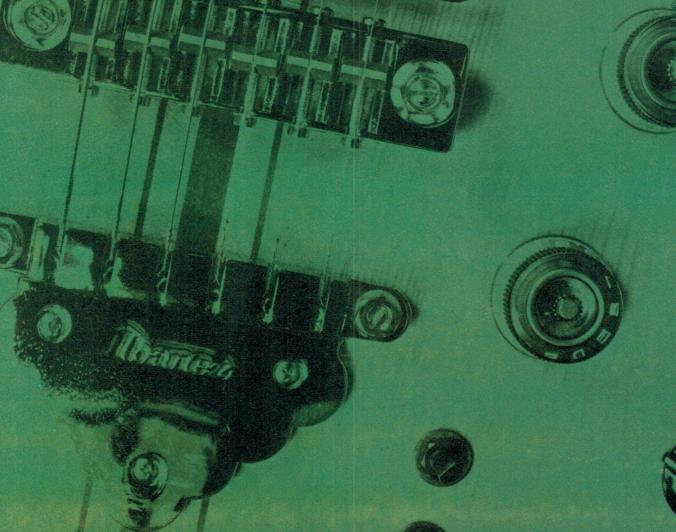
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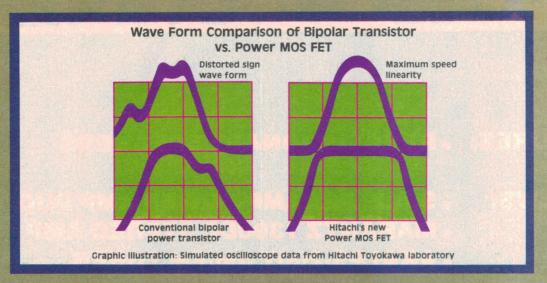
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MARANTZ 1300DC STEREO AMP 154 . AKAI PS-200T AM/FM TUNER





# The world's fastest integrated amplifier



# Hitachi Power MOS FET

The HA-7700 Stereo Integrated Amplifier brings you stunning sound reproduction. The Hitachi Power MOS FET offers ultra-high switching speed for dramatically reduced distortion and outstanding transient response. It features the same incredible technology that went into our renowned HMA-7500 Stereo Power Amplifier and HA-8700 Stereo Integrated Amplifier.

Power output is 70 watts per channel with no more than 0.008% total harmonic distortion from 20 to 20,000 Hz. And all stages are direct coupled, so you get the purest waveform reproduction fidelity from input to output.

The RIAA phono equalizer is a top-precision design employing only the highest-quality components for low-distortion and true-to-life disc playback. There's a full complement of control and convenience features for maximum system flexibility.

The HA-7700. True purity in waveform reproduction is here.

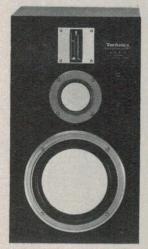




# © Solling news

# Technics' award winners released here

Technics launched their 1980 releases at a press conference in Terrigal, NSW, in March, featuring a number of award-winning products in the line-up.



Technics' Stereo Division Director, Mr Toshiro Masui said that the company entered seven of its new line-up in the 1980 Japanese Grand Prix for Audio and all seven came away with an award.

Technics' SL10 linear tracking turntable collected a special award and was presented at the conference as something of an audio star.

Although it is unlikely to become an audio buff's dream it will certainly fill a hole in the market place.

Priced at \$699 (recommended retail) it is the ultimate in simple sophistication.

That may sound like a contradiction in terms, but that is what this newcomer is. Featuring a sophisticated arm and platter drive system plus automatic record size selection and track repeat features, the unit is no larger than an LP cover in overall dimensions.

It comes with a moving coil cartridge and a built-in head amp and will run off both mains and 12 volts/dc. But, although the workings are extremely sophisticated, it is so simple to operate even a baby would get by without doing any damage.

It is aimed at the "female market" that hitherto has been badly neglected in the technological rat race that surrounds the hi-fi industry.

Whether the ladies will be interested to know that the SL10 will operate on its top as well as bottom, back, and sides is hard to guess. But it was all part of the entertaining demonstration given by an engineer from Technics' record turntable factory in Osaka.

Other items of interest released at the press conference included new "honeycomb" speakers and a new type of "Class A" amplifier that will sell for between \$299 (40 watts per channel) to \$5000 for 200 watts per channel.

There was much discussion on this new amplifier, for which extravagant claims are made as to performance, but little was resolved.

Microcassette radio portables were shown, and a novel set of headphones that hung on one's ears like ear rings.

A new portable cassette player which comes with head-phones attached for private listening only will probably interest the mums and dads fed up with having their homes polluted by teenage rock music, although the price of between \$150 and \$200 may dampen their interest.

The "honeycomb" speakers are an interesting concept and one that may help to heighten the Technics speaker reputation that drags well behind its



reputation for producing electronics.

Technics borrowed technology from the Harrier Jump Jet for the concept.

The face of the drivers in this new speaker consist of an aluminium honeycomb 'sandwich'. Technics argue that a speaker driver is a piston that pushes air. The requirements for this piston is that it be light, so that it can be pushed with minimum effort, but rigid so that the sound is clean.

The sound from these speak-

ers appeared excellent although no one at Terrigal was prepared to commit themselves. Private listening sessions with known material in known surroundings will be the ultimate test.

But off the cuff, they sounded alright with quite an accurate mid-range and plenty of bottom end 'oomph'.

The new Technics line up is, to say the least, interesting if not spectacular, and all will need closer examination when the stocks become available.

**Dennis Lingane** 

# Speakers and cartridges from Concept.

Concept Audio Pty Ltd have announced their appointment as importers and distributors for the KLH loudspeaker line manufactured in the USA.

KLH have developed a 'computer controlled' range of loudspeakers which have been named KLH-1, KLH-2 and KLH-3 and which have an estimated retail price of \$1995, \$1198 and \$698 respectively. The KLH-4 is similar to the KLH-3 only without the analog computer and has an estimated retail price of \$448.

Concept Audio are also dis-

tributors of the Rega turntables and cartridges. The new Rega R100 cartridge, which has a recommended retail price of \$85, has been specially designed to work in all medium-mass type tone-arms.

Further information can be obtained from Concept Audio Pty Ltd, 22 Wattle Road Brookvale NSW 2100; (02) 938-3700.

### **Tune in on Audiosound**

If you're seeking good sound from AM or FM broadcasts then you should seriously consider the Audio sound tuner range.

The model T751 is an AM/FM tuner and the T752 is a high performance FM tuner only. Both use meticulously designed IF and RF sections resulting in high quality sound performance.

The AM100 tuner for AM only, which was released in 1970, has also been updated and is now appearing as model AM101.

This model can be supplied to cover University Radio 1750 kHz, but at the expense of the lower end which is then 560 kHz instead of 530 kHz.

Further information brochures, specifications and prices can be obtained from Audiosound Electric Services, 148 Pitt Road, North Curl Curl NSW 2099 (02) 938-2068.

# When you design

a monitor loudspeaker as famous as the Model SIX, it's very hard to go one better.

After 4 years of research we did!



# ELEVEN SERIES II

In hand finished Amercian Walnut, individually assembled and tested. 120 watts RMS per channel. Recommended resale \$750 pr.

A TOUGH ACT TO FOLLOW



Available at most reputable high fidelity sound centres or information from

eterson SPEAKER LABORATORIES Pty Ltd

7 Alex Avenue, Moorabbin 3189. Telephone (03) 553-1055.

# news

# Low profile stereo cassette decks

Latest releases from Toshiba include low profile stereo cassette decks with metal tape compatibility standing just 100 mm high.

The two units are the Toshiba PC-X20 model and the Toshiba PC-X40 model with multi MQS (Music Quick Sensor) system. Both offer the choice of metal tape recording and playback as well as use of normal and Cr02 tapes.

The PC-X20 and PC-X40 stereo cassette decks incorporate the following common features:

- Wow and flutter of only 0.05% WRMS (0.16% DIN) and frequency response of 20 Hz to 18 kHz with metal tape.
- S/N ratio of 62 dB (metal tape), and distortion of 0.04% (metal tape).
- A two-bar display for recording level indication using IED digital peak meters with the

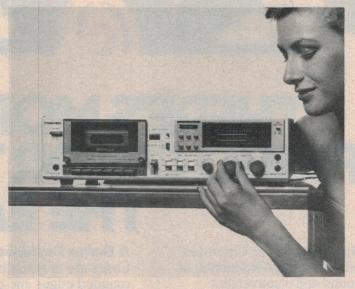
newly developed dot display; two bar-graph meters light up in green below -10 dB. From -10 dB to 0 dB green dots show the level, while above 0 dB red dots show the level.

- Soft eject and easy removal mechanism in the cassette holder.
- Dolby noise reduction, cue/review functions for easy search of recorded position, and provision for external audio timer for unattended recording and playback.

Additional highlights of the Toshiba PC-X40 stereo cassette deck are:

 Multi Music Quick Sensor system which allows programmed music of up to six tracks at a time.

Programmed music posi-



tions are shown by red LEDs in multi programming, and single programming for a certain track is also possible up to the fifth track in advance, excluding the first or current track being played. An auto repeat function gives continuous playback of recorded tape for background music.

More information from Toshiba Australia's Pty Ltd, 16 Mars Rd, Lane Cove NSW 2066.

# Pioneer price cuts attack furniture-grams

Pioneer Electronics has launched a double-barrelled attack on the \$400-450 hi-fi systems market.

This market, currently estimated to be worth at least five million dollars per year, is being partially satisfied by some three-in-ones and what are commonly known as furniture-grams.

Price reductions on Pioneer's Formula 4000 receiver system and the MS-350 compact three-in-one will lead the attack, according to Pioneer.

The Formula 4000 will now sell at \$399 (rrp) a reduction of \$100, and the MS-350 will sell for the same price, a \$70 reduction

Both models include a belt-drive turntable and powerful AM/FM receiver to take full advantage of the new FM stations which commence operation this year.

Each is covered by Pioneer's three-year parts and labour warranty and can be purchased with matching cabinet for only \$459.

For further information please contact: Rod Knapp, Publicity-Promotions Officer, Melbourne 90-9011 or Aly Jocys, Publicity-Promotions Officer Sydney 93-0246.

### Sound Archives conference

The 1980 Conference of the Australian Branch of the International Association of Sound Archives will be held in Canberra on May 10 and 11, 1980.

Venue for the Conference is the Common Room, Bruce Hall, Australian National University, Canberra, A.C.T. It is situated on the campus in Daley Road (telephone: (062) 49-2818).

All persons interested in the creation, use and preservation of sound are invited to attend. Contact Peter Burgis, IASA Secretary, on (062) 621-513 for details.



### Third-octave analyser

The Abacus Arta 8000 analyser is a versatile instrument that displays the real-time intensity and spectral distribution of sounds.

Loudspeaker measurements, whether in production testing or on site with room interaction, are important for high quality sound reproduction. Pink noise/real-time analyser testing is currently being used in studio control rooms, film dubbing theatres, cinemas and with sound reinforcement systems.

Deficiencies in system performance may be corrected architectually, or electrically with equalisers, to adjust the electro-acoustic response to the desired 'house curve'.

The Arta 8000 analyser has numerous applications in the

design, evaluation, maintenance and installation of audio circuits and systems. These include signal, hum and noise tracing; cable high frequency loss measurement; filter, tone control and equaliser circuits, cables and magnetic recorder heads; loudspeaker cross-over design and many other specialist applications in the field of audio and acoustic engineering.

For further details, please contact the Dindima Group Pty. Ltd., PO Box 106, Vermont. Vic. 3133.



# THERE'S MORE TO AGFA FERRO COLOR THAN MEETS THE EARS.

Agfa Ferro Color Cassettes offer superb reproduction of sound and a convenient colour-coded reference system.

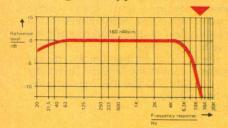
With a choice of three colours and three tape durations – 60, 90 and 120 – you have up to nine combinations for a comprehensive, easy-select library.

Add colour-coding to the many other features and it's easy to choose Agfa Ferro Color Cassettes.



**High Dynamics:** Agfa Ferro Color Cassettes have a high quality iron oxide coating to increase dynamic range and frequency responses.

The result is a rich, clear, transparent sound ideal for the recording of all types of music.



A Better Designed Case:

Cases are of smooth lines, with rounded edges and corners to improve handling and efficiency.

### A Better Designed Cassette:

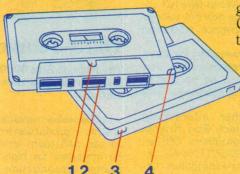
The Cassettes are of the screwed type and side one can be easily identified.

Inside the cassette is a special noise shield to avoid unwanted 'hum'.

To prevent unintentional erasure, knock-out tabs are located in the rear. These are optional either side.



For the convenience of colour-coding and for superb sound reproduction you'll be glad you chose Agfa Ferro Color Cassettes – there's more to them than meets the ears!



### Practical aids in Agfa-Gevaert cassettes:

- 1. immediate positive identification of side one.
- 2. metal noise-shield avoids unwanted "hum".
- 3. knock-out tabs at rear of cassette prevent unintentional erasure (optionally either side).

4. screwed cassettes.



Agfa-Gevaert for still cameras, flash-guns, colour film for slides, prints and movies, magnetic tapes.

# RARE ADDITIONS FROM MARANTZ WORTH READING ABOUT. AND LISTENING TO.



Rāre: very valuable.
Addi'tions: the things added.
Ma'rāntz: a range of ultra-high

ma rantz: a range of ultra-nigh performance sophisticated components blending state-of-the-art engineering and operational versatility.

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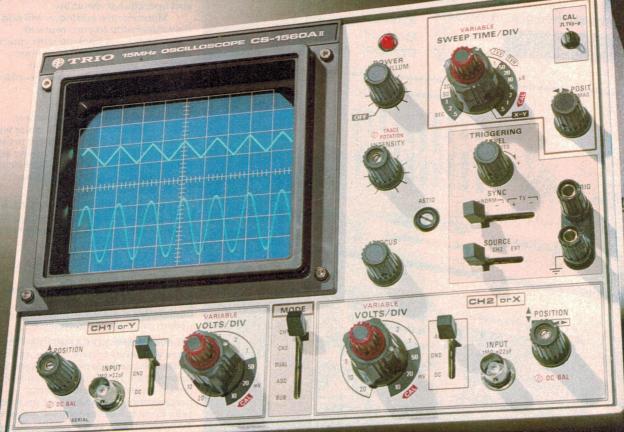
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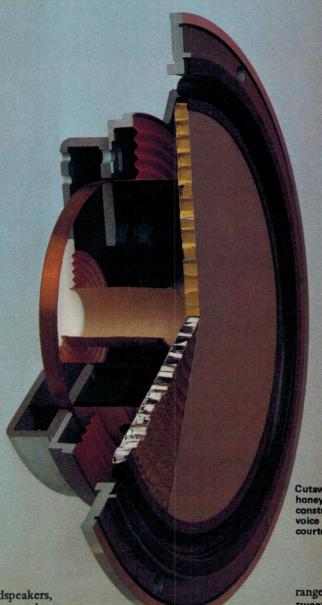
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# Revolutionary "honeycomb disc" drivers in new loudspeakers

Roger Harrison



Cutaway view of the Technics 320 mm honeycomb disc woofer showing the construction of the diaphragm and the voice coil (see also, page 142). Picture courtesy National.

A NEW RANGE of loudspeakers, released recently by Technics, employ revolutionary drivers having a special flat disc construction made of a unique aluminium honeycomb 'sandwich' said to have great advantages over conventional paper cone drivers.

Claimed to represent a "significant step forward" in the quest for realistic

material, Technics' honeycomb disc drivers have been incorporated in their new SB range of loudspeakers - the SB-SB-3, SB-5, SB-7 and SB-10.

Five honeycomb disc drivers were developed specially for this new range of speakers: a 320 mm woofer, a reproduction of complex musical 250 mm woofer, a 220 mm bass/mid- claimed advantages.

range, an 80 mm mid-range and a 28 mm

Compared with conventional cone diaphragm drivers, a flat diaphragm driver excels in two vital areas, according to Technics: smooth frequency response and simple alignment of acoustic centres. Let's examine how these honeycomb disc drivers are constructed and the reasons behind the

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AUDIO REFLEX

### 'Honeycomb disc" drivers

### Of pistons and paper

It is not without justification that the loudspeaker has often been called the weakest link in the chain of hi-fi music recording and reproduction. For over half a century the dynamic speaker, with its magnet, voice coil and paper cone, has remained principally the same, although great improvements have been made in many constructional details leading to the high quality drivers available today.

Nevertheless, much money and time has been spent in an attempt to develop "the perfect reproducer".

The familiar conical shape of the diaphragm of conventional loudspeakers was never a virtue of the basic design but a necessity forced upon speaker designers because of the need to obtain a rigid moving surface with a soft, pliant material - paper. The need for flat diaphragm speakers was apparent quite early in the piece, but solving the problem of obtaining a material suitable for the application, that did not exhibit significant resonances and was light, yet rigid, was beyond the technology of the times.

One of the serious limitations of a conventional paper cone speaker is the narrow frequency range over which it acts like a piston. Beyond a certain frequency, depending on the particular driver's construction, 'partial vibrations' occur on the cone – known as "cone break-up". Also, the semi-enclosed airfilled cavity within the cone volume has a resonance effect known as "front cavity effect" which limits the upper frequency performance of conventional drivers. Both of these effects reduce the usable bandwidth of paper cone drivers and contribute to distortion.

A further factor contributing to the limitations of conventional speakers is that the cone, being made of wood pulp, is difficult to manufacture with close uniformity from unit to unit. Secondly, its characteristics deteriorate over time, contributing to the gradual deterioration of a loudspeaker over its

Many manufacturers have gone to considerable lengths to overcome these failings, with varying degrees of success. They are contributing factors to the

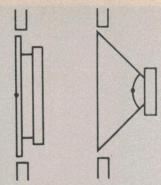


Figure 1. The dot shows the relative centres of a flat diaphragm driver (left) and a cone type driver

high cost of good quality paper cone speakers.

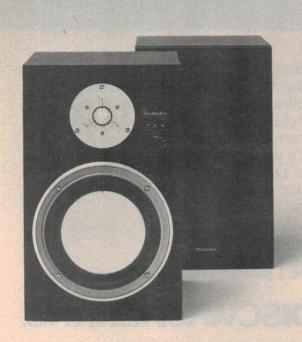
### Flat diaphragm speakers

The theoretical superiority of a flat speaker diaphragm over a cone type has been known for a long time. A rigid, flat diaphragm offers inherently lower distortion, a smoother frequency response, better dispersion and wider bandwidth. Flat diaphragm drivers offer a further advantage. The acoustic centre of a flat diaphragm driver is on the front surface of the diaphragm. A linear phase system is loudspeaker constructed by mounting flat diaphragm speakers on a plane surface. As the

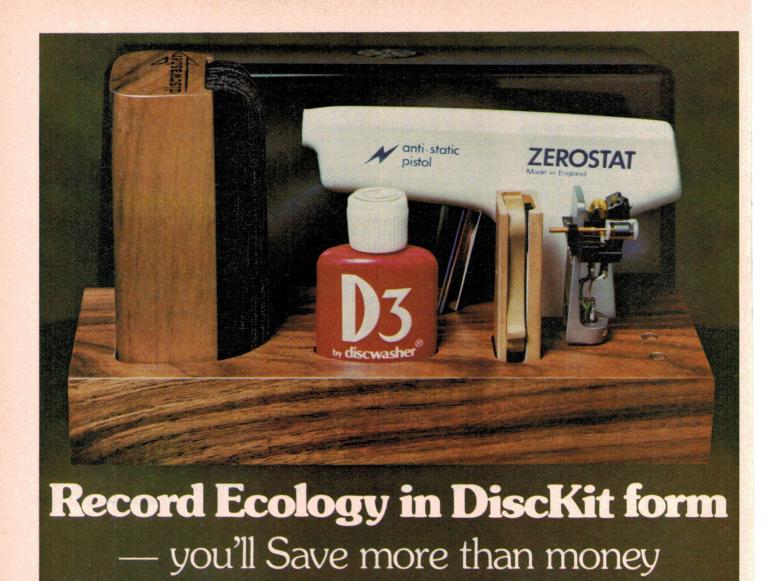
continued on page 140

At left is Technics' SB-3 two-way speaker system featuring a 220 mm bass/mid-range driver and a 28 mm tweeter — both employing honeycomb disc construction. At right is the SB-10

system. This is a three--way employing a 320 mm woofer, an 80 mm mid-range - both honeycomb disc types, and a special 'leaf' tweeter.







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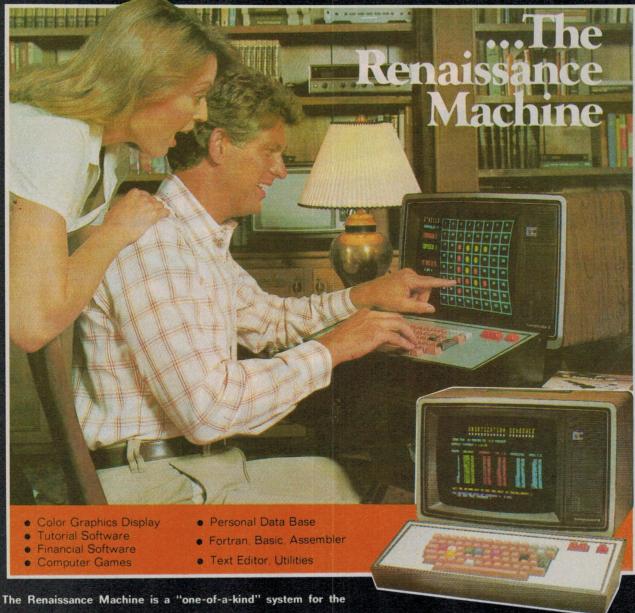
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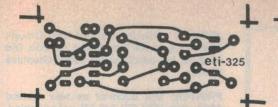
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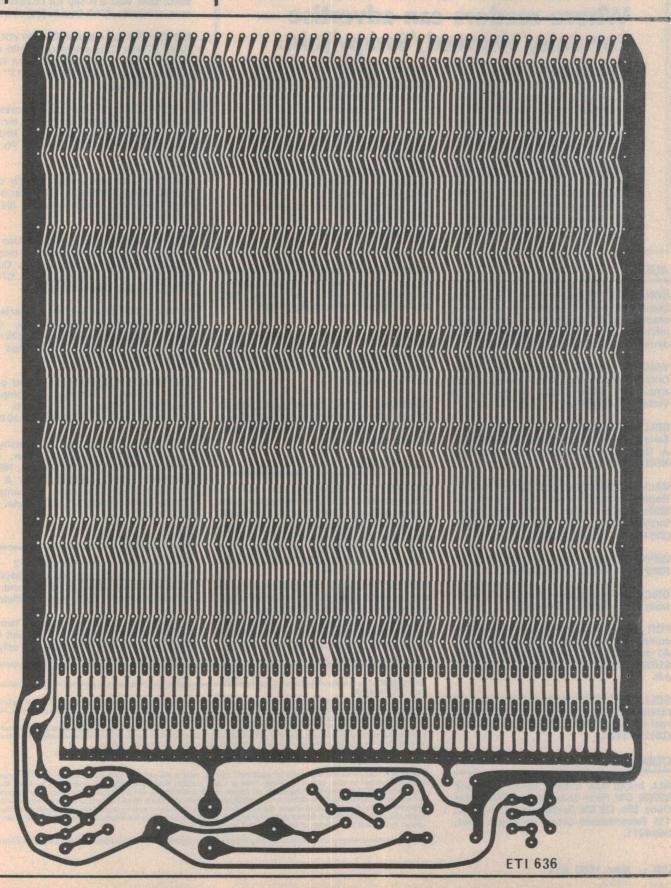
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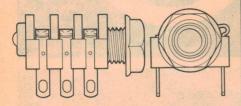
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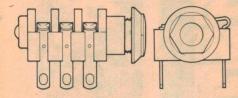
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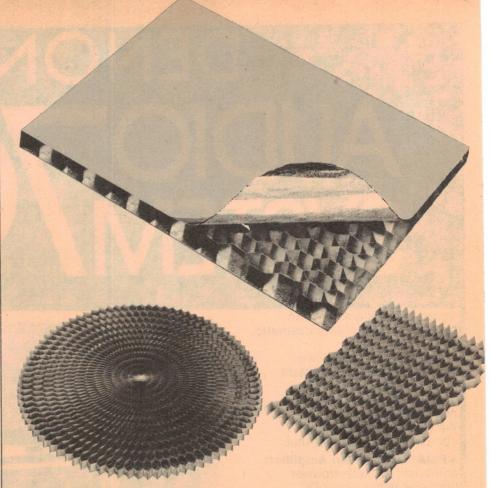


Figure 2. At top is a "honeycomb sandwich" structure (a). The basic honeycomb at bottom right (b), usually made of aluminium, is sandwiched between layers of thin metal foil. This is unsuitable for speakers however, and Technics engineers developed the circular structure shown at bottom left (c).

acoustic centre of conventional cone drivers is located near the voice coil, they have to be mounted on a stepped surface in order to align their acoustic centres, which gives a constructional disadvantage as well as introducing possible diffraction problems with the mid-range driver and the tweeter.

Attempts to develop a flat diaphragm driver have stepped up in recent years as the demand for better reproduction has increased. The quality of every other component in the reproduction chain has increased dramatically over the past decade, but the loudspeaker has lagged somewhat behind. You may remember one of the first successful commerciallyproduced flat diaphragm drivers was the B139, designed by well-known Raymond Cooke of the British KEF company. This uses an oval-shaped diaphragm made of polystyrene.

Whilst this approach was an early solution to the problem of providing a light, rigid planar diaphragm, Technics researchers looked at various techniques used in other branches of engineering aimed at producing light, rigid surfaces. In the aircraft industry they found that "honeycomb" structures are used in the floors, wings and other parts of civil and military aircraft.

The honeycomb structure consists of hexagonal 'cells' of a light metal aluminium) sandwiched (usually between thin sheets of light metal forming a 'skin' for the structure, as can be seen in figure 2, (a) and (b). The honeycomb possesses a very high bending strength, and is thus very rigid, yet very light weight.

However, this form of honeycomb construction is not ideal for a speaker diaphragm, Technics' engineers found. For a number of reasons, a circular diaphragm was decided as being the optimum shape and a honeycomb structure having "axial symmetry" was developed. A 'normal' honeycomb (with linear symmetry) and Technics axial symmetry honeycomb are compared in Figure 2, (b) and (c), above.

A normal honeycomb structure does exhibit the same characteristics in all directions, as it bends or flexes more easily in the transverse direction than in the longitudinal direction. In a speaker having a round diaphragm, this directionality would be an unwelcome characteristic, as the diaphragm needs to be equally rigid in all directions taken from the centre. Hence the development of the axial symmetry honeycomb core. The bending strength of this type of diaphragm is the same on any radius.

Another advantage arises from this form of construction. As its mass is greater towards the centre, its vibration 'nodes' also move closer towards the centre than for a solid disc of similar weight, but uniform density.

This helps to simplify driver construction, as we shall see shortly.

### Of modes and nodes

When a guitar string is made to vibrate at an octave above its fundamental frequency there will be a point, exactly half way along the string, that does not vibrate at all. Such points are called "nodes"

The same phenomenon can be observed in flat objects set to vibrate — such as drum heads and xylophone blocks . . . and speaker diaphragms. With vibrating flat objects, 'nodal lines' may be observed. In high school physics you may remember seeing this demonstrated where sand was sprinkled on a horizontal flat metal or glass plate that was supported at its centre. With the plate set to vibrate by drawing a violin bow across the edge, the sand would bounce about and settle in a characteristic pattern — along the nodal lines where it was not vibrating. A

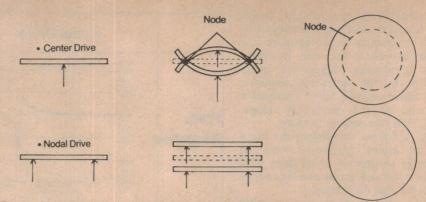


Figure 3. Illustrating the principle of "nodal drive". When driven at the centre the disc will tend to resonate and vibrate as shown at top. When driven at or near the indicated node line, this spurious vibration is eliminated.

variety of patterns may be generated in this way, each representing a distinct "vibration mode". A German physicist name Walter Ritz first examined the vibration modes of square diaphragms in 1909 and calculated the many modes possible.

Such vibration modes are distinctly undesirable in a speaker diaphragm as they introduce harmonic distortion. Remember that I mentioned the term "cone break-up" previously? This is where the speaker diaphragm changes its mode of operation from that of a piston and goes into various vibration modes as the drive frequency is increased.

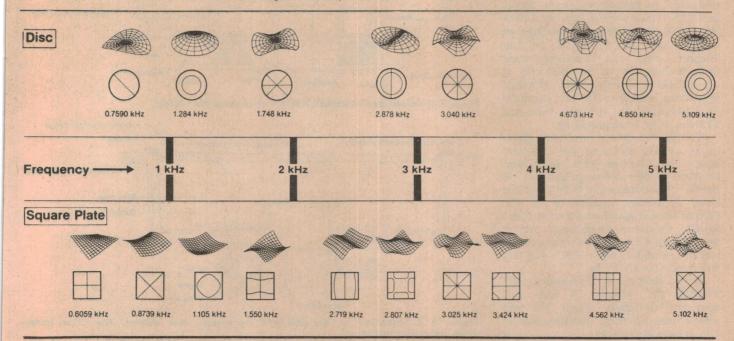
Where, and in what shapes, these nodal patterns appear on a speaker diaphragm depends on several factors, including the diaphragm's basic resonant frequency, its shape and the frequency at which it is driven.

A computer analysis of the nodal patterns of a disc and a square plate for a range of frequencies is given in the illustration here, showing that the disc has a simpler arrangement of nodal lines. This indicates that it exhibits less harmonic distortion as it is driven over a range of frequencies.

These unwelcome vibration modes can be prevented in either of two ways: by driving the diaphragm across its entire surface (which is technically extremely difficult and thus costly) or by applying the drive where it intersects the most nodal lines. Centre drive is undesirable as can be seen from Figure 4. "Nodal drive", as Technics call it, prevents spurious vibration modes forming, forcing the diaphragm to move as a rigid piston over a wide drive frequency range.

The dramatic effect on the usable frequency range of a disc diaphragm

Figure 4. Computer analysis of the modes of vibration of a disc and a square plate showing the flexing patterns and the nodal lines produced (lines of least vibration) when driven at different frequencies. Clearly, a disc has the least complicated variety of vibration modes. (All diagrams courtesy National).



with nodal drive, compared to centre drive, is readily apparent from Figure 5. Serious resonances occur at quite low frequencies when the disc is centre driven, producing pronounced peaks and dips in the frequency response. Nodal drive moves these resonances well up in the frequency range, extending it two octaves or more.

With a square diaphragm, the more complex nodal patterns make it impossible to provide nodal drive with a single voice coil across as wide a range

as with the disc diaphragm. Now, nodal drive for a disc diaphragm requires a voice coil and magnet structure that can drive the disc at a considerable distance from the centre. Technics have solved this problem with two basic construction methods. A cross-section of the 320 mm woofer shows one form of construction. The voice coil in this driver is 160 mm in diameter! This woofer is used in the new SB-10 loudspeaker and, although crossed over to the mid-range driver at 400 Hz in this design, it can be used to 3.3 kHz, Technics claim. The reverserolled edge construction prevents spurious sonic radiation from the edge of the diaphragm near the upper frequency limit of the driver's range.

The other type of construction is illustrated in Figure 7. This shows the 250 mm woofer where the voice coil mounting bobbin applies nodal drive to the diaphragm via a rigid cone.

top-of-the-line model Technics' SB-10 loudspeaker is a three-way, threedriver combination employing the 320 mm honeycomb disc woofer, the 80 mm honeycomb disc tweeter and a new "leaf" tweeter. The bass is crossed over to the mid-range at 400 Hz and mid-range to tweeter crossover occurs at 4 kHz. The system is rated at 100 W DIN (150 W music) and develops an output level of 87 dB/W at 1m. Technics claim the frequency range extends from 28 Hz to 125 kHz at 10 dB below average level. Nominal impedance is 8 ohms. The unit measures 711 mm high, by 402 mm wide and 318 mm deep. It weighs 32 kg.

The SB-7 is also a three-way, three-driver system and uses the 250 mm honeycomb disc bass driver, the 80 mm honeycomb disc mid-range and the leaf tweeter. It is rated at 90 W DIN and the lower frequency extends to 34 Hz. Output level is specified the same as the SB-10. Crossover frequencies are at 900 Hz and 4.5 kHz. The unit is a little smaller, measuring 630 x 360 x 318 mm and it weighs only 19 kg.

Only time and experience will adjudge the success of this new approach to driver design. We will review one of these loudspeakers in ETI as soon as possible.

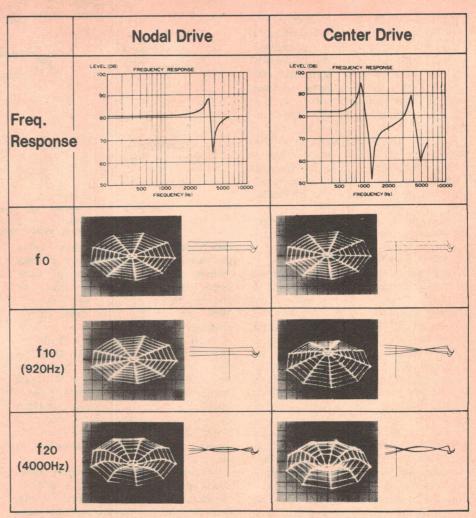


Figure 5. Illustrating how the frequency response of a disc, i.e.: its range of 'pistonic motion', is extended by nodal drive.

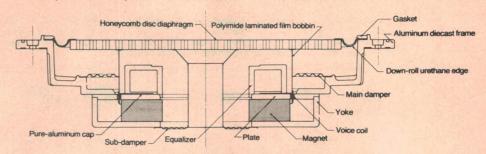


Figure 6. Cross-section of Technic's 320 mm honeycomb disc woofer.

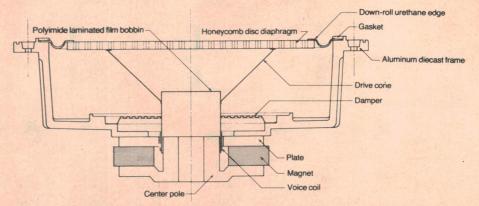


Figure 7. Cross-section of the 250 mm honeycomb disc woofer. The other honeycomb disc drivers are similar.

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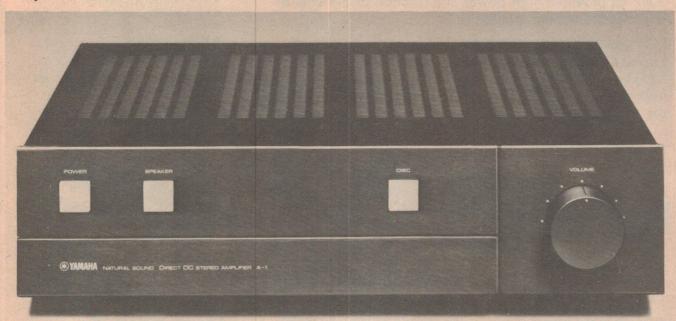
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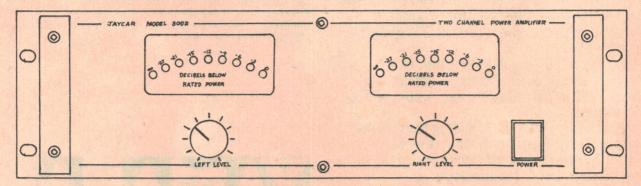




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# Preamp-power amp duo from S.A.E.

The SAE model 3000 preamp and associated model 2200 power amp, coming from a company renowned for quality products, do not rest on the laurels of their predecessors.

THE SAE MODEL 3000 preamplifier and the associated 2200 stereo power amplifier are two attractive pieces of equipment from an organisation which is already renowned for the quality of its products. The most striking feature of the combination are the number of controls and their layout which appear deliberately designed to complicate what might otherwise have been a far simpler panel appearance.

Both of these pieces of equipment are designed for rack mounting and when mounted in either a portable or permanent racking system, do provide a striking and attractive appearance. The design is in keeping with the current American consumer vogue which is primarily aimed at impressing your friends and neighbours as much as impressing the purchaser.

### **Features**

The 3000 preamplifier has its controls laid out in three basic rows and with three major groupings from left to right. On the extreme left hand side of the amplifier is a power on/off switch with a headphone socket immediately below. Adjacent to these are two columns of controls with Channel A and Channel B

controls side by side.

The top row contains the two treble controls, below it the two mid-range controls and at the bottom the two bass filter controls. The treble provides a nominal of +15 dB of boost and cut at 20 kHz, the bass a nominal +15 dB of boost and cut at 20 Hz and the mid range +7 dB range at 1 kHz.

The central group of controls provide tape controls in the top row with four push buttons whose function are not clearly evident from the designations, but this is soon cleared up by the handbook. These buttons make it possible to monitor source or tape, monitor tape 1 or tape 2, copy from tape 1 to tape 2 or tape 2 to tape 1 and tape on to one recorder while monitoring another.

Although not as well designated as we would desire, getting used to them is a relatively simple task and they do provide excellent flexibility.

In the row below the tape control switches are the low pass filter switches with a 30 Hz and 100 Hz cutoff frequencies, plus a tone control defeat switch which has the ability to switch the tone controls into the tape recorder circuit path or in the normal preamplifier line circuit.

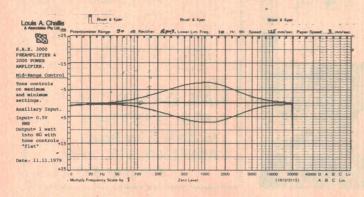
In the bottom row is a balance control which provides up to 40 dB differential balance adjustments between left and right channels.

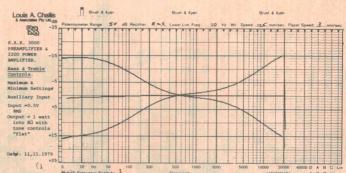
The central group switch controls are a -12 dB mute switch, adjacent to which are three mode controls for mono A, mono B, stereo or reverse, whilst in the bottom row is a fader volume control with a -70 dB to a maximum gain with calibrations of 70, 40, 35, 30, 25, 20, 15, 10, 5 and zero dB.

The rear of the amplifier features inputs by standard coaxial sockets for two photo cartridges, tuner or auxiliary, tape 1 in and out, tape 2 in and out plus outputs to two amplifiers.

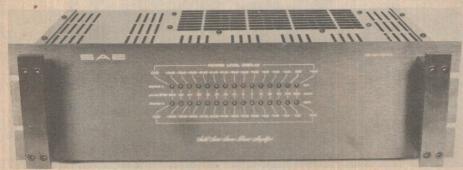
Whilst the unit comes wired and labelled 240 volts ac, 50/60Hz, it is interesting to note that the ubiquitous switched and unswitched sockets which do not comply with Australian Electrical Supply Association's rules are still located on the rear of the unit.

The power amplifier has the same sort of bold black appearance as the preamp but it is not as easy to mount in a 19" rack. It is however, more interesting in many respects than the preamplifier. The first and foremost eyecatching factor is the use of an array of light









emitting diodes as a power level display. This incorporates diodes which read with 3 dB incremental steps from -36 dB to +3 dB. This corresponds to power levels from .02 watts to 200 watts in to 8 ohms, together with an idle position which indicates that the amplifier is operating. LED arrays like this provide a graphic and exciting display when the unit is in operation and are as functional as they are attractive.

One feature we did not like on the front panel was the use of impractical handles which, regrettably, have dangerous sharp corners of the type we criticised so strongly in the Jands J600 amplifiers three years ago.

The rear of the amplifier features an internal heatsink construction with a very open area for cooling air paths. These are cleverly designed and obviously effective. The rear of the amplifier features two coaxial input

sockets, large universal terminals for input and output and a two-wire mains lead with parallel pin plugs intended to be plugged into one of the switched mains outputs of the preamplifier.

The constructional features of both the preamplifier and the main amplifier are exemplary and it is interesting to note that the power amplifier incorporates a large toroidal transformer which is the heart of the power supply for the unit. Both the units are well constructed and the designers have placed a lot of thought and emphasis in providing good operational flexibility.

# On test

The frequency response with the tone control 'centred' or 'defeated' is essentially unchanged, extending from 5 Hz to 67 kHz and is ably supplemented in the low frequency region by the two

lot cut filter positions which allow programme hum or room resonance disabilities to be minimised.

The hum and noise levels of the unit are not quite as low as we would have expected and on the phono input the level at -65 dB linear (unweighted) and -68 dB (A — weighted) are acceptable but certainly not superlative. The auxiliary input produces a comparable level of hum and consequently it would appear that it is the output stages of the preamplifier which is generating that level of hum.

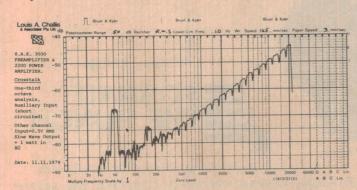
The distortion characteristics of the amplifier are, however, exemplary and at the 100 watt level the performance is almost in the category of being "state of the art".

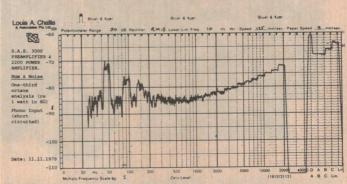
At 100 Hz the distortion level is a maximum of .024%, at 1 kHz .009% and at 6.3 kHz .013%. At lower power levels the distortion levels are even lower still and are, without a doubt, a credit to the system's designers.

We were surprised that the distortion in the left channel and the right channel were significantly different, with the left channel generally producing higher magnitudes than the right channel produced. Even so, the left channel produced inconsequential levels of distortion and the difference between the channels is really of academic interest.

Subjectively

The subjective impressions of the amplifier's performance were outstanding. Firstly, the flexibility of the preamplifier stage showed through to the fore under the real life living room conditions. We were pleasantly surprised by the ease with which we could copy from one recorder to another and even more so by the general ease with which other equipment could be interconnected and played through the







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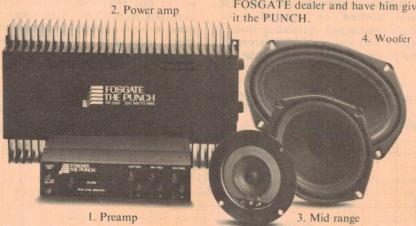
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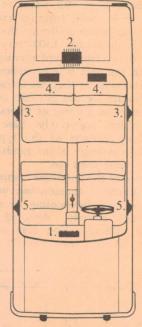
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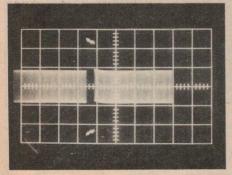


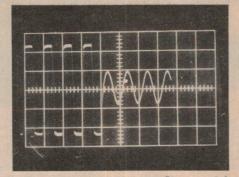


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# review





Transient overload recovery test for the S.A.E. preamp and power amp system. Picture at left shows oscilloscope trace of output with sweep speed of 50 ms per division. The right hand picture is the same waveform expanded to 1 ms per division. (10 dB overload re rated power into 8 ohms, both channels driven; overload duration - 20 ms, repetition rate - 512 ms; IHF-A-202).

system. The preamplifier, amplifier and associated peripherals fit well in a mobile racking system which we used for the evaluation. We employed a system based on an Audio Technica AT-30E moving coil cartridge mounted in a Technics direct drive turntable. The output was monitored on a pair of Quad electrostatic speakers.

The transparency of the sound, lack of colouration and superb transient response of the system was fully evident. With the electrostatic speakers the amplifier hum level was undetectable at normal programme levels but wideband

hiss was just detectable close to the speakers. With a sub-woofer system connected, the hum was just detectable at 100 Hz. The hum and noise is dominated primarily by wideband transistor noise. This does produce an audible hiss at maximum amplification levels.

Summary

The SAE 3000 preamplifier and 2200 power amp are a well-designed system providing generally exemplary performance with an unusual degree of flexiibility. Whilst we were not initially enraptured by the appearance of the pre-

amplifier we soon found that the designers had done a very good job in providing a degree of functionality greater than the average user could reasonably ask for.

We rate this combination highly in terms of performance and most particularly for its operational flexibility.

# SAE MODEL 3000 PREAMPLIFIER AND 2200 POWER AMPLIFIER

**PREAMP MODEL 3000** 

Dimensions: 483mm wide x 132mm high x 130mm deep

Weight: 4.7 kg.

Price:

POWER AMP MODEL 2200

Dimensions: 483mm wide x 133mm high

x 203mm deep

Weight: 11 kg.

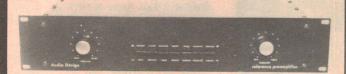
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		MDA GUIDED	PERFORMANCE OF	HARMONIC DISTORTION: (at rated power of 100 watts		100Hz Right	Left	1kHz Right	Left	6.3kHz	
Louis A Challis and Associates Pty	22	000 PREAMPL	CPLER (S.N. 2902) AND S.A.E. PLIFIER (S.N. 8420)		2nd 3rd 4th 5th		-85.4 -90.6	-89.4			-84.8 dB -80.0 dB dB
Louis A Chailis and Associates Pty	Ltd				THD	.017%	.024%	.005%	.009%	.013%	.01%
Our Ref: E27  FREQUENCY RESPONSE: (-3dB re 1 watt, 0.5V Input to Aux.)	Left: Right:	Tone Control  4Hz to 70k 5Hz to 67k			2nd 3rd 4th 5th	-80.5 -89.9 -92.9	-77.1 -87.0 -90.2	-91.8 -92.3	-86.5		-82.7 dB dB dB dB
	Left: Right:	Tone Contr 4Hz to 73k 4Hz to 72k		TRANSIENT INTERMODULATION DISTORTION: (3.15kHz square wave and 15kHz sine wave mixed 4:1)		Less th	nan 0.18				
SENSITIVITY: (for 1 watt in 80)*	Aux.: Tuner: Tape: Phono: Overload:	Left 12.5mV 12.5mV 12.5mV 12.5mV 120µV 260mV	Right 12.6mV 12.6mV 12.6mV 120µV 260mV	NOISE & HUM LEVELS:  (re 1 watt into 80)  (with volume control set for 1 watt output with, 0.5V input -Aux.  5mV input -Phono)		Aux.: Phono:	-66.50 -64.00	dB(Lin)		. OdB (A)	
INPUT IMPEDANCE:	Aux.:	Left 43kΩ	Right 43kΩ	MAXIMUM OUTPUT POWER AT CLIPPING POINT: (IHF-A-202)		96V P-1					
	Tuner: Tape: Phono:	43kΩ 43kΩ 42kΩ	43kΩ 43kΩ 43kΩ	(20mS burst repeated at 500mS intervals)		Dynamic	c Headro	oom = 1.	.6dB (re	e 100 wa	tts)
OUTPUT IMPEDANCE:	0.17Ω (			*Note: This sensitivity may recontrol is at maximum. may be higher with tor	. Fig	ures que	ition o	f tone i	switch wone in,	when gar sensit	in vity

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# You have to be very confident before you claim anything will permanently remove static electricity from a gramophone record.

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Derek Pugh of Concept Audio confidently introduces to Australia a remarkable new product. It's called Permostat. And it permanently renders records free of static electricity.

What is this thing called static?

The contact of two dissimilar materials is liable to cause an exchange of electrical charge. Thus when a record is removed from its sleeve, subjected to cleaning by a pad or brush or is in contact with a stylus, the record surface is inevitably left in a highly charged state.

### What are the effects of static?

Not unlike a common magnet attracting iron particles, static scavenges and draws dust particles onto the record surface where they can be pushed along the grooves, creating various degrees of distortion. A highly charged record surface can cause micro discharging, uneven cartridge attraction and alteration of the stylus tracking force, resulting in wow and flutter, distortion and record stylus wear.

### Permostat?

Permostat is a uniquely formulated fluid which when applied to a record totally and permanently eliminates static.

How permanent is permanent?

It is claimed that playing a record one hundred times corresponds to the normally expected use of a given record by a consumer. This is also the number of plays used by record companies for evaluating their products. Tests prove that Permostat eliminates static for at least one hundred continuous plays.

Are there any adverse effects?

Laboratory tests confirm no detectable change in sound quality, surface noise, frequence response and fidelity.

Who produces Permostat?

Permostat has been researched, developed and produced by the British firm, Milty Products, a leader in the field of record care and maintenance, whose Pixall record cleaner has already won the coveted Japanese Grand Prix award.

Where can I buy Permostat?

You'll find Permostat in all good hi-fi, audio, record and department stores. However, if you have any difficulty in obtaining Permostat, please fill in the coupon below.

Dear Derek Pugh. Permostat had better permanently render my records free of static. Or I shall be making one or two phone calls.

(BLOCK CAPITALS PLEASE)

Name

Address

Please supply (state quantity required)

Permostat Kit(s) @ \$15.95 ☐ Permostat Refill @ \$9.95 ☐

P&P Incl. I enclose a Cheque/P.O. value \$

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Preamplifiers: SAE make a comprehensive range of high quality low distortion preamplifiers. All models include two stage Phono Circuit tape facilities and filters. Two of the range incorporate parametric equalization.

**Equalizers:** There are three parametric equalizers in the range, all of which are three octave and

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Impulse Noise Reduction System: This is a specifically designed unit to reduce the "click" and "pop" (impulse noise) which are present in phonograph records and other program sources.

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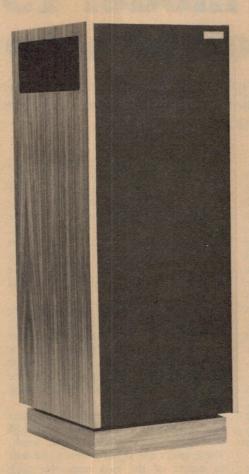
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# Marantz model 1300DC stereo power amp

Louis Challis found this amplifier "... an excellent example of careful design and planning. What has resulted is a first class piece of electronics."

IT IS ONLY a few weeks since we tested a high powered Marantz receiver (the model 2600, April issue . . . Ed.) and as a result, the model 1300DC amplifier is of particular interest to us. One might think from the size, most the weight, particularly unquestionably the power output developed by the range of Marantz amplifiers and radio receivers which are submitted to us, that the catch cry of the Marantz Dompany is "big is beautiful". This is another particularly good example of the design trend which is still very much in vogue in the USA.

# The unit

The appearance of the 1300DC is impressive. Whilst it most certainly would not be everybody's cup of tea, it is nonetheless clear that from an ergonomic standpoint the designers have done a commendable job.

The major controls are cleverly aligned in the centre level of the three rows of controls located on the front panel. The front panel is unusual, firstly in that it incorporates a panel fascia which extends beyond the main face by about 3 mm. This panel has, on the left hand side of the top row, push button switches for the two phono inputs, tuner and auxiliary, only one of which can be selected at a time, with

push button switches for tape 1 and tape 2 monitor, adjacent. On the right hand side of the escutcheon is a tone defeat push button, and switches for selecting turnover frequencies for the bass and treble controls of 100 Hz and 10 kHz respectively. These can change the base turnover frequency from 500 Hz to 100 Kz and the treble turnover frequency from 2 kHz and 10 kHz.

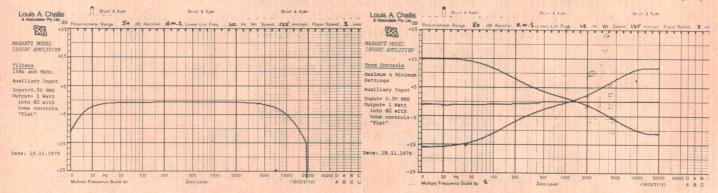
Two other filter switches are provided, one a low cut filter, with an 18 dB per octave slope with a corner frequency of 15 Hz, together with a 9 kHz high cut filter with similar characteristics. The last switch in the top row is a conventional 20 dB muting switch.

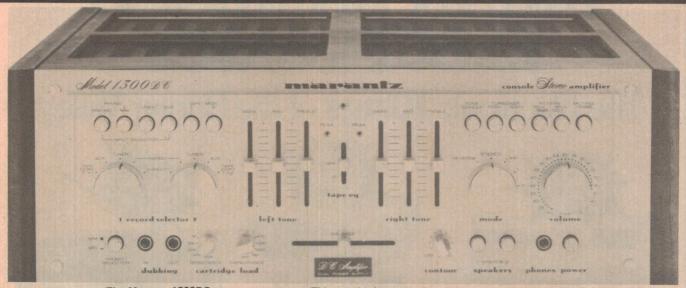
The middle row of main controls has two record selector switches instead of the more conventional single knob. These select the signal source to be sent to either of the two respective tape recorders which may be connected to the unit. Record Selector 1 switch is intended to provide the input for the main recorder whilst the Record Selector 2 switch is intended to select the inputs of the secondary or optional tape recorder. Both of these rotary selector switches can operate independently of the main input selector push buttons and they each

provide facilities for direct connection where the audio signal from the chosen source, selected by the input push buttons, is either directly connected to a tape recorder or alternatively one tape recorder is connected to the other tape recorder. Possibly more important, they make it feasible for tape recording to take place from one input whilst monitoring or listening to another input which may or may not be recorded simultaneously and may or may not be re-equalised simultaneously.

Obviously there are other ways to solve this problem and it does take some careful thought and comprehension of the philosophy of this design facility in order to prevent accidental disconnection of a signal source which is being recorded or monitored. Most people are obviously more used to a more conventional and somewhat simpler arrangement for providing these sorts of facilities, but there can be no denying that the concept Marantz have chosen does provide a greater degree of flexibility, even though the route by which it is chosen may not appear the most direct.

Marantz have incorporated three tone control circuits for each of the two channels? a bass, a mid-range and a treble control. These are vertical sliders with mechanical indents to simplify





The Marantz 1300DC stereo power amp. This one is shown in the optional wooden cabinet.

setting. Slider controls are preferable to rotary switches or horizontal faders and are ergonomically well designed as they give a graphical indication of what is happening in a simple and direct manner. Between the two sets of tone controls for the left and right channels Marantz have incorporated the tape equalisation switch. This allows the reequalisation of program content being fed from the record player, tuner or auxiliary input, and more importantly, being fed from the main tape recorder to the secondary recorder.

In the upper position with the tape equaliser switch set to the "one" position recording should take place on the main recorder, whilst in the "two" position, onto the secondary recorder.

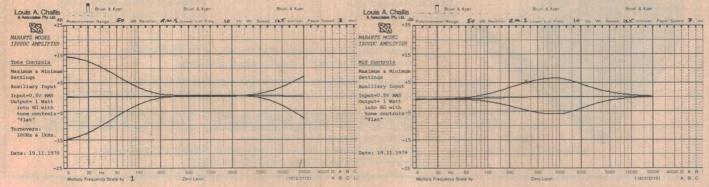
Flanking this tape equalising switch are two peak overload lights which operate when either amplifier reaches the clipping point (200 watts output into 8 ohms). On the right hand side of the tone control circuits is a mode switch for reverse and normal stereo,

left plus right, and left or right respectively. The volume control is located at the extreme right and features mechanical indents and a calibrated 80 dB dynamic range. The bottom row of controls contains push button for selecting moving magnet or moving coil cartridges at phono 1 selector input, two standard tip and sleeve microphone sockets, sensitivity suitable for normal dynamic microphones, and rotary switches for selecting moving magnet cartridge input impedances. These provide for impedances of 1k ohm, 10k, 27k, 47k and 100k ohms, and capacitances of 100, 150, 220, 330 picofarads, which facilitates optimum termination of a wide range of cartridges.

In the centre of the bottom row is another slide control with indent, which is located in the horizontal plane for balancing the two channels. To its right is a contour switch for setting the loudness contours. This has a sensible off position at the extreme anticlockwise

end. Two speaker push buttons are provided for selecting system 1 and 2, with a minimum impedance of 4 ohms total. The remaining controls are a tipring-and-sleeve headphone phono socket and a mains power switch. The power switch is coupled to a LED which is located at top centre on the front escutcheon.

The front panel is fabricated in a light, gold-anodised, brushed satin aluminium with black stencilled lettering. The cabinet cover is in black, vinyl-coated steel, with an extensive area of slots to provide good ventilation for the electronic circuitry. The rear panel, which is set a long way back from the front panel, has been restructured for the Australian market. It does not switched incorporate the unswitched outlets that the Japanese and American models contain. More important, it also incorporates the very useful addition of DIN record/replay sockets to simplify inter-connection of the external tape recorders.



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# The new generation of factory-built or kit-set Peerless loudspeakers



It's true most speakers look alike and that price alone never tells the whole story. But now the new generation Danish-built Peerless loudspeakers give you a recognizable difference in sound quality-a difference that has set Peerless a notch above the others for over 50 years.

The range of new generation Peerless loudspeakers includes the fully assembled PAS series plus the moneysaving PLK kit-sets. Both series contain drive units with the following characteristics.

Peerless 'X' Line Woofers

☐ Large ceramic ferrite magnets for high power handling. Specially coated cones reduce colouration to a minimum.

Cones are supported by a single-roll foam or rubber surround to maintain excellent linear motion. 

Bass response is clean and tight at all listening levels.

☐ Sealed back units prevent interaction with the woofer. Distortion and colouration are reduced to a minimum. 

The rear side of the cone is coated with a special damping material to eliminate colouration. 

Specially impregnated polyurethane cone rim provides high degree of linearity.

Dome tweeters designed for the highest accuracy of reproduction with low distortion flat response and wide dispersion. 

The sealed back isolates the tweeter from interference. 

Specially developed dome fabric ensures no degradation of performance even after prolonged heavy loading.  $\square$  Assembly mounted on a precision diecast plate where rigidity ensures permanent alignment.

Peerless Dividing Networks

☐ Peerless crossovers use air-cored chokes for maximum power handling, and special electrolytic capacitors to ensure long term reliability. 

All components are mounted on fibreglass printed circuit boards for maximum durability, while coded clip connectors eliminate the need for soldering.

Power handling

The power handling capacity is high and conservatively rated at 100W RMS, however, due to the high efficiency of Peerless speakers, the recommended amplifier power is between 25-100W RMS.

Whether you settle for the smart timber-veneered PAS assembled series or the PLK kit-set, you're getting the same Danish-made Peerless quality - a quality selected by many of the world's most reputable names in loudspeakers, for inclusion in their own speaker systems.

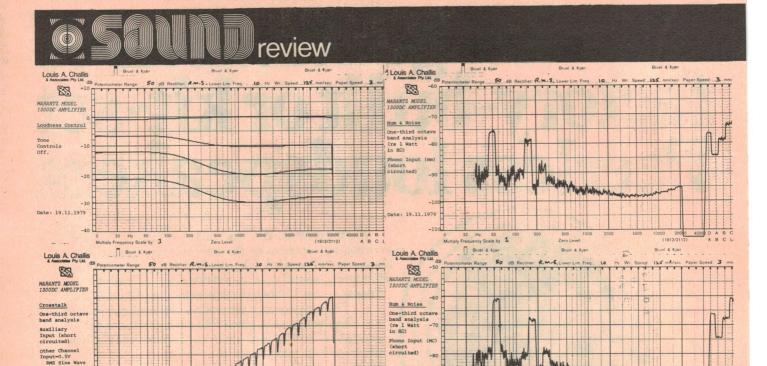
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Another notable difference between this amplifier and other units is the incorporation of a fifth foot squarely under the middle of the unit. This distributes the loading which is actually at its greatest underneath the centrally located transformer.

Date: 19.11.1979

The inside of this amplifier is as impressive as any piece of professional equipment that we have recently seen. The first and most obvious feature are the two separate power supplies used to feed each of the output power amplifier stages. Whilst these are derived from a single, large fully-screened conventional power transformer, the actual windings for the two power supplies, the filter circuits, regulators, protection circuits and capacitors are completely separate.

Visual inspection shows that the designers have gone to a great deal of trouble to provide high strength and good ventilation in the thermal dissipation paths. One was immediately aware of the excellent accessability for maintenance purposes and the extent of their care in maximising screening to minimise electrostatic and electromagnetic induction problems between the input circuits at the rear of the amplifier and the switching and control circuits located at the front.

In the low level circuits the designers have made very extensive use of flat ribbon cables as well as board mounted regulators to feed preamplifiers, to achieve a better performance and reliability. Whilst the components are in

the main commercial or consumer type standard the construction appears to be highly professional and this particular unit would obviously fair almost as well in professional usage as it would in its obviously intended role as a consumer based amplifier.

Date: 19.11.1979

## On test

The objective testing of this unit showed that it has excellent performance. The frequency response extends from 1.4 Hz to 150 kHz with the tone controls defeated. This drops to 82 kHz with the tone control centred. The input sensitivities were 12 millivolts for auxiliary input, tuner and tape, 125 microvolts for the moving magnet phono input and 20 microvolts for the moving coil input. The overload sensitivity for the moving magnet input is 280 millivolts which is more than adequate.

The amplifier's output impedance is less than 80 milliohms, and in a real situation would be limited by speaker cabling and not by the amplifier itself.

The harmonic distortion of the amplifier at the 150 watt level is excellent with 0.08% at 100 Hz, 0.05% at 1 kHz and less than 0.02% at 6.3 kHz. At the 1 watt level these figures are substantially lower, being .003\$, .005% and .004% respectively. The transient intermodulation distortion is very much less than 0.1%, whilst the hum and noise levels are better than 92 dB(A) on the auxiliary input, -84 dB(A) on the

moving magnet input, and 74 dB(A) on the moving coil input. The transient overload recovery of the unit proved to be impeccable. The crosstalk between channels is very low, but is a function of frequency. Even at 20 kHz this is still better than 50 dB and this is obviously the result of the use of two separate power supplies.

# Subjectively

We were unable to technically fault any of the unit's measured parameters and so we proceeded to our subjective evaluation. We first monitored the output through two pairs of highpowered JBL110 loudspeakers. The outputs could be readily pushed to 110 dB at three metres with no significant distortion. We then evaluated the amplifier with a pair of Quad electrostatic speakers. The lack of coloration and the unit's performance was quite impeccable. We noted at the maximum gain position that the hum and noise levels were inaudible on any of the selected programme content and at any of the listening levels at which we played the equipment.

Whilst the facilities are, in the main, conventional it became obvious that if one intended to dub from one tape recorder to another the record selector facilities provided by the two selector knobs provided distinct advantages over the more conventional controls with which we are accustomed. Whilst we were impressed by, and found the major

controls ergonomically attractive, the actual number of controls and their distribution did not immediately provide a feeling of ease. Obviously, with continuing use such discomfort would soon be obviated by familiarity. But unlike some of the other American amplifiers which we have recently tested we feel that the ergonomic concepts of this unit, independently from their technical functions, have been well thought out and these are backed up by

excellent electronic design.

Summary

The Marantz 1300DC amplifier is an excellent example of careful design and planning. What has resulted is a first class piece of electronics. Whilst we do not personally like the styling, once again we have to admit our grudging admiration for the circuit designers who have produced such an excellent piece of equipment.

### MARANTZ MODEL 1300DC STEREO AMPLIFIER

Dimensions: 416 mm wide x 146 mm high x 430 mm deep.

Weight 24.5 kg. Price: Manufactured by Marantz Company of U.S.A.

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				HARMONIC DISTORTION:		100Hz	1kHz	6.3kHz	
				(at rated power of 150 watts	2nd	-74.9	-83.7	-79.5	dB
	MEASURED	PERFORMANCE	OF	into $8\Omega = .346 \text{ Volts}$ )	3rd	-62.6	-66.8	-82.9	dB
MARAN	TZ 1300DC A	MPLIFIER (S.	N. 91A010087)		4th	-93.5	-95.2	-	dB
Louis A Challis and Associates Pty Ltd					5th	-93.5	-		dB
					THD	0.076%	0.046%	0.013%	
FREQUENCY RESPONSE:		Tone Contro				100Hz	lkHzl	6.3kHz	
(-3dB re 1 watt, 0.5V	Left:	1.3Hz to 82		(at 1 watt into 8Ω)	2nd	-71.2	-86.7	-89.4	dB
Input to Aux.)	Right:	1.4Hz to 85			3rd	-75.1	2 - 0	-95.	dB
			ols Defeated		4th	-86.2	-	-	dB
	Left:	1.2Hz to 11			5th	-86.1		-	dB
	Right:	1.3Hz to 11	L5kHz		THD	0.033%	0.005 %	0.004%	
SENSITIVITY:		Left	Right	TRANSIENT INTERMODULATION DIS	TORTION:				
(for 1 watt in 8Ω)	Aux:	12mV	12mV	(3.15kHz square wave & 15kHz					
	Tuner:	12mV	12mV	sine wave 4:1 (Output 150watts	) Less th	an 0.1%			
	Tape:	12mV	12mV	NOISE & HUM LEVELS:					
	Phono (MM	1) 1251IV	125µV	(re 1 watt into $8\Omega$ )					
	Overload	280mV	280mV	(with volume control set for		Aux:	-82dB(Lin)	-92d	B(A)
	Phono (MC		20μV	1 watt output with,		Phono (MM)	~72dB(Lin)	-84d	B(A)
TAININ THRUNANCE	Thomas (rec			0.5V input (Aux)		Phono (MC)	-60dB(Lin)	-74d	B(A)
INPUT IMPEDANCE:	2000	Left 39kΩ	Right 39kΩ	5mV input (Phono MM)					
	Aux: Tuner:	39kΩ	39kΩ	0.5mV input (Phono MC)					
		39kΩ	39kΩ	MAXIMUM OUTPUT POWER AT					
	Tape:	39846	3981	CLIPPING POINT:					
and other values of	Phono (M)	M) 47kΩ	47kΩ	(IHF-A-202)					
impedance as per spec.	Phono (MC	C) 50Ω	50Ω	(20mS burst repeated at		114V P-P			
				500mS intervals)	-	203 Watts			
OUTPUT IMPEDANCE:	@ lkhz =	= 80 milliohn	ns	Dynamic He	adroom =		150 Watts	)	



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In 1978 DISCPROTEC won the coveted Grand Prix Gold Award in Tokyo.

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You simply spray DiscProtec fluid on your record. The liquid "carrier" immediately evaporates, leaving a tiny amount of solid lubricant and antistat. A few moments of buffing and DiscProtec is evently distributed to create a sub-microscopic layer of protection. Surface static charge is eliminated and surface tension is vastly reduced, creating a very slippery surface (you can actually feel the change as you buff). It is this layer, just a few dozen molecules thick, which will protect your records from further deterioration during playing or storage.



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# **Akai PS-200T tuner**

Incorporating the latest in technological features, this tuner "... is one of the most exciting we have evaluated".

WITH ALL the attention on digital quartz watches, synthesizers and other esoteric equipment, it is not surprising that many manufacturers should offer receivers and tuners with digital displays for the frequency selection and other features which are in keeping with the electronic revolution.

Akai have recently released their new PS range of preamplifiers and separate power amplifiers. It is not surprising that the PS200T is designed to complement these two pieces of equipment. This tuner is remarkably large but, quite apart from its size, is particularly attractive. The front panel has a brushed satin aluminium front into which is inset a bronze anodised escutcheon. In the top left hand section of this insert is the digital display. This utilises large, green numerals and letters to designate the mode of operation, the frequency and other information.

The FM or AM mode and the frequency, in either MHz or kHz, is designated on the display. The display also indicates whether a preselected station is in operation and if the preselection function is being utilised. At the top right hand corner of the digital display are five bezel lights to show the incoming signal's relative strength, a display to show whether the FM frequency lock is operational and a multipath signal indicator to alert the user of the presence of signals with significantly different path lengths which are the antennae and the stereo detector.

The last indicator in this area operates when a stereo signal is detected by its pilot tone so that the user can tell whether he is listening to a stereo or a mono station. On the right of this display are three touch controls of the basic type utilised for all operational functions, with the exception of the mains switch. The uppermost control stops the frequency scanning and locks it, except when the automatic preset

control is operating. Below this are two arrow-shaped top controls to select either an upward or downward scanning mode. If these are operated at the ends of the frequency range on either the FM or AM mode the switching cycle reverses itself automatically and proceeds to scan in the opposite direction unless stopped by the control or through the selection of a preset station.

Immediately below the digital display and the upward/downward scanning touch controls is a row of fifteen preset station selector touch buttons together with a memory light and memory activator switch. These controls, which provide fifteen memories for FM, are activated through touching the memory switch with a frequency selected on the display and then subsequently touching one of the preset station controls which then 'remembers' that particular frequency.

## **Features**

Unlike a previous generation of synthesizer tuners that we examined some years ago which forgot the frequency the moment the mains was turned off, Akai have incorporated a little battery pack at the rear of the unit. In the absence of mains power, like the proverbial elephant, the memory remains operational and does not forget. Notwithstanding, even without the batteries, the CMOS circuitry has the capacity to remember for some minutes.

The heart of the memory system is a four-bit, one chip microcomputer which holds all the data and with the preset address memory which can memorise up to thirty stations. Frankly, there are less than fifteen AM stations that I would "want to remember" and regrettably only four FM stations in Sydney at the moment. Even so, the facility is there even though the stations may not be.

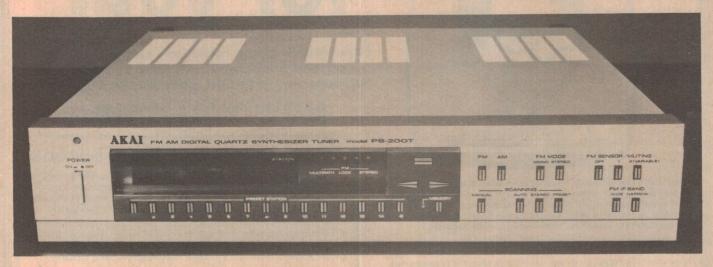
The other controls are also neat and equally clever. Apart from the normal

FM/AM, FM mono and stereo manual scanning, the automatic scanning capabilities and options involved therein are particularly clever. Firstly in the manual scanning mode, the unit jumps in 9 kHz increments on AM and in 50 kHz increments on FM. These frequencies have apparently been chosen to suit Japanese requirements for the US version makes use of 10 kHz AM and 100 kHz FM increments. With the manual control selected it is only necessary to touch the upward or downward scanning control which increments in single steps for a single touch or cycles automatically through the frequencies if the finger remains on the control for more than 11/2 seconds.

The receiver cycles up or down automatically looking for a station carrier with reasonable strength which it locks on to for approximately six seconds unless stopped. Otherwise it recommences its search process. It is not a good idea to look for a low strength signal in the auto mode as it is liable to scan over such a station and ignore any detected, in preference to another station with a higher signal strength. If the stereo mode is selected the search sequence stops each time the receiver detects a strong signal which it again holds for six seconds before recommencing its search programme.

In the preset mode the receiver will scan between the preselected stations only, locking on to that station for only six seconds unless stopped.

The only controls at the extreme right hand side of the escutcheon are the FM sensor/muting control which are normally in off position and which should be only depressed when tuning for a weak signal. A "level one" switch is provided which cuts interstation distortion generated prior to the input of the receiver, and which cannot be adjusted out. A "level two" control is provided for variable adjustment of the detection/muting level making use of a



muting level control at the rear of the receiver. Other controls are two optional stages of intermediate frequency filter bandwidths which are — 60 dB at +/- 300 kHz in the narrow mode and -50 dB at +/- 400 kHz bandwidth in the wideband mode.

The choice would undoubtedly be very valuable in America and Japan but as yet is of little significance in Australia.

The rear of the receiver has very few controls. The controls that are there consist of a distant or local FM sensitivity switch, a 75 ohm coaxial socket for the FM antenna, a special earth and aerial socket for AM, a distant or local switch for the AM band, a muting level control which works in conjunction with the level 2 variable control on the front panel of the receiver, two independent level controls for the left and right channels audio output, and a pair of fixed and variable coaxial audio outputs for feeding to the associated tune amplifier.

The mains connection is by means of a mains cord which differs from the brochure which shows the use of an IEC socket. The battery compartment is located at the top of the panel and it accepts three 1½ volt penlight cells to maintain the digital memory.

The inside of the equipment looks more like a piece of computer electronics than a piece of consumer electronics! The unit is divided into three sections. At the right hand front is the microprocessor and digital memory board which also contains the programmable counters and the logic

for the digital display. This is effectively screened off from the radio frequency tuner section which, not so surprisingly, does not contain normal tuning capacitors of the type we have grown to accept in FM and AM receivers. Instead of the conventional tuning section, both the FM and AM sections of this receiver incorporate digital quartz synthesizers to provide precise RF and mixer frequencies. These are followed by a multistage surface acoustic wave (SAW) filter and conventional ceramic filters in the subsequent stages. Akai does not say much about the surface acoustic wave filters but they are obviously very effective and precise.

The rear of the tuner contains a fancy regulated power supply for the circuitry together with the intermediate frequency stage filter located in its own separate screened can well isolated from the rest of the circuitry.

The microcomputer controlled synthesizer gives a more precise tuning performance than other systems and is coupled with a phase-locked loop which eliminates the possibility of further drift. These operate with variable capacitance diodes to control the local oscillator frequency.

# **Test results**

The RF sensitivity of this receiver falls a little short of what we would have otherwise expected from this unit. In particular, in the wide band mode the sensitivity is 1.3 microvolts for 20 dB signal-to-noise ratio with the input

switch set to the distant position, 7 microvolts when set to local.

In the AM mode in the distant position the sensitivity is 190 microvolts for 20 dB signal to noise ratio with 30% modulation and 2.6 millivolts in the local position. These figures may appear reasonable but suffer a little because of the absence from the lack of a tuned radio frequency stage which add so much to improve the overall signal-toratio and selectivity in noise conventionally designed radio receivers. The ultimate signal to noise ratio of the unit with 1 mV across at the input is 67 dB which is good considering that the program content has a far lower signal to noise ratio.

The FM band frequency response is particularly flat, being -3 dB down at 20 Hz and 16 kHz with the notch at 19 kHz extending down to 25 dB as a result of the effective removal of the pilot tone signal. The channel separation, as measured by our signal generator, is better than 37 dB midband and is limited by the generator performance rather than by the receiver. There is no significant difference between the FM audio response in either wide band or narrow band modes and so there is no loss of signal quality by utilising the narrow band position.

The AM response is smooth but uninspiring with a bandwidth extending from 70 Hz to 2.2 kHz at the -6 dB points. This makes it very suitable for listening to soap operas and the races. It is a shame that the designers of such equipment do not allow for the quality

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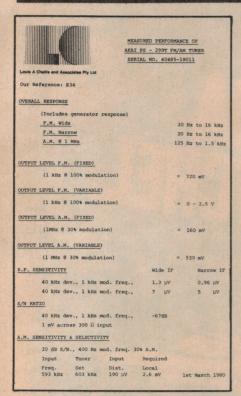
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# SMITH ELECTRON



OUR OTHER ADVERTS IN THIS MAGAZINE FOR OUR STORE ADDRESSES AND RESEL

# review



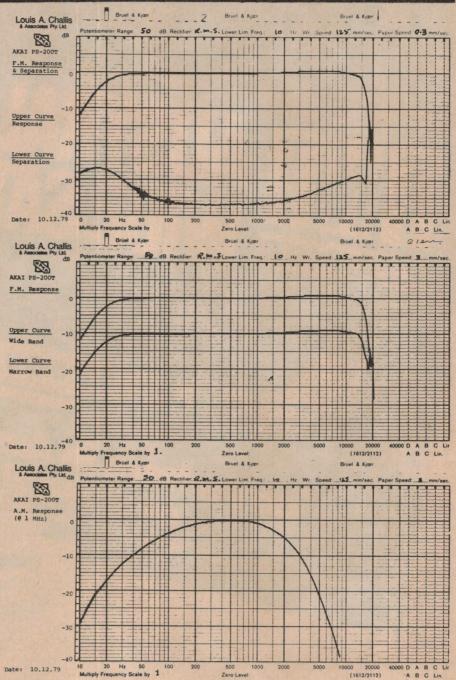
of transmission which our local AM stations provide and provide an AM band width of comparable quality to the FM. In practical use the ergonomic design of this receiver can only be described as simply delightful. The controls are quickly mastered, and provided you have hooked up a suitable aerial the quality of sound and the ease with which a station can be selected is inspiring.

Once the local stations have been selected, logged and recorded by the preset station facility their reselection takes virtually all the hard work out of what can sometimes be a laborious task. The quality of the signal we received on the FM was excellent and that from the AM, passable.

With only a 100 mm length of aerial on the rear of the receiver it happily picks up local stations on FM but requires a somewhat better aerial for AM reception (at least ½ metre of wire even without the benefit of an earth). With the addition of two good aerials, one for FM and one for AM, this unit can pull in distant stations with very reasonable ease.

# Summary

The quality of the sound is in general terms as good as some of the best tuners and receivers we have listened to but the sensitivity is not as good as the



very best. It is apparent that this unit has been designed for people who are not looking for the ultimate in radio frequency performance but are looking for the ultimate in ergonomic performance and an appearance to match.

The Akai PS-200T Tuner is one of the most exciting tuners we have evaluated, but at a selling price of \$899 recommended retail, will tend to discourage the majority of people who could most appreciate its functional beauty.

# THE AKAI PS-200T FM/AM DIGITAL QUARTZ SYNTHESIZER TUNER

Dimensions: 440mm wide x 90mm high x 443mm deep

Weight: 7.8 kg. Price: \$889 rrp.

Manufactured by: AKAI Electric Co., Tokyo, Japan

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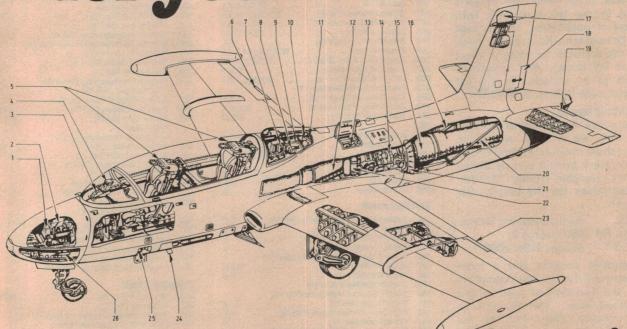
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\* 11th year will be required for 1982 entry for Certificate of Technology Scheme.

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# KITS for projects

WE GET MANY enquiries from readers wanting to know where they can get kits for the projects we publish. This list is a guide to suppliers of kits and components for ETI projects.

We have only listed the projects published in the last few years, with their dates of publication, so this page can also be used as an index, even though kits are not available for some of them (as far as we know). Any companies who wish to be included in this list should phone Jan Collins on 334282.

### Printed circuit boards

Those suppliers listed against specific projects here are able to supply pc boards for those projects. Printed circuit boards for every project ever published in ETI are available through the following companies (to the best of our knowledge):

RCS Radio Radio Despatch Service 651 Forest Rd 869 George St Bexley NSW Sydney NSW 2000

For current projects and a more comprehensive list of pc board suppliers refer to the Shoparound page in this and previous issues. This list will be updated roughly every four to six months.

## **Key to Companies**

- Applied Technology Pty Ltd, 1A Paterson Avenue, Waitara, NSW 2077
- Bill Edge Electronic Agencies, 115 Parramatta Road, Concord (PO Box 1005, Burwood North 2134).
- J.R. Components, PO Box 128, Eastwood, NSW 2122.
- Dick Smith Electronics P/L, Cnr Waterloo & Lane Cove Roads, North Ryde, 2113.
- All Electronic Components, 118 Lonsdale Street, Melbourne, Vic 3000
- Tasman Electronics, 12 Victoria Street, Coburg, Vic 3058.
- Jaycar Pty Ltd, PO Box K39, Haymarket, NSW 2000.
- S M Electronics, 10 Stafford Court, Doncaster East, Vic
- Ellistronics, 289 Latrobe Street, Melbourne, Vic 3000.
- Mode Electronics, PO Box 365, Mascot, NSW 2020.
- Nebula Electronics Pty Ltd, 15 Boundary Street, Rushcutters Bay, NSW 2011.
- 0 Orbit Electronics, PO Box 7176, Auckland, New Zealand.
- Pre-Pak Electronics, 718 Parramatta Road, Croydon.
- Rod Irving, PO Box 135, Northcote, Vic 3070.
- Silicon Valley, 23 Chandos Street, St. Leonards,
- W Willis Electronics, 993 Hay Street, Perth, WA 6000.
- Trilogy, 40 Princes Highway, Fairy Meadow, NSW 2519.

	ject Electronics	495			
041	Continuity Tester W,R,D,B,Y,L		scellaneous		
042	Soil Moisture Indicator	546	GSR Monitor (Mar 77)		
044	Two Tone Door Bell (Oct 76) . W,R,D,E,A,F,B,Y,L	547 548	Telephone Bell Extender (Jun 77) E		
045	500 Second Timer W,D,E,A,B,Y,L	549	Photographic Strobe (May 77) W,E Induction Balance Metal		
047	Morse Practice Set		Detector (May 77) W D F I		
048	Buzz Board W,D,A,B,Y,L	550	Digital Dial (Aug 78) F.O.		
061 062	Simple Amplifier (Oct 76) W,R,D,E,A,B,Y,L	551	Light Chaser (Sep 78) W.E.O		
063	Simple AM Tuner (Mar 77)	552	LED Pendant (Sep 78) A		
064	Simple Intercom (Nov 76)	553 556	Tape/Slide Synchroniser (Oct 78) E Wind Speed/Direction Indicator (Dec 78)		
065	Electronic Siren W,R,D,E,O,A,B,Y,L	557	Reaction Timer (Feb 79)		
066	Temperature Alarm (Dec 76) W,D,E,A,B,Y,L	558	Mast-head Strobe (Feb 79)		
067	Singing Moisture Meter D,B,Y	559	Cable Tester (Mar 79)		
068	LED Dice Circuit (Oct 76) W,R,D,E,A,B,L	575	Portable Fluorescent Light Wand for		
071	Electronic Tie Breaker (Jan 77) Tape Noise Limiter (Jun 78)	577	Car, Camping (Aug 79) W		
072	Two-Octave Organ (Jun 78) W,D,B,Y	581	General Purpose Power Supply		
081	Tachometer (Mar 77) W.E.O	582	House Alarm (Jul 77) W,E,O,A,		
082/			House Alarm —		
528			Installation Instructions (Aug 77) W		
083	Train Controller	583	Marine Gas Alarm (Aug 77) D,E,M		
085	Over-rev Alarm W,H,D,E,A,B,Y,L	585 586	Ultrasonic Switch (Sep 77) R,D,E,O,F		
086	FM Antenna W	587	Shutter Speed Timer (Oct 77) E UFO Detector (May 78)		
087	Over-LED W,E	588	Theatrical Lighting Controller		
088	Hi-Fi Speaker W		(Nov & Dec 77 Jan & Mar 78) N		
Tes	t Equipment	589	Digital Temperature		
132		500	Meter (PCB135) (Dec 77) E		
133	Experimenter's Power Supply (Feb 77) E,O Phase Meter (Apr 77) E	590 591	LCD Stopwatch (Oct 78) O,N		
134	True RMS Voltmeter (Aug77) E	592	Up/Down Presettable Counter (Jul 78) D,E Light Show Controller (Aug 78)		
135	Digital Panel Meter (Oct 77) E	593	Colour Sequencer (Dec 78)		
136	Linear Scale Capacitance Meter (Mar 78)	594	Development Timer (Apr 79) E		
137	Audio Oscillator (May 78) W,D,E	595	Aquarium Lamp Controller (May 79)		
138	Audio Wattmeter (Nov 78) E,B SWR/Power Meter (May 78)	Flor	stronio Music		
140	1GHz Frequency Meter-timer (Mar 78)	602	etronic Music		
141	Logic Trigger (Jan 79)	603	Mini Organ (Aug 76) W,D,E,A Sequencer (Aug 77) W		
142	High Current Power Supply (Feb 79) W,E	604	Accentuated Beat Metronome (Sep 77) E		
143	Curve Tracer (Jan 79) W	605	Temp Stabilized Log-exponential		
144	Expanded-scale RMS Voltmeter (Jun 79) E		Converter (Sep 78)		
148	Versatile Logic Test Probe (Jul 79) E,L	Com	puter Projects		
SIM	ole Projects	630	Hex Display (Dec 76) E.A		
243	Bip Beacon (Apr 77)	631	ASCII Keyboard (Dec 76) W,E,O,A		
244	Alarm Alarm (Feb 77) F	631	Keyboard Encoder (Apr 77) W,E,O,A		
245	White Line Follower (Nov 77) F Rain Alarm (Apr 78) F	632	Video Display Unit (Jan 77) E,O,A		
248	Simple 12V to 22V Converter (Jul 78)	633	TV Sync Generator (Jan 77) E,A 8080 Educational/Prototyping		
249	Electronic Combination Lock (Apr 79) E	004	Interface (Jul, Aug 78)		
252	The Passionmeter (Aug 79)	635	Microcomputer Power Supply (Sep 77) O		
253	Electronic Grenade (Hot Potato) (May 79)	637	Cuts Cassette Interface (Jun 78) V,E,A		
254	Egg Timer (Jun 79) W	638	Eprom Programmer (Jul 78) W,E,A		
	rists' Projects	639 640	Computerised Musical Doorbell (Mar 78) A		
316	Transistor Assisted Ignition (May 77) W,E,O,K	641	S100 VDU (Apr, May, Jun 78)		
317	Rev. Monitor Counter (Jul 77) E	642	16k S100 RAM Card (Feb 79)		
319	Digital Car Tacho (Jul 78) W,E,K Variwiper MK II (Sep 78) W,E,O	650	STAC Timer (Nov 78) E,A,L		
320	Battery Condition Indicator (Apr 79) E,L	651	Binary to Hex Number Converter (Jun 79) E		
	Audio Projects  712 CB Power Supply (Jun 77)				
		712	CB Power Supply (Jun 77) W,E		
448 449	Disco Mixer (Nov 76)	713	Add-on FM Tuner (Sep 77)		
450	Balanced Microphone Amp (Nov 76) W,D,E,J,F,Y Bucket Brigade Audio Delay Line (Dec 77) W,E	714 715	VHF-Log-Periodic Antenna (Feb, Mar 78)		
451	Hum Filter (Jul 79)	716	VHF Power Amplifiers (Nov 77) VHF Power Amplifiers (Jan, Feb 78)		
455	Class A Headphone Amp (Nov 78)	717	Crosshatch Generator (May 78) W.D.E.A.Y		
470	60 W Amp Module (May 79) W,R,E,F,B,P,L,A,V	718	SW Radio (Oct 78)		
471	High Performance Stereo Preamp Control	719	RF Field Strength Indicator (Nov 78)		
472	Unit (Jun 79)	720	2m VMOS Power Amp (Jan 79)		
	Amp (Jul 79) W,R,E,F,B,A,V,L	721 722	Aircraft Band Converter (Mar 79) W,E Antenna for Aircraft Band		
473	Series 4000 Moving-coil Cartridge	,	Converter (May 79)		
	Preamplifier F,J	724	Microwave Oven Leak Detector (Jul 79) D.E.B		
480	50-100 Watt Amp	725	Simple SSB Generator employs Polyphase		
481	Modules (Dec 76)	700	Network using Standard Components (Aug 79) . E.L		
481	High Power PA/Guitar Amp (Jun 77) W	730	Get Going on Radioteletype (Aug 79) E,L		
482	Stereo Amp (Jan 77) O.F.		ronic Games		
482	Stereo Amp Part 2 (Feb 77) O.E	804	Selectagame (Nov 76) O		
483	Sound Level Meter (Feb 78) E	804	Selectagame (Rifle Project) (Mar 77) O		
484 485	Simple Compressor Expander (Jul 77) E,A Graphic Equaliser (Jun 77)	805 806	Puzzle of the Drunken Sailor (Oct 77)		
486	Howl-round Stabiliser (Nov 77)	810	Skeet (Jan 78)         0           Stunt Cycle TV Game (Jun 78)         D,O		
487	Audio Spectrum Analyser (Feb 78)	811	TV Tank Game (Oct 78)		
489	Audio Spectrum Analyser 2 (Apr 78) E,J	812	Wheel of Fortune (Dec 78)		
490	Audio Compressor (Dec 78)	813	Race Track Game (Jan 79)		
491	Simple Graphic Equaliser (Mar 79) W,E	814	The 'Dinky-Die' (Aug 79)		



Editor

Roger Harrison VK2ZTB

Project Manager Phil Wait VK2ZZQ

**Editorial Staff** 

Roberta Kennedy Jonathan Scott VK2YBN David Tilbrook VK2YMI Jan Vernon

Art Direction and technical photography

**Ivy Hansen** 

Lavout Bill Crump

Reader Services Jan Collins

Managing Editor Collyn Rivers

**Acoustical Consultants** Louis Challis & Associates

Editorial and Sales Office 4th Floor, 15 Boundary St **Rushcutters Bay NSW 2011** Ph: 33-4282; Tlx: 27243

Sales Manager: Bob Taylor Sales Admin: Jan Collins (address as above)

Melbourne Tom Bray 150 Lonsdale St Melbourne Vic 3000 Ph: 662-1222; Tlx AA34543

Adelaide Admedia Group 24 Kensington Rd Rose Park SA 5067 Ph: 332-8144; Tlx AA82182

Brisbane Geoff Horne Agencies 60 Montanus Drive Bellbowrie QLD 4070 Ph: 202-6229

Hobart 23 Lord St Sandy Bay Tas 7005 Ph: 34-2630

Perth Aubrey Barker 133 St Georges Terrace Perth WA 6000 Ph: 322-3184; Tlx: AA93810 Ph: 751-3383; Tlx: 620892

Auckland Geoff Collins Catalyst Ltd Cnr. Pauls & Airedale Sts Auckland NZ Ph: 79-4168

London Australian Consolidated Press Ludgate House 107 Fleet St London EC4A 2AL Ph: 353-1040: Tlx: 267163

Genzo Uchida Bancho Media Services 15 Sanyeicho Shin iuku-Ku Tokyo 160 Ph: 359-8866 Cable: Elbanchorito

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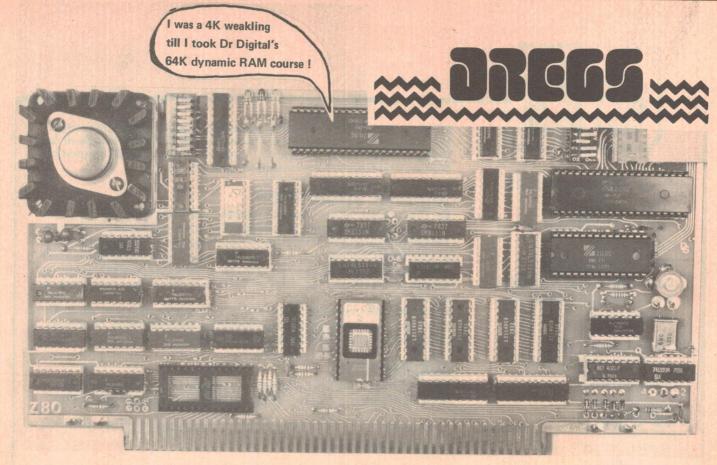
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ONE DOESN'T EXPECT advertising copywriters to be all that technically accurate when it comes to preparing advertisements for the daily press, just so long as what is said is not too wide of the mark or hopelessly vague.

A West Australian reader spotted an advertisement in a local daily, The West Australian (10-3-80), for STC's new Telefax document transmission machine which broke all the rules without (hopefully) breaking the law. Here's what it read:

"For the business that truly needs instant information delivery STC Telefax Facsimile is the instant answer: Documents, plans, photographs, in fact any printed matter can be sent interstate or across the city and be on the right desk in 3 minutes flat. Think of it as your 3-minute interstate courier.

"Today, STC has the technology to turn information into laser light and back again, by using optic fibres. These optic fibres will replace yesterday's huge data transmission cables; they are threads of glass, fine as human hair. Their advantages are vast because their size is so small. Just one tiny fibre can carry as much information as a giant telephone cable as thick as your arm" (our emphasis).

Einstien, Planck, Shannon and co. were mere dabblers, eh?

# **Space spectaculars**

First came "A Space Odyssey: 2001", the archetypal science fiction/fantasy/prediction space spectacular (cross out whichever term is not applicable).

Then came a seven/eight year drought, followed by "Star Wars". A cowboys-&-indians/cops-&-robbers movie, only set in the vast, four-dimensional panorama of space.

Hot on its heels came "Star Trek; the motion picture", a revamp of the ancient TV series (borrowing concepts from "Superman: the movie" and "Star Wars"), and "Alien", a meld of the recently popular horror/supernatural epics, plus a number of lesser rivals known for their meteoric rise and fall, and little else.

You could have laid very good odds on the Disney empire getting into the act somewhere along the line and be assured of winning, if you could have found a bookie to take the bet. Sure enough, their contribution to the rash of space spectacular productions in the closing years of the last decade (depending on when you count the decade from . . .) is "The Black Hole". This seems to borrow from such diverse fields as the 'disaster' movies (like "Airport" and "Concorde"), the space spectaculars that preceeded it

and the cowboys/indians — cops/robbers formulae of old.

The Black Hole seems to be the penultimate in the 'space opera' genre. What next — "The Seven White Dwarfs"?

# Very red faces dept.

Our April Dregs column noted that June and November 1976 were two bad months for certain staff members of our illustrious rival E...A....

The column stated that those issues inadvertently featured ETI's Australian and UK advertising sales managers (respectively) on E...A....'s June front cover and page 26 of their November issue.

Our comment that E...A...'s front cover featured our (then) sales manager Howard Jenkins was published in the belief that the statement was correct. We now understand from E...A...'s editor-in-chief and from Howard Jenkins that the pix was actually of E...A...'s Greg Swain.

The November pix did feature ETI UK's sales manager but the pix accompanied a feature put out by the UK Information Service (concerning Viewdata) and there was no way that any other magazine could know that the pix was that of one of our own staff.

We unreservedly apologise for any embarrassment caused.

# AND IT'S ALL IN OUR COLOUR CATALOGUE

The truth is, JVC have always produced real hi-fi components and we believe this current range represents JVC's finest range ever. Here are some real innovations and performance features to whet your appetite:— Quartz locked turntables with uncanny accuracy; Receivers/Amplifiers, some with built-in SEA Graphic Equaliser and DC, class A/B amplification; Cassette deck with JVC automatic computerised tape tuning; Computer designed

speaker systems; Separate but matching JVC components designed to compliment one another, perfectly. And all this real hi-fi know-how is yours ...merely for the asking.

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Just fill out this coupon and we'll fill you in on what's available and new in terms of JVC hi-fi entertainment...and it's all FREE!

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Just address your envelope to... JVC Hi-Fi Advisory Service, Post Office Box 307, North Ryde, N.S.W. 2113

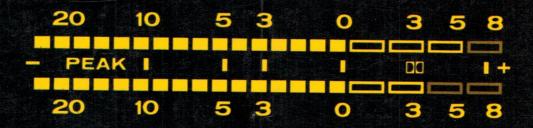


the right choice



If you think they look different, wait till you've heard them!

# What you see on the meters you'll hear on the tape.





Including the latest ideas is audio technology in modestly priced hi-fi components is a principle to which Technics is committed.

The inclusion of our most accurate metering system, the FL (fluorescent) bar graphs in the RS-M17 model cassette deck is another example.

electronically controlled so response time is instantaneous. Each bar length is proportional to the sound level, and there's no overshoot - a characteristic of conventional needle-type meters. The meters give direct parallel readout for instant comparison between channels.

Other practical features on the To make an accurate recording you RS-M17 cassette deck are rewind autoneed accurate meters. The FL meters are play, so you spend more time listening to

your tapes and less time just pressing buttons; the highly reliable Super Permalloy head; 3-position tape selection for optimum results from the tape type you use; and Dolby\* noise reduction system.

You won't find a similarly priced cassette deck with more features than the RS-M17. See for yourself and your Technics dealer.